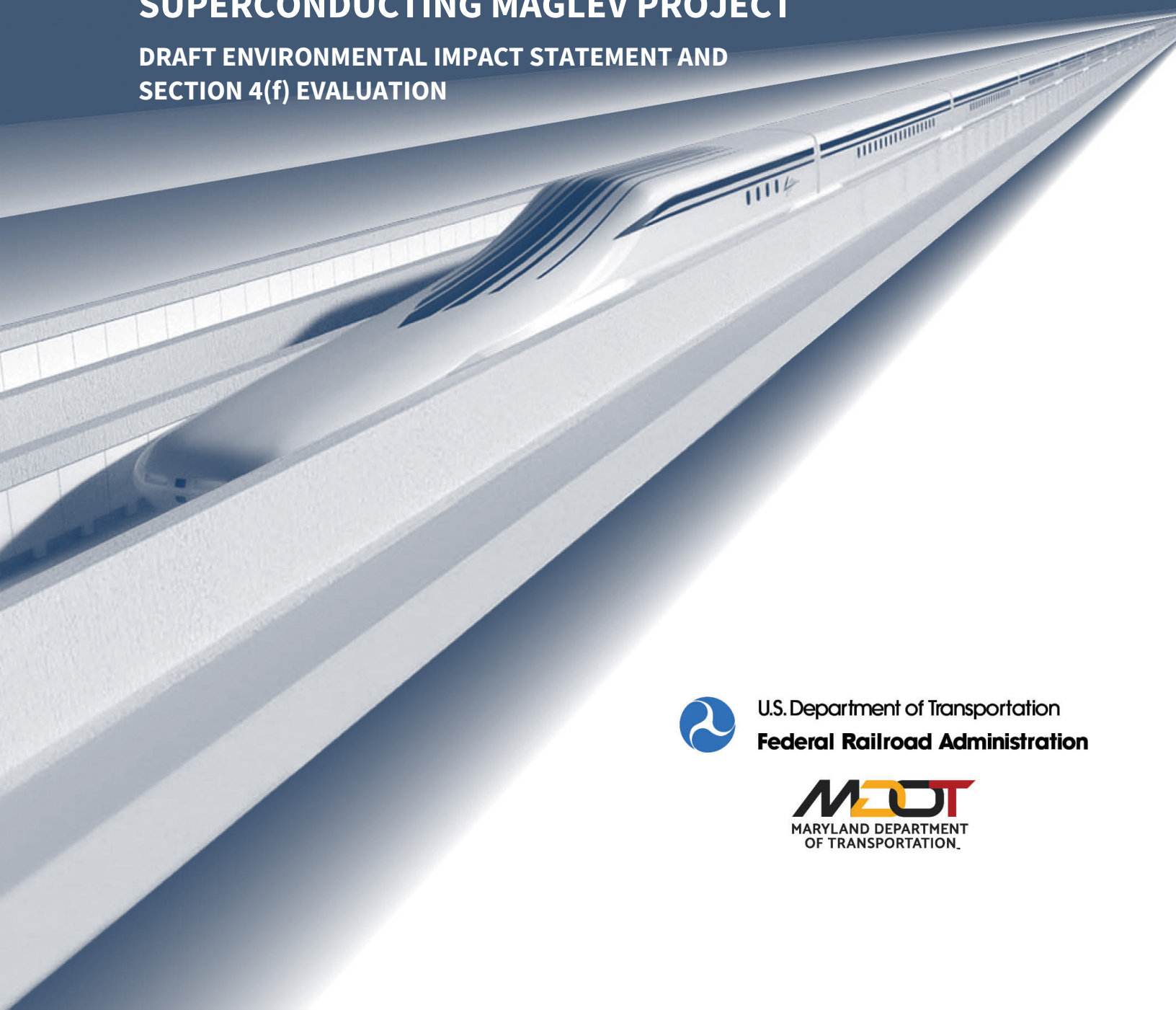
Appendix D.9

Air Quality Technical Report

Attachments

BALTIMORE-WASHINGTON, D.C. SUPERCONDUCTING MAGLEV PROJECT

DRAFT ENVIRONMENTAL IMPACT STATEMENT AND SECTION 4(f) EVALUATION



U.S. Department of Transportation
Federal Railroad Administration

MARYLAND DEPARTMENT OF TRANSPORTATION

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ATTACHMENT A – SAMPLE CO CAL3QHC MODELING OUTPUT PRINTOUT

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CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.0 Dated 95221                    PAGE  1

   JOB: 2027 Baltimore3 Howard and Conway                RUN: 2027 Baltimore3 Howard and Conway

     DATE :  8/ 9/20
     TIME :  1:18:10

        The MODE flag has been set to c for calculating CO averages.

      SITE & METEOROLOGICAL VARIABLES
      -------------------------------
      VS =   0.0 CM/S       VD =   0.0 CM/S       Z0 = 175. CM
       U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =  0.0 PPM

      LINK VARIABLES
      --------------
        LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                             *   X1        Y1        X2        Y2      *     (FT)   (DEG)           (G/MI)   (FT) (FT)       (VEH)
     ------------------------*-----------------------------------------*-----------------------------------------------------------
      1. A-WB-W Conway St    * ********  589339.9  ********  589295.6 *     619.   266. AG   1933.   7.1   0.0 56.0
      2. A-WB-W Conway St-1  * ********  589295.6  ********  589289.1 *     322.   269. AG    473.   7.1   0.0 32.0
      3. A-WB-W Conway St-2  * ********  589295.6  ********  589266.9 *     337.   265. AG    730.   7.1   0.0 32.0
      4. A-WB-W Conway St-3  * ********  589295.6  ********  589251.3 *     339.   262. AG    730.   7.1   0.0 32.0
      5. A-SB-S Howard St    * ********  590250.0  ********  589643.3 *     607.   178. AG   1326.   7.1   0.0 56.0
      6. A-SB-S Howard St-1  * ********  589643.3  ********  589284.9 *     360.   186. AG     33.   7.1   0.0 32.0
      7. A-SB-S Howard St-2  * ********  589643.3  ********  589255.3 *     388.   182. AG    646.   7.1   0.0 32.0
      8. A-SB-S Howard St-3  * ********  589643.3  ********  589257.8 *     385.   180. AG    646.   7.1   0.0 32.0
      9. A-NB-Camden Sta     * ********  588632.2  ********  589110.7 *     479.   357. AG     77.   7.1   0.0 32.0
     10. A-NB-Camden Sta-1   * ********  589110.7  ********  589244.1 *     134.     2. AG     68.   7.1   0.0 32.0
     11. A-NB-Camden Sta-2   * ********  589110.7  ********  589252.6 *     142.   359. AG      9.   7.1   0.0 32.0
     12. A-EB-Camden Sta-1   * ********  589244.1  ********  589244.3 *     172.    90. AG     68.   7.1   0.0 32.0
     13. A-EB-Camden Sta-2   * ********  589252.6  ********  589264.9 *     218.    87. AG      9.   7.1   0.0 32.0
     14. A-NB-I395           * ********  588286.9  ********  588957.5 *     671.   358. AG   3508.   7.1   0.0 56.0
     15. A-NB-I395-1         * ********  588957.5  ********  589204.9 *     249.     6. AG   1437.   7.1   0.0 44.0
     16. A-NB-I395-2         * ********  588957.5  ********  589262.0 *     306.   354. AG   2071.   7.1   0.0 44.0
     17. D-EB-W Conway St    * ********  589204.9  ********  589278.9 *     897.    85. AG   1437.   7.1   0.0 56.0
     18. D-NB-S Howard St    * ********  589278.0  ********  590248.5 *     972.   357. AG   2325.   7.1   0.0 56.0
     19. D-WB-Camden Sta     * ********  589277.1  ********  589266.9 *     196.   267. AG    261.   7.1   0.0 32.0
     20. D-SB-Camden Sta     * ********  589266.9  ********  588633.3 *     634.   177. AG    261.   7.1   0.0 32.0
     21. D-SB-I395           * ********  589248.5  ********  588288.4 *     962.   177. AG   2821.   7.1   0.0 68.0
     22. Q-WB-W Conway St-1  * ********  589295.6  ********  589291.2 *     217.   269. AG     24. 100.0   0.0 32.0 0.85  11.0
     23. Q-WB-W Conway St-2  * ********  589295.6  ********  589220.9 *     880.   265. AG     24. 100.0   0.0 32.0 1.06  44.7
     24. Q-WB-W Conway St-3  * ********  589295.6  ********  589180.6 *     880.   262. AG     24. 100.0   0.0 32.0 1.06  44.7
     25. Q-SB-S Howard St-1  * ********  589643.3  ********  589632.1 *      11.   186. AG     19. 100.0   0.0 32.0 0.05   0.6
     26. Q-SB-S Howard St-2  * ********  589643.3  ********  589425.3 *     219.   186. AG     19. 100.0   0.0 32.0 0.73  11.1
     27. Q-SB-S Howard St-3  * ********  589643.3  ********  589424.3 *     219.   180. AG     19. 100.0   0.0 32.0 0.73  11.1
     28. Q-EB-Camden Sta-1   * ********  589244.1  ********  589244.1 *      29.    90. AG     24. 100.0   0.0 32.0 0.11   1.5
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29. Q-EB-Camden Sta-2	* ********	589252.6	********	589252.8 *	4.	81.	AG	24.	100.0	0.0	32.0	0.01	0.2
30. Q-NB-I395-2	* ********	588957.5	********	589306.6 *	351.	354.	AG	38.	100.0	0.0	44.0	0.58	17.8

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

DATE : 8/ 9/20
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ADDITIONAL QUEUE LINK PARAMETERS

LINK DESCRIPTION	*	CYCLE LENGTH (SEC)	RED TIME (SEC)	CLEARANCE LOST TIME (SEC)	APPROACH VOL (VPH)	SATURATION FLOW RATE (VPH)	IDLE EM FAC (gm/hr)	SIGNAL TYPE	ARRIVAL RATE
22. Q-WB-W Conway St-1	*	140	78	4.0	473	1397	16.09	1	3
23. Q-WB-W Conway St-2	*	140	78	4.0	730	1717	16.09	1	3
24. Q-WB-W Conway St-3	*	140	78	4.0	730	1717	16.09	1	3
25. Q-SB-S Howard St-1	*	140	62	4.0	33	1392	16.09	1	3
26. Q-SB-S Howard St-2	*	140	62	4.0	646	1719	16.09	1	3
27. Q-SB-S Howard St-3	*	140	62	4.0	646	1719	16.09	1	3
28. Q-EB-Camden Sta-1	*	140	78	4.0	68	1615	16.09	1	3
29. Q-EB-Camden Sta-2	*	140	78	4.0	9	1787	16.09	1	3
30. Q-NB-I395-2	*	140	62	4.0	2071	3471	16.09	1	3

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
1. R1	*	********	589317.9	6.0	*
2. R2	*	********	589315.7	6.0	*
3. R3	*	********	589313.6	6.0	*
4. R4	*	********	589311.4	6.0	*
5. R5	*	********	589309.3	6.0	*
6. R6	*	********	589307.1	6.0	*
7. R7	*	********	589307.1	6.0	*
8. R8	*	********	589334.3	6.0	*
9. R9	*	********	589369.3	6.0	*
10. R10	*	********	589404.3	6.0	*
11. R11	*	********	589439.2	6.0	*
12. R12	*	********	589474.1	6.0	*
13. R13	*	********	589509.2	6.0	*
14. R14	*	********	589503.1	6.0	*
15. R15	*	********	589468.3	6.0	*
16. R16	*	********	589433.4	6.0	*
17. R17	*	********	589398.4	6.0	*
18. R18	*	********	589363.5	6.0	*
19. R19	*	********	589328.5	6.0	*
20. R20	*	********	589298.2	6.0	*

21. R21	*	********	589290.6	6.0 *
22. R22	*	********	589288.4	6.0 *
23. R23	*	********	589286.2	6.0 *
24. R24	*	********	589284.0	6.0 *
25. R25	*	********	589281.8	6.0 *
26. R26	*	********	589087.0	6.0 *
27. R27	*	********	589116.9	6.0 *
28. R28	*	********	589146.9	6.0 *
29. R29	*	********	589176.9	6.0 *
30. R30	*	********	589206.8	6.0 *
31. R31	*	********	589224.9	6.0 *
32. R32	*	********	589226.1	6.0 *
33. R33	*	********	589227.5	6.0 *
34. R34	*	********	589150.0	6.0 *
35. R35	*	********	589120.0	6.0 *
36. R36	*	********	589090.1	6.0 *

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

DATE : 8/ 9/20
TIME : 1:18:10

RECEPTOR LOCATIONS

RECEPTOR	*	COORDINATES (FT) X	Y	Z	*
37. R37	*	********	589060.1	6.0	*
38. R38	*	********	589030.2	6.0	*
39. R39	*	********	589000.2	6.0	*
40. R40	*	********	588988.1	6.0	*
41. R41	*	********	589023.1	6.0	*
42. R42	*	********	589058.1	6.0	*
43. R43	*	********	589093.0	6.0	*
44. R44	*	********	589127.2	6.0	*
45. R45	*	********	589159.8	6.0	*
46. R46	*	********	589184.6	6.0	*
47. R47	*	********	589195.3	6.0	*
48. R48	*	********	589199.8	6.0	*
49. R49	*	********	589202.9	6.0	*
50. R50	*	********	589205.9	6.0	*
51. R51	*	********	589209.1	6.0	*
52. R52	*	********	589212.1	6.0	*

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
0.	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.8	0.8	0.8	0.8	0.8	0.8	0.4	0.3	0.4	0.4	0.4	0.5	0.3
1.	0.0	0.0	0.0	0.0	0.1	0.1	0.4	0.8	0.8	0.8	0.8	0.8	0.8	0.4	0.4	0.4	0.4	0.5	0.5	0.4
2.	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.8	0.8	0.8	0.8	0.7	0.7	0.6	0.4	0.4	0.5	0.5	0.5	0.4
3.	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.5	0.7	0.5	0.5	0.5	0.4
4.	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.7	0.7	0.7	0.7	0.7	0.7	0.6	0.7	0.7	0.6	0.6	0.6	0.4
5.	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.6	0.6	0.6	0.6	0.6	0.6	0.7	0.7	0.7	0.7	0.6	0.6	0.5
6.	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.5	0.5	0.6	0.6	0.6	0.7	0.7	0.7	0.7	0.6	0.6	0.5
7.	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.5	0.5	0.5	0.6	0.6	0.7	0.8	0.7	0.7	0.6	0.6	0.5
8.	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.4	0.4	0.4	0.4	0.4	0.4	0.8	0.7	0.7	0.7	0.6	0.6	0.6
9.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.4	0.4	0.4	0.4	0.4	0.8	0.7	0.7	0.7	0.6	0.6	0.6
10.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.4	0.4	0.4	0.4	0.4	0.9	0.7	0.7	0.7	0.6	0.6	0.6
11.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.9	0.7	0.7	0.7	0.6	0.6	0.6
12.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.9	0.8	0.7	0.7	0.6	0.6	0.6
13.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.9	0.8	0.7	0.7	0.6	0.6	0.6
14.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.3	0.9	0.8	0.8	0.7	0.6	0.7	0.6
15.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.7	0.6	0.7	0.6
16.	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.8	0.6	0.7	0.6
17.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.8	0.6	0.7	0.6
18.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.7	0.6	0.6	0.5
19.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.7	0.5	0.6	0.5
20.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.7	0.5	0.6	0.5
21.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.8	0.6	0.5	0.6	0.5
22.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.8	0.8	0.6	0.6	0.6	0.5
23.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.8	0.8	0.6	0.5	0.6	0.5
24.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.8	0.7	0.6	0.5	0.6	0.5
25.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.8	0.7	0.6	0.6	0.6	0.5
26.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.9	0.8	0.7	0.6	0.6	0.6	0.5
27.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.9	0.7	0.6	0.6	0.6	0.6	0.5
28.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.9	0.7	0.6	0.6	0.6	0.6	0.5
29.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.7	0.6	0.6	0.6	0.5

30.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.8	0.7	0.6	0.6	0.6	0.5
31.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.7	0.6	0.5	0.6	0.5
32.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.7	0.5	0.5	0.6	0.5
33.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.7	0.5	0.5	0.6	0.5
34.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.7	0.5	0.5	0.6	0.5
35.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.6	0.5	0.5	0.6	0.5
36.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.6	0.5	0.5	0.6	0.5
37.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.6	0.5	0.5	0.6	0.5
38.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.6	0.5	0.5	0.6	0.5
39.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.8	0.7	0.6	0.5	0.5	0.6	0.5
40.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.7	0.6	0.5	0.5	0.6	0.5
41.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.7	0.6	0.5	0.5	0.6	0.5

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

42.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
43.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
44.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
45.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
46.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
47.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
48.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
49.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.7	0.6	0.6	0.5	0.5	0.5	0.5
50.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.6	0.6	0.6	0.5	0.5	0.5	0.5
51.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.1	0.6	0.6	0.6	0.5	0.5	0.5	0.5
52.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
53.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
54.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
55.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
56.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
57.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
58.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
59.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
60.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
61.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
62.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
63.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
64.	*	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4

65.	*	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
66.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
67.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
68.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
69.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
70.	*	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
71.	*	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
72.	*	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
73.	*	0.2	0.1	0.1	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
74.	*	0.2	0.1	0.1	0.1	0.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
75.	*	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.4
76.	*	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.5
77.	*	0.2	0.2	0.2	0.1	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.5	0.5
78.	*	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.6	0.5
79.	*	0.3	0.2	0.2	0.3	0.3	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.6	0.5
80.	*	0.3	0.2	0.2	0.3	0.3	0.3	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.5	0.6	0.5
81.	*	0.3	0.2	0.2	0.3	0.5	0.4	0.3	0.1	0.1	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.6	0.6	0.7
82.	*	0.3	0.4	0.4	0.5	0.6	0.5	0.4	0.1	0.1	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.6	0.6	0.7
83.	*	0.4	0.4	0.4	0.6	0.6	0.5	0.4	0.1	0.1	0.0	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.6	0.6	0.7
84.	*	0.4	0.4	0.5	0.6	0.7	0.7	0.5	0.1	0.1	0.1	0.0	0.0	0.0	0.6	0.6	0.6	0.5	0.6	0.6	0.9
85.	*	0.5	0.4	0.5	0.7	0.7	0.7	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.6	0.6	0.6	0.6	0.6	0.7	0.9
86.	*	0.5	0.4	0.6	0.7	0.7	0.7	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.6	0.6	0.6	0.6	0.6	0.7	0.9
87.	*	0.5	0.6	0.8	0.7	0.7	0.7	0.5	0.2	0.1	0.1	0.0	0.0	0.0	0.6	0.6	0.6	0.6	0.6	0.7	0.9
88.	*	0.5	0.6	0.8	0.7	0.7	0.7	0.5	0.2	0.1	0.1	0.1	0.0	0.0	0.6	0.6	0.7	0.6	0.6	0.7	0.9
89.	*	0.5	0.7	0.8	0.7	0.7	0.8	0.6	0.2	0.1	0.1	0.1	0.0	0.0	0.6	0.6	0.7	0.6	0.7	0.7	0.9
90.	*	0.5	0.7	0.8	0.7	0.7	0.8	0.8	0.2	0.2	0.1	0.1	0.0	0.0	0.6	0.6	0.7	0.6	0.7	0.8	1.0
91.	*	0.5	0.7	0.8	0.7	0.7	0.9	0.8	0.2	0.2	0.1	0.1	0.0	0.0	0.6	0.7	0.7	0.6	0.7	0.8	1.0
92.	*	0.5	0.8	0.8	0.7	0.8	0.9	0.8	0.2	0.2	0.1	0.1	0.1	0.0	0.6	0.7	0.7	0.6	0.7	0.9	1.0
93.	*	0.6	0.8	0.8	0.8	0.8	0.9	0.8	0.3	0.2	0.1	0.1	0.1	0.0	0.6	0.7	0.7	0.7	0.7	1.0	1.0

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

94.	*	0.7	0.8	0.8	0.8	0.9	0.9	0.8	0.4	0.2	0.2	0.1	0.1	0.0	0.7	0.7	0.7	0.7	0.7	1.0	1.0
95.	*	0.8	0.8	0.8	0.8	1.0	1.0	0.8	0.4	0.2	0.2	0.1	0.1	0.1	0.7	0.7	0.7	0.7	0.7	1.0	1.0
96.	*	0.8	0.9	1.0	0.9	1.0	1.0	0.9	0.5	0.2	0.2	0.1	0.1	0.1	0.7	0.7	0.8	0.7	0.7	1.0	1.1
97.	*	0.9	0.9	0.9	0.9	1.0	1.0	0.9	0.5	0.2	0.2	0.1	0.1	0.1	0.7	0.7	0.7	0.7	0.7	1.0	1.0
98.	*	0.9	0.9	0.9	0.9	1.1	1.0	0.9	0.5	0.2	0.2	0.2	0.1	0.1	0.7	0.7	0.7	0.7	0.7	1.0	1.0
99.	*	0.9	1.0	0.9	1.0	1.1	1.1	1.0	0.5	0.2	0.2	0.2	0.1	0.1	0.7	0.7	0.7	0.7	0.7	0.9	1.0

100.	*	0.9	1.0	1.0	1.1	1.0	1.1	1.0	0.5	0.2	0.2	0.2	0.1	0.1	0.7	0.8	0.7	0.7	0.7	0.9	1.2
101.	*	1.0	1.0	1.0	1.1	1.1	1.1	1.0	0.5	0.2	0.2	0.2	0.1	0.1	0.7	0.8	0.7	0.7	0.8	0.9	1.2
102.	*	1.0	1.0	1.0	1.2	1.1	1.1	1.1	0.5	0.2	0.2	0.2	0.2	0.1	0.7	0.8	0.7	0.7	0.8	0.9	1.1
103.	*	1.0	1.1	1.0	1.1	1.1	1.1	1.1	0.5	0.2	0.2	0.2	0.2	0.1	0.7	0.8	0.7	0.7	0.8	0.9	1.0
104.	*	0.9	1.0	1.0	1.1	1.1	1.1	1.0	0.5	0.2	0.2	0.2	0.2	0.1	0.8	0.8	0.7	0.7	0.9	0.9	1.0
105.	*	0.9	1.0	1.1	1.1	1.1	1.1	1.0	0.6	0.2	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.9	0.9	1.1
106.	*	0.9	1.0	1.0	1.1	1.1	1.1	1.0	0.6	0.3	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.9	0.8	1.1
107.	*	1.0	1.0	1.0	1.1	1.1	1.1	1.0	0.6	0.3	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.9	0.8	1.1
108.	*	1.0	1.0	1.0	1.1	1.1	1.1	0.9	0.6	0.3	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.9	0.8	1.0
109.	*	1.0	1.0	1.0	1.1	1.1	1.1	0.9	0.6	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.8	1.0
110.	*	1.0	1.1	1.0	1.1	1.1	1.0	0.9	0.6	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.8	1.0
111.	*	1.0	1.1	1.0	1.1	1.1	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.8	1.0
112.	*	1.0	1.0	1.0	1.1	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.7	1.1
113.	*	1.0	1.0	1.0	1.1	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.7	1.1
114.	*	1.0	1.0	1.0	1.1	1.0	1.0	0.9	0.5	0.5	0.2	0.2	0.2	0.2	0.8	0.8	0.7	0.7	0.8	0.7	1.0
115.	*	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.6	0.7	0.8	0.8	1.0
116.	*	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.6	0.7	0.8	0.8	0.9
117.	*	1.0	1.0	1.0	1.0	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.8	0.6	0.7	0.7	0.8	0.9
118.	*	1.0	1.0	0.9	1.0	1.0	1.0	0.9	0.5	0.4	0.2	0.2	0.2	0.2	0.8	0.7	0.6	0.8	0.7	0.8	0.9
119.	*	0.9	1.0	0.9	0.9	1.0	1.0	0.9	0.5	0.4	0.1	0.2	0.2	0.2	0.8	0.7	0.6	0.8	0.7	0.9	0.9
120.	*	0.9	1.0	0.9	0.9	1.0	0.9	0.9	0.4	0.4	0.2	0.2	0.2	0.2	0.8	0.7	0.6	0.8	0.7	0.8	0.9
121.	*	0.9	1.0	0.9	0.9	1.0	0.9	0.9	0.4	0.4	0.2	0.2	0.2	0.2	0.7	0.7	0.6	0.8	0.7	0.8	1.0
122.	*	0.9	1.0	0.9	0.9	1.0	0.9	0.9	0.4	0.4	0.2	0.1	0.2	0.2	0.7	0.7	0.6	0.8	0.7	0.8	0.9
123.	*	0.9	0.9	0.9	0.9	1.0	0.9	0.9	0.4	0.4	0.2	0.1	0.2	0.2	0.7	0.7	0.6	0.8	0.7	0.8	0.9
124.	*	1.0	0.9	0.9	0.9	0.9	0.9	0.9	0.4	0.4	0.4	0.2	0.3	0.3	0.7	0.7	0.6	0.8	0.7	0.8	0.9
125.	*	1.0	0.9	0.9	0.9	0.9	0.9	0.8	0.5	0.5	0.4	0.2	0.3	0.3	0.7	0.7	0.6	0.8	0.7	0.8	0.9
126.	*	1.0	0.9	0.9	0.9	0.9	0.9	0.7	0.5	0.5	0.4	0.2	0.2	0.3	0.7	0.7	0.6	0.8	0.7	0.8	0.9
127.	*	1.0	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.3	0.7	0.7	0.6	0.8	0.8	0.8	0.9
128.	*	1.0	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.3	0.7	0.7	0.6	0.8	0.8	0.7	0.8
129.	*	1.0	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.8	0.8	0.7	0.8
130.	*	1.0	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.8	0.8	0.7	0.8
131.	*	1.0	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.8	0.9	0.8
132.	*	0.9	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.8	0.9	0.8
133.	*	0.9	0.9	0.9	0.9	0.9	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.6	0.9	0.9
134.	*	0.9	0.9	0.9	0.9	0.9	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.5	0.7	0.9	1.0
135.	*	0.9	0.9	0.9	0.9	0.9	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.6	0.9	1.0
136.	*	0.9	0.9	0.9	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.6	0.8	1.0
137.	*	0.9	0.9	0.8	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.7	0.7	1.0
138.	*	0.9	0.9	0.8	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.8	0.7	1.0
139.	*	0.9	0.9	0.8	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.8	0.7	1.0
140.	*	0.9	0.8	0.8	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.7	0.7	1.0
141.	*	0.9	0.8	0.8	0.8	0.8	0.7	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.7	0.6	0.7	0.7	0.9
142.	*	0.9	0.8	0.8	0.8	0.8	0.7	0.6	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.6	0.8	0.8	1.0
143.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.7	0.8	0.8	1.0
144.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.5	0.5	0.4	0.2	0.2	0.2	0.7	0.7	0.6	0.7	0.8	0.8	1.0
145.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.7	0.6	0.7	0.8	0.8	1.1

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

146.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.8	0.5	0.8	0.8	0.8	1.1
147.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.8	0.5	0.7	0.8	0.8	1.1
148.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.7	0.6	0.7	0.9	0.9	1.1
149.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.7	0.7	0.7	0.9	1.0	1.2
150.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.8	0.7	0.8	0.9	1.0	1.2
151.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.7	0.7	0.8	0.9	1.0	1.2
152.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.4	0.2	0.2	0.2	0.8	0.7	0.7	0.9	0.9	1.0	1.2
153.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.5	0.3	0.2	0.2	0.2	0.9	0.8	0.8	1.0	0.9	1.0	1.2
154.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.5	0.4	0.3	0.2	0.2	0.2	0.9	0.8	0.8	1.0	0.9	1.1	1.2
155.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.5	0.6	0.4	0.3	0.2	0.2	0.2	0.9	0.9	0.9	1.0	1.0	1.1	1.1
156.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.6	0.4	0.3	0.2	0.2	0.3	1.0	0.8	0.8	1.0	1.0	1.0	1.2
157.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.6	0.4	0.3	0.3	0.3	0.3	1.0	0.8	1.0	1.0	1.0	1.0	1.3
158.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.6	0.5	0.3	0.3	0.3	0.3	1.0	0.8	1.0	1.0	1.0	1.1	1.3
159.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.7	0.5	0.4	0.3	0.3	0.3	1.0	0.9	1.0	1.1	1.1	1.2	1.3
160.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.6	0.8	0.6	0.4	0.3	0.3	0.3	1.0	0.9	1.0	1.1	1.1	1.2	1.2
161.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.8	0.8	0.5	0.3	0.3	0.3	1.0	0.8	1.0	1.0	1.2	1.2	1.2
162.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.8	0.8	0.7	0.4	0.3	0.3	1.1	0.8	1.0	1.0	1.2	1.2	1.2
163.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.8	0.8	0.7	0.5	0.4	0.5	1.1	0.8	1.1	1.0	1.2	1.1	1.2
164.	*	0.8	0.8	0.8	0.8	0.8	0.7	0.7	0.8	0.8	0.7	0.6	0.6	0.5	1.1	0.8	1.1	1.2	1.1	1.2	1.2
165.	*	0.8	0.8	0.8	0.8	0.8	0.8	0.8	1.0	0.9	0.8	0.8	0.7	0.7	1.1	0.8	1.1	1.2	1.1	1.2	1.2
166.	*	0.8	0.8	0.8	0.8	0.8	0.8	0.8	1.0	0.9	0.9	0.8	0.7	0.7	1.1	0.9	1.1	1.1	1.1	1.2	1.2
167.	*	0.8	0.8	0.8	0.8	0.8	0.8	0.9	1.0	0.9	0.9	0.8	0.8	0.6	1.0	0.9	1.0	1.1	1.1	1.1	1.1
168.	*	0.8	0.8	0.8	0.8	0.9	0.9	0.9	1.1	0.9	0.9	0.8	0.7	0.7	0.9	0.9	0.9	1.0	1.0	1.0	1.1
169.	*	0.8	0.8	0.8	0.8	0.9	0.8	0.9	1.1	1.0	0.9	0.8	0.8	0.8	0.9	0.9	0.9	1.0	0.9	1.0	1.1
170.	*	0.8	0.8	0.8	0.8	0.9	0.8	1.0	1.3	1.0	0.9	0.8	0.8	0.8	0.9	0.9	0.9	0.9	0.9	1.0	1.1
171.	*	0.8	0.8	0.8	0.8	0.9	0.9	1.1	1.3	1.3	0.8	0.8	0.8	0.8	0.9	0.9	0.9	0.8	0.9	1.0	1.1
172.	*	0.8	0.8	0.8	0.9	0.9	0.9	1.1	1.3	1.2	1.0	0.8	0.8	0.9	0.9	0.9	0.9	0.8	0.9	1.0	1.1
173.	*	0.8	0.8	0.8	0.9	0.9	0.9	1.1	1.3	1.3	1.3	0.9	1.0	0.9	0.9	0.8	0.9	0.8	0.9	0.9	1.0
174.	*	0.8	0.8	0.8	0.9	0.9	1.0	1.2	1.4	1.3	1.3	1.1	1.0	1.0	0.9	0.7	0.9	0.8	0.9	0.9	1.0
175.	*	0.8	0.8	0.9	0.9	1.0	1.1	1.3	1.4	1.4	1.2	1.1	1.0	1.0	0.8	0.7	0.8	0.8	0.9	0.9	0.9
176.	*	0.8	0.8	0.9	0.9	1.0	1.1	1.3	1.5	1.4	1.2	1.3	1.0	1.1	0.8	0.7	0.7	0.7	0.9	0.9	0.9
177.	*	0.8	0.8	0.9	0.9	1.0	1.1	1.4	1.5	1.4	1.3	1.3	1.2	1.1	0.8	0.7	0.7	0.7	0.7	0.9	0.8
178.	*	0.8	0.9	0.9	1.0	1.1	1.1	1.4	1.6	1.5	1.3	1.3	1.2	1.1	0.7	0.7	0.7	0.7	0.7	0.6	0.8
179.	*	0.8	0.9	0.9	1.0	1.2	1.1	1.4	1.6	1.5	1.4	1.5	1.2	1.1	0.7	0.6	0.6	0.7	0.6	0.6	0.7
180.	*	0.8	0.9	0.9	1.0	1.2	1.2	1.4	1.6	1.5	1.4	1.5	1.3	1.2	0.7	0.6	0.6	0.7	0.5	0.6	0.7
181.	*	0.9	0.9	1.0	1.0	1.2	1.2	1.5	1.6	1.6	1.4	1.5	1.3	1.2	0.7	0.6	0.6	0.5	0.5	0.6	0.7

182.	*	0.9	0.9	1.0	1.1	1.2	1.3	1.5	1.6	1.7	1.4	1.5	1.2	1.3	0.7	0.6	0.5	0.4	0.5	0.5	0.7
183.	*	0.9	0.9	1.0	1.1	1.3	1.3	1.5	1.6	1.7	1.4	1.5	1.3	1.3	0.4	0.5	0.5	0.4	0.5	0.5	0.6
184.	*	0.9	1.0	1.0	1.1	1.2	1.3	1.5	1.7	1.7	1.5	1.5	1.3	1.3	0.4	0.4	0.4	0.4	0.4	0.5	0.6
185.	*	0.9	1.0	1.1	1.1	1.3	1.3	1.5	1.7	1.7	1.5	1.4	1.3	1.2	0.4	0.4	0.4	0.4	0.4	0.5	0.6
186.	*	0.9	1.0	1.1	1.1	1.3	1.3	1.5	1.8	1.7	1.4	1.4	1.3	1.2	0.4	0.3	0.3	0.4	0.4	0.4	0.5
187.	*	1.0	1.0	1.1	1.1	1.3	1.4	1.5	1.8	1.7	1.5	1.5	1.2	1.2	0.4	0.3	0.3	0.3	0.4	0.4	0.4
188.	*	1.0	1.0	1.1	1.2	1.3	1.4	1.5	1.8	1.6	1.5	1.5	1.2	1.3	0.3	0.2	0.2	0.2	0.2	0.3	0.4
189.	*	1.0	1.1	1.1	1.2	1.3	1.5	1.5	1.8	1.6	1.5	1.5	1.2	1.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4
190.	*	1.0	1.1	1.1	1.3	1.3	1.5	1.5	1.7	1.5	1.5	1.4	1.2	1.3	0.1	0.1	0.2	0.2	0.2	0.2	0.4
191.	*	1.0	1.1	1.1	1.4	1.3	1.5	1.5	1.7	1.4	1.5	1.3	1.2	1.3	0.1	0.1	0.1	0.2	0.2	0.2	0.3
192.	*	1.0	1.1	1.1	1.4	1.3	1.6	1.5	1.7	1.4	1.4	1.3	1.2	1.3	0.1	0.1	0.1	0.1	0.2	0.2	0.3
193.	*	1.1	1.1	1.1	1.4	1.2	1.6	1.5	1.7	1.4	1.4	1.3	1.2	1.3	0.1	0.1	0.1	0.1	0.1	0.2	0.3
194.	*	1.1	1.1	1.2	1.4	1.2	1.6	1.5	1.7	1.3	1.4	1.2	1.2	1.3	0.1	0.1	0.1	0.1	0.1	0.1	0.3
195.	*	1.1	1.1	1.2	1.4	1.2	1.6	1.5	1.7	1.4	1.3	1.2	1.2	1.2	0.1	0.1	0.1	0.1	0.1	0.1	0.3
196.	*	1.1	1.1	1.2	1.4	1.2	1.5	1.5	1.6	1.4	1.2	1.2	1.1	1.3	0.1	0.1	0.1	0.1	0.1	0.1	0.3
197.	*	1.1	1.1	1.4	1.4	1.3	1.5	1.5	1.6	1.4	1.3	1.1	1.1	1.3	0.1	0.1	0.1	0.1	0.1	0.1	0.3

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

198.	*	1.1	1.1	1.4	1.4	1.3	1.5	1.5	1.6	1.3	1.2	1.1	1.1	1.3	0.1	0.1	0.1	0.1	0.1	0.1	0.2
199.	*	1.1	1.2	1.4	1.4	1.4	1.5	1.6	1.5	1.3	1.2	1.0	1.1	1.2	0.0	0.0	0.0	0.1	0.1	0.1	0.2
200.	*	1.1	1.2	1.4	1.4	1.4	1.4	1.5	1.5	1.2	1.1	1.1	1.1	1.1	0.0	0.0	0.0	0.0	0.1	0.1	0.2
201.	*	1.1	1.2	1.4	1.3	1.4	1.4	1.5	1.2	1.1	1.1	1.1	1.2	1.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2
202.	*	1.1	1.2	1.4	1.2	1.4	1.3	1.4	1.2	1.1	1.1	1.1	1.1	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
203.	*	1.1	1.2	1.4	1.2	1.4	1.4	1.3	1.2	1.1	1.0	1.1	1.1	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
204.	*	1.1	1.4	1.3	1.2	1.4	1.4	1.4	1.3	1.1	1.0	1.1	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
205.	*	1.2	1.4	1.3	1.2	1.3	1.4	1.4	1.3	1.1	1.0	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
206.	*	1.2	1.3	1.3	1.2	1.3	1.3	1.4	1.3	1.1	1.1	1.1	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
207.	*	1.2	1.3	1.3	1.2	1.3	1.3	1.4	1.2	1.1	1.1	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
208.	*	1.2	1.3	1.3	1.2	1.3	1.3	1.4	1.2	1.1	1.1	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
209.	*	1.3	1.4	1.3	1.2	1.2	1.3	1.4	1.1	1.0	1.0	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
210.	*	1.4	1.4	1.3	1.2	1.2	1.3	1.4	1.1	0.9	1.0	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
211.	*	1.4	1.4	1.2	1.2	1.3	1.3	1.4	1.0	0.9	0.9	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2
212.	*	1.4	1.4	1.2	1.3	1.3	1.2	1.3	1.0	0.9	0.8	1.0	1.0	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2
213.	*	1.5	1.4	1.3	1.2	1.3	1.2	1.3	1.0	0.9	0.9	1.0	1.0	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2
214.	*	1.5	1.4	1.3	1.2	1.3	1.2	1.3	1.0	0.8	0.9	1.0	1.0	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2
215.	*	1.5	1.4	1.3	1.2	1.2	1.1	1.2	1.0	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2
216.	*	1.5	1.4	1.2	1.3	1.2	1.1	1.2	1.0	0.9	0.9	0.9	0.8	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.2
217.	*	1.5	1.4	1.2	1.3	1.3	1.1	1.2	0.9	0.9	0.9	0.9	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
218.	*	1.5	1.4	1.2	1.3	1.3	1.1	1.2	0.9	0.8	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
219.	*	1.5	1.4	1.2	1.3	1.3	1.1	1.2	0.9	0.8	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
220.	*	1.5	1.4	1.2	1.3	1.2	1.1	1.2	0.9	0.8	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
221.	*	1.5	1.4	1.2	1.3	1.2	1.1	1.3	0.9	0.8	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
222.	*	1.4	1.4	1.2	1.3	1.2	1.1	1.3	0.9	0.8	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
223.	*	1.4	1.3	1.2	1.3	1.2	1.1	1.3	0.9	0.9	0.9	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.2
224.	*	1.4	1.3	1.2	1.3	1.1	1.1	1.3	0.8	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
225.	*	1.4	1.3	1.2	1.3	1.0	1.1	1.3	0.8	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
226.	*	1.4	1.3	1.2	1.3	1.0	1.0	1.3	0.8	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
227.	*	1.3	1.3	1.2	1.3	1.0	1.0	1.1	0.7	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
228.	*	1.3	1.3	1.2	1.3	1.0	1.0	1.1	0.7	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
229.	*	1.3	1.3	1.2	1.3	1.0	1.0	1.1	0.8	0.9	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
230.	*	1.2	1.3	1.2	1.2	1.0	1.0	1.1	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
231.	*	1.2	1.3	1.2	1.1	1.0	1.0	1.0	0.8	0.7	0.7	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.3
232.	*	1.2	1.3	1.2	1.0	1.0	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
233.	*	1.2	1.3	1.2	1.0	1.0	1.1	1.0	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3

234.	*	1.2	1.3	1.2	1.0	1.0	1.1	1.0	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
235.	*	1.2	1.3	1.1	1.0	0.9	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
236.	*	1.2	1.3	1.1	1.0	0.9	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
237.	*	1.2	1.2	1.1	1.0	0.9	1.0	1.1	0.9	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
238.	*	1.2	1.1	1.1	1.0	0.9	1.0	1.1	0.9	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
239.	*	1.1	1.1	1.1	1.0	0.9	1.0	1.1	0.9	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
240.	*	1.1	1.1	1.1	1.0	0.8	1.0	1.0	0.9	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
241.	*	1.1	1.1	1.0	1.0	0.9	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
242.	*	1.1	1.1	0.9	1.0	0.9	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
243.	*	1.1	1.1	0.9	1.0	0.9	0.9	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
244.	*	1.1	1.1	0.9	1.0	0.9	0.9	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
245.	*	1.1	1.1	0.9	1.0	0.9	0.9	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
246.	*	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.3
247.	*	1.1	0.9	1.0	1.0	0.9	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
248.	*	1.1	0.9	1.0	1.0	0.9	0.8	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
249.	*	1.1	1.0	1.0	1.0	0.9	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

250.	*	1.1	1.0	1.0	1.0	0.9	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
251.	*	1.1	1.0	1.0	1.0	0.9	0.9	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
252.	*	0.9	0.9	1.0	1.0	0.9	0.9	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
253.	*	0.9	0.9	1.0	1.0	0.9	0.9	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
254.	*	0.9	0.9	1.0	1.0	0.8	0.8	1.0	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
255.	*	0.9	1.0	0.9	0.9	0.7	0.7	1.0	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
256.	*	0.9	0.9	0.9	0.9	0.7	0.7	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
257.	*	0.9	0.9	0.9	0.9	0.6	0.7	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
258.	*	0.9	0.9	0.9	0.8	0.6	0.7	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
259.	*	0.8	0.8	0.8	0.7	0.6	0.4	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
260.	*	0.8	0.8	0.8	0.7	0.7	0.4	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
261.	*	0.8	0.8	0.8	0.6	0.5	0.4	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.2
262.	*	0.8	0.8	0.7	0.4	0.5	0.4	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1
263.	*	0.7	0.7	0.7	0.4	0.5	0.4	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.1
264.	*	0.7	0.7	0.5	0.4	0.5	0.4	0.9	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
265.	*	0.7	0.6	0.5	0.4	0.4	0.5	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
266.	*	0.7	0.6	0.4	0.4	0.4	0.5	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
267.	*	0.6	0.4	0.4	0.4	0.4	0.5	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
268.	*	0.5	0.4	0.4	0.4	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0

269.	*	0.5	0.4	0.4	0.3	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
270.	*	0.4	0.3	0.3	0.3	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
271.	*	0.3	0.3	0.2	0.3	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
272.	*	0.3	0.3	0.2	0.3	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
273.	*	0.3	0.2	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
274.	*	0.2	0.2	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
275.	*	0.2	0.2	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
276.	*	0.2	0.2	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
277.	*	0.1	0.2	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
278.	*	0.1	0.1	0.2	0.3	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
279.	*	0.1	0.1	0.2	0.2	0.3	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
280.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
281.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
282.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
283.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
284.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
285.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
286.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
287.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
288.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
289.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
290.	*	0.1	0.1	0.2	0.2	0.2	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
291.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
292.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
293.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
294.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
295.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
296.	*	0.1	0.1	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
297.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
298.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
299.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.6	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
300.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
301.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

302.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
303.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0

304.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
305.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
306.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
307.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
308.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
309.	*	0.1	0.2	0.2	0.2	0.2	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
310.	*	0.1	0.2	0.2	0.2	0.3	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
311.	*	0.1	0.2	0.2	0.2	0.3	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
312.	*	0.1	0.2	0.2	0.2	0.3	0.4	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
313.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
314.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
315.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
316.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
317.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0
318.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
319.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
320.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
321.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
322.	*	0.1	0.2	0.2	0.2	0.3	0.4	0.7	0.9	0.9	0.9	0.9	0.9	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
323.	*	0.1	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
324.	*	0.2	0.2	0.2	0.2	0.3	0.5	0.7	0.9	0.9	0.9	0.9	0.9	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
325.	*	0.2	0.3	0.2	0.2	0.3	0.5	0.8	0.9	0.9	0.9	0.9	0.9	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
326.	*	0.2	0.3	0.2	0.2	0.3	0.5	0.8	0.9	0.9	0.9	0.9	0.9	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
327.	*	0.2	0.3	0.3	0.2	0.3	0.5	0.8	0.9	0.9	0.9	0.9	0.9	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
328.	*	0.2	0.3	0.3	0.2	0.3	0.5	0.8	0.9	0.9	0.9	0.9	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
329.	*	0.2	0.3	0.3	0.2	0.3	0.5	0.8	1.0	1.0	1.0	1.0	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
330.	*	0.2	0.3	0.3	0.3	0.3	0.4	0.8	1.0	1.0	1.0	1.0	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
331.	*	0.2	0.3	0.3	0.3	0.3	0.4	0.8	1.0	1.0	1.0	1.1	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
332.	*	0.2	0.3	0.3	0.3	0.4	0.4	0.8	1.0	1.0	1.0	1.1	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
333.	*	0.2	0.3	0.3	0.3	0.4	0.4	0.8	1.0	1.0	1.0	1.1	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
334.	*	0.2	0.3	0.3	0.3	0.4	0.4	0.8	1.0	1.0	1.1	1.1	1.1	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
335.	*	0.2	0.3	0.3	0.3	0.4	0.5	0.8	1.0	1.0	1.1	1.1	1.1	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
336.	*	0.2	0.3	0.3	0.3	0.4	0.5	0.8	1.0	1.0	1.1	1.1	1.1	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
337.	*	0.2	0.2	0.3	0.3	0.4	0.5	0.8	1.0	1.1	1.1	1.1	1.1	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0
338.	*	0.2	0.2	0.3	0.3	0.4	0.5	0.9	1.2	1.2	1.2	1.2	1.2	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
339.	*	0.1	0.2	0.3	0.3	0.4	0.5	1.0	1.2	1.2	1.2	1.2	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
340.	*	0.1	0.2	0.3	0.3	0.4	0.5	1.0	1.2	1.2	1.2	1.2	1.1	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
341.	*	0.1	0.2	0.3	0.3	0.4	0.5	0.9	1.2	1.2	1.2	1.2	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
342.	*	0.1	0.2	0.3	0.3	0.4	0.5	0.9	1.2	1.2	1.2	1.1	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
343.	*	0.1	0.1	0.2	0.3	0.4	0.5	0.8	1.2	1.2	1.1	1.0	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
344.	*	0.1	0.1	0.2	0.3	0.4	0.5	0.7	1.2	1.2	1.1	1.0	1.0	1.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
345.	*	0.1	0.1	0.2	0.3	0.3	0.5	0.7	1.2	1.1	1.1	1.0	1.0	1.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0
346.	*	0.1	0.1	0.2	0.3	0.3	0.4	0.7	1.1	1.1	1.0	1.0	1.0	1.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0
347.	*	0.1	0.1	0.1	0.3	0.3	0.4	0.7	1.1	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.0	0.0	0.0	0.0	0.0
348.	*	0.1	0.1	0.1	0.3	0.3	0.4	0.7	1.1	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.1	0.1	0.1	0.0
349.	*	0.1	0.1	0.1	0.2	0.3	0.4	0.7	1.0	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.2	0.1	0.1	0.0
350.	*	0.0	0.1	0.1	0.2	0.3	0.4	0.7	1.0	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.2	0.2	0.1	0.1

351.	*	0.0	0.1	0.1	0.1	0.3	0.4	0.7	1.0	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.2	0.2	0.2	0.1
352.	*	0.0	0.1	0.1	0.1	0.3	0.4	0.6	1.0	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.2	0.2	0.2	0.1
353.	*	0.0	0.0	0.1	0.1	0.3	0.4	0.6	1.0	1.0	1.0	1.0	1.0	1.1	0.2	0.2	0.2	0.2	0.2	0.2	0.1

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC1 REC2 REC3 REC4 REC5 REC6 REC7 REC8 REC9 REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40
REC41 REC42 REC43 REC44 REC45 REC46 REC47 REC48 REC49 REC50 REC51 REC52

354.	*	0.0	0.0	0.1	0.1	0.3	0.4	0.6	1.0	1.0	1.0	1.0	1.0	1.0	0.2	0.2	0.2	0.2	0.2	0.2	0.2
355.	*	0.0	0.0	0.1	0.1	0.1	0.3	0.6	1.0	1.0	1.0	1.0	1.0	0.9	0.3	0.2	0.2	0.2	0.2	0.3	0.2
356.	*	0.0	0.0	0.1	0.1	0.1	0.3	0.6	0.9	0.9	0.9	0.9	0.9	0.9	0.3	0.3	0.3	0.2	0.2	0.3	0.2
357.	*	0.0	0.0	0.0	0.1	0.1	0.3	0.5	0.9	0.9	0.9	0.9	0.9	0.9	0.3	0.3	0.3	0.3	0.3	0.4	0.2
358.	*	0.0	0.0	0.0	0.1	0.1	0.3	0.5	0.9	0.9	0.9	0.9	0.9	0.9	0.4	0.3	0.3	0.3	0.4	0.4	0.2
359.	*	0.0	0.0	0.0	0.1	0.1	0.2	0.5	0.9	0.9	0.9	0.9	0.8	0.8	0.4	0.3	0.3	0.4	0.4	0.5	0.3
360.	*	0.0	0.0	0.0	0.0	0.1	0.2	0.5	0.8	0.8	0.8	0.8	0.8	0.8	0.4	0.3	0.4	0.4	0.4	0.5	0.3
MAX	*	1.5	1.4	1.4	1.4	1.4	1.6	1.6	1.8	1.7	1.5	1.5	1.3	1.3	1.1	0.9	1.1	1.2	1.2	1.2	1.3
DEGR.	*	213	204	197	191	199	192	199	186	184	184	179	180	192	162	155	163	164	161	159	157

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

MODEL RESULTS

REMARKS : In search of the angle corresponding to
the maximum concentration, only the first
angle, of the angles with same maximum
concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND * CONCENTRATION
ANGLE * (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28 REC29 REC30 REC31 REC32 REC33 REC34 REC35 REC36 REC37 REC38 REC39 REC40

0.	*	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.5	0.5	0.4	0.4	0.4	0.4	1.1
1.	*	0.2	0.2	0.1	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.3	0.4	0.5	0.5	0.4	0.4	0.4	0.5	1.1
2.	*	0.2	0.2	0.1	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.3	0.4	0.6	0.5	0.6	0.4	0.5	0.5	1.0
3.	*	0.2	0.2	0.1	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.3	0.4	0.6	0.7	0.6	0.4	0.5	0.5	1.1

4.	*	0.2	0.2	0.1	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.6	0.7	0.6	0.5	0.5	0.5	0.9
5.	*	0.3	0.2	0.2	0.1	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.6	0.7	0.7	0.5	0.5	0.5	0.9
6.	*	0.3	0.2	0.2	0.1	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.4	0.4	0.6	0.7	0.6	0.6	0.5	0.6	0.8
7.	*	0.3	0.2	0.2	0.1	0.0	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.6	0.6	0.6	0.8
8.	*	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.5	0.7	0.7	0.7	0.6	0.6	0.6	0.7
9.	*	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.3	0.4	0.4	0.4	0.5	0.8	0.6	0.7	0.6	0.6	0.7	0.7
10.	*	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.4	0.5	0.7	0.8	0.7	0.6	0.6	0.7	0.6
11.	*	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.4	0.5	0.7	0.8	0.7	0.6	0.7	0.8	0.6
12.	*	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.5	0.5	0.7	0.8	0.7	0.6	0.7	0.8	0.6
13.	*	0.3	0.3	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.4	0.4	0.5	0.5	0.7	0.8	0.8	0.6	0.8	0.8	0.6
14.	*	0.4	0.3	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.4	0.3	0.5	0.5	0.7	0.8	0.8	0.7	0.8	0.8	0.5
15.	*	0.4	0.3	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.4	0.3	0.5	0.5	0.7	0.8	0.8	0.7	0.8	0.8	0.5
16.	*	0.4	0.3	0.2	0.2	0.2	0.1	0.1	0.2	0.3	0.4	0.3	0.5	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.4
17.	*	0.5	0.3	0.3	0.2	0.2	0.1	0.1	0.2	0.3	0.4	0.3	0.5	0.6	0.8	0.9	0.6	0.8	0.8	0.8	0.4
18.	*	0.5	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.3	0.4	0.4	0.5	0.5	0.8	0.8	0.7	0.8	0.8	0.7	0.4
19.	*	0.5	0.3	0.3	0.2	0.2	0.2	0.2	0.1	0.2	0.4	0.4	0.5	0.5	0.8	0.8	0.7	0.8	0.8	0.7	0.3
20.	*	0.4	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.5	0.4	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.3
21.	*	0.4	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.5	0.4	0.6	0.8	0.8	0.8	0.8	0.7	0.8	0.3
22.	*	0.4	0.3	0.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.4	0.6	0.7	0.6	0.8	0.8	0.7	0.8	0.3
23.	*	0.4	0.2	0.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.4	0.6	0.7	0.7	0.8	0.8	0.7	0.8	0.2
24.	*	0.4	0.2	0.3	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.4	0.6	0.7	0.7	0.8	0.7	0.8	0.8	0.2
25.	*	0.4	0.2	0.3	0.3	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.4	0.6	0.8	0.7	0.8	0.7	0.8	0.9	0.2
26.	*	0.4	0.3	0.2	0.3	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.8	0.7	0.8	0.7	0.8	0.9	0.2
27.	*	0.4	0.3	0.2	0.3	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.7	0.7	0.8	0.9	0.2
28.	*	0.4	0.3	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.7	0.7	0.9	0.9	0.2
29.	*	0.4	0.3	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.6	0.8	0.7	0.7	0.9	0.9	0.2
30.	*	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.8	0.7	0.7	0.9	1.0	0.2
31.	*	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.7	0.7	0.9	1.0	0.2
32.	*	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.7	0.8	0.9	1.0	0.2
33.	*	0.4	0.4	0.2	0.2	0.1	0.1	0.2	0.2	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.7	0.8	0.9	1.0	0.2
34.	*	0.4	0.4	0.2	0.2	0.1	0.1	0.1	0.2	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.7	0.8	0.9	1.0	0.2
35.	*	0.4	0.4	0.2	0.2	0.1	0.2	0.1	0.2	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.7	0.8	1.0	1.0	0.2
36.	*	0.4	0.4	0.2	0.2	0.1	0.2	0.1	0.2	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.8	0.8	0.9	1.1	0.2
37.	*	0.4	0.4	0.2	0.2	0.1	0.2	0.1	0.2	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.8	0.7	0.9	1.1	0.2
38.	*	0.4	0.4	0.2	0.2	0.1	0.2	0.1	0.1	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.8	0.7	1.0	1.0	0.2
39.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.1	0.1	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.8	0.8	1.0	1.0	0.2
40.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.1	0.1	0.3	0.4	0.4	0.6	0.6	0.7	0.7	0.8	0.8	1.0	1.0	0.2
41.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.4	0.4	0.6	0.6	0.7	0.7	0.7	0.8	1.0	1.0	0.2

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40

42.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.4	0.4	0.6	0.6	0.7	0.8	0.7	1.0	1.0	1.0	0.2
43.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.7	0.8	0.8	1.0	1.0	1.0	0.2
44.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.7	0.8	0.8	1.0	1.0	1.0	0.2
45.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.7	0.9	0.8	1.0	1.0	1.0	0.2
46.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.7	0.8	0.9	1.0	1.0	1.0	0.2
47.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.9	0.9	0.9	1.0	1.0	1.0	0.2
48.	*	0.4	0.4	0.2	0.1	0.1	0.2	0.2	0.1	0.2	0.3	0.4	0.6	0.6	0.9	0.9	1.0	1.0	1.0	1.0	0.2
49.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.2	0.2	0.2	0.3	0.3	0.6	0.6	0.9	0.9	1.1	1.0	1.0	1.0	0.2
50.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.2	0.2	0.2	0.3	0.3	0.5	0.6	0.9	0.9	1.1	1.0	1.0	0.9	0.2
51.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.2	0.2	0.2	0.3	0.3	0.5	0.6	1.0	1.0	1.1	1.0	1.0	0.9	0.2
52.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.2	0.2	0.2	0.3	0.3	0.5	0.6	1.0	1.0	1.0	1.0	0.9	0.9	0.2
53.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.2	0.2	0.2	0.3	0.3	0.5	0.6	0.9	1.0	0.9	0.9	0.9	0.9	0.2
54.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.3	0.2	0.2	0.3	0.3	0.5	0.6	0.9	1.0	0.9	0.9	0.9	1.0	0.2
55.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.3	0.2	0.2	0.3	0.3	0.5	0.6	0.9	1.0	0.9	0.9	1.0	1.0	0.2
56.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.3	0.2	0.2	0.3	0.3	0.4	0.6	1.0	1.0	0.9	0.9	1.0	1.0	0.2
57.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.3	0.2	0.3	0.3	0.3	0.3	0.6	1.0	1.0	0.9	1.0	1.0	1.0	0.2
58.	*	0.4	0.4	0.2	0.1	0.1	0.3	0.3	0.2	0.3	0.3	0.3	0.3	0.5	1.0	1.0	0.9	1.0	1.0	1.0	0.2
59.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.4	0.2	0.3	0.3	0.3	0.3	0.5	1.0	1.1	1.0	1.0	1.0	1.0	0.2
60.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.4	1.0	1.0	1.0	1.0	1.0	1.0	0.2
61.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.4	1.0	1.0	1.0	1.0	1.0	1.0	0.2
62.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.3	1.0	1.1	1.0	1.0	1.0	1.0	0.2
63.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.5	1.0	1.1	1.0	1.0	1.0	1.0	0.2
64.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.5	1.1	1.0	1.0	1.0	1.0	1.0	0.2
65.	*	0.4	0.4	0.2	0.1	0.1	0.4	0.4	0.3	0.3	0.3	0.3	0.3	0.5	1.1	1.0	1.0	1.0	1.0	1.0	0.2
66.	*	0.4	0.4	0.1	0.1	0.1	0.5	0.4	0.4	0.3	0.3	0.3	0.4	0.5	1.1	1.1	1.1	1.0	1.0	1.0	0.2
67.	*	0.4	0.4	0.1	0.1	0.1	0.5	0.5	0.4	0.4	0.5	0.4	0.4	0.5	1.1	1.1	1.1	1.0	1.0	1.0	0.2
68.	*	0.4	0.4	0.1	0.1	0.1	0.5	0.5	0.4	0.4	0.5	0.4	0.5	0.6	1.1	1.1	1.1	1.0	1.0	1.0	0.2
69.	*	0.4	0.4	0.1	0.1	0.1	0.5	0.5	0.5	0.5	0.5	0.4	0.5	0.6	1.2	1.1	1.1	1.0	1.0	1.0	0.2
70.	*	0.4	0.3	0.1	0.1	0.1	0.5	0.5	0.5	0.5	0.5	0.4	0.5	0.7	1.3	1.1	1.1	1.0	1.0	1.0	0.2
71.	*	0.4	0.3	0.1	0.1	0.1	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.8	1.3	1.1	1.1	1.0	1.0	1.0	0.2
72.	*	0.4	0.3	0.1	0.1	0.1	0.6	0.5	0.5	0.5	0.6	0.5	0.6	1.0	1.3	1.1	1.1	1.0	1.0	1.0	0.2
73.	*	0.4	0.3	0.1	0.1	0.1	0.6	0.5	0.5	0.5	0.7	0.5	0.8	1.0	1.2	1.1	1.1	1.0	1.0	1.0	0.1
74.	*	0.4	0.3	0.1	0.1	0.1	0.6	0.5	0.5	0.5	0.8	0.7	0.9	1.0	1.2	1.1	1.1	1.0	1.0	1.0	0.1
75.	*	0.4	0.3	0.1	0.1	0.1	0.6	0.5	0.5	0.6	0.8	0.7	1.0	1.0	1.2	1.1	1.1	1.0	1.0	1.0	0.1
76.	*	0.5	0.3	0.1	0.1	0.1	0.6	0.5	0.5	0.6	0.8	0.7	1.0	1.0	1.2	1.1	1.0	1.0	1.0	0.9	0.0
77.	*	0.5	0.4	0.1	0.1	0.1	0.6	0.5	0.5	0.5	0.7	0.8	1.0	1.1	1.2	1.1	1.0	1.0	1.0	0.9	0.0
78.	*	0.5	0.3	0.2	0.1	0.1	0.6	0.5	0.5	0.5	0.6	0.9	1.0	1.1	1.2	1.1	1.0	1.0	1.0	0.9	0.0
79.	*	0.5	0.3	0.2	0.3	0.2	0.6	0.6	0.5	0.5	0.6	1.0	1.0	1.1	1.2	1.1	1.0	1.0	0.9	0.9	0.0
80.	*	0.6	0.4	0.2	0.3	0.3	0.6	0.6	0.5	0.5	0.6	1.0	1.0	1.1	1.2	1.1	1.0	1.0	0.9	0.9	0.0
81.	*	0.7	0.4	0.4	0.4	0.4	0.6	0.6	0.5	0.5	0.6	1.0	1.0	1.0	1.2	1.1	1.0	0.9	0.9	0.8	0.0
82.	*	0.7	0.4	0.4	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.9	0.9	1.0	1.2	1.1	1.0	0.9	0.9	0.8	0.0
83.	*	0.7	0.5	0.4	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.9	1.0	1.0	1.2	1.0	1.0	0.9	0.9	0.8	0.0
84.	*	0.8	0.6	0.4	0.4	0.4	0.5	0.6	0.5	0.5	0.6	0.9	1.0	1.0	1.2	1.0	0.9	0.9	0.8	0.8	0.0
85.	*	0.8	0.6	0.4	0.4	0.4	0.5	0.6	0.6	0.5	0.6	0.8	1.0	1.1	1.2	1.0	0.9	0.9	0.8	0.8	0.0
86.	*	0.7	0.8	0.5	0.5	0.5	0.5	0.5	0.6	0.5	0.6	0.8	1.0	1.1	1.2	1.0	0.9	0.9	0.8	0.8	0.0
87.	*	0.8	0.7	0.6	0.5	0.5	0.5	0.5	0.6	0.5	0.6	0.8	1.0	1.1	1.2	0.9	0.9	0.8	0.8	0.8	0.0

88.	*	0.8	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.8	0.9	1.1	1.2	0.9	0.9	0.8	0.8	0.8	0.0
89.	*	0.9	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.8	0.9	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.0
90.	*	0.9	0.7	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.8	0.8	1.1	1.0	0.9	0.9	0.8	0.8	0.8	0.0
91.	*	0.9	0.7	0.7	0.6	0.6	0.5	0.5	0.5	0.5	0.6	0.7	0.7	1.0	1.0	0.9	0.8	0.8	0.8	0.8	0.0
92.	*	0.9	0.7	0.7	0.6	0.6	0.4	0.5	0.5	0.5	0.6	0.7	0.7	1.0	1.0	0.9	0.8	0.8	0.8	0.8	0.0

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
93.	*	0.9	0.7	0.8	0.6	0.6	0.4	0.5	0.5	0.5	0.5	0.7	0.7	1.0	1.0	0.9	0.8	0.8	0.8	0.8	0.0
94.	*	0.9	0.8	0.9	0.7	0.6	0.4	0.5	0.5	0.5	0.5	0.6	0.7	0.8	1.0	0.9	0.8	0.8	0.8	0.8	0.0
95.	*	1.0	0.9	0.9	0.7	0.6	0.4	0.4	0.5	0.5	0.5	0.6	0.6	0.8	1.0	0.8	0.8	0.8	0.8	0.9	0.0
96.	*	1.0	0.9	0.9	0.6	0.6	0.4	0.4	0.5	0.5	0.5	0.6	0.6	0.7	1.0	0.8	0.8	0.8	0.8	0.9	0.0
97.	*	1.2	1.0	0.9	0.6	0.5	0.4	0.4	0.5	0.5	0.5	0.6	0.5	0.6	1.0	0.8	0.8	0.8	0.8	0.9	0.0
98.	*	1.1	1.0	0.8	0.5	0.5	0.4	0.4	0.4	0.5	0.6	0.6	0.5	0.6	0.9	0.8	0.8	0.8	0.8	0.8	0.0
99.	*	1.2	1.0	0.6	0.6	0.5	0.4	0.4	0.4	0.5	0.5	0.5	0.5	0.7	0.9	0.8	0.8	0.8	0.8	0.8	0.0
100.	*	1.2	0.9	0.6	0.6	0.5	0.4	0.4	0.4	0.5	0.5	0.5	0.6	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0
101.	*	1.1	0.8	0.6	0.6	0.6	0.4	0.4	0.4	0.5	0.5	0.6	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0
102.	*	1.1	0.8	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0
103.	*	1.0	0.7	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0
104.	*	1.0	0.6	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.7	0.8	0.8	0.8	0.8	0.8	0.8	0.0
105.	*	1.0	0.6	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.6	0.7	0.8	0.9	0.8	0.8	0.8	0.8	0.8	0.0
106.	*	0.9	0.6	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.6	0.7	0.8	0.9	0.8	0.8	0.8	0.9	0.8	0.0
107.	*	0.8	0.6	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.6	0.7	0.8	0.9	0.8	0.8	0.8	0.9	0.8	0.0
108.	*	0.7	0.6	0.6	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.7	0.8	0.9	0.8	0.8	0.8	0.9	0.8	0.0
109.	*	0.7	0.6	0.6	0.6	0.6	0.5	0.4	0.4	0.4	0.4	0.5	0.6	0.8	0.9	0.8	0.8	0.8	0.9	0.9	0.0
110.	*	0.7	0.7	0.7	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.5	0.6	0.8	0.9	0.8	0.8	0.8	0.8	0.9	0.0
111.	*	0.6	0.7	0.7	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.8	0.8	0.9	0.0
112.	*	0.6	0.7	0.7	0.7	0.5	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.8	0.8	0.9	0.0
113.	*	0.7	0.7	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.8	0.8	0.8	0.0
114.	*	0.7	0.7	0.7	0.7	0.5	0.4	0.5	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.9	0.8	0.8	0.0
115.	*	0.7	0.7	0.8	0.7	0.6	0.4	0.5	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.9	0.8	0.8	0.0
116.	*	0.7	0.8	0.7	0.6	0.6	0.4	0.5	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.9	0.8	0.8	0.0
117.	*	0.9	0.8	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	0.9	0.8	0.8	0.9	0.8	0.8	0.0
118.	*	0.9	0.8	0.7	0.6	0.6	0.4	0.4	0.5	0.4	0.4	0.5	0.6	0.6	0.9	0.8	0.8	0.9	0.8	0.8	0.0
119.	*	0.9	0.7	0.6	0.6	0.6	0.4	0.4	0.5	0.4	0.4	0.5	0.6	0.6	0.9	0.8	0.8	0.9	0.9	0.8	0.0
120.	*	0.9	0.7	0.6	0.6	0.6	0.4	0.4	0.5	0.4	0.4	0.5	0.6	0.6	0.9	0.8	0.8	0.9	0.9	0.7	0.0
121.	*	0.9	0.7	0.6	0.6	0.6	0.3	0.4	0.5	0.4	0.4	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.9	0.8	0.0
122.	*	0.9	0.7	0.6	0.6	0.6	0.3	0.4	0.4	0.5	0.4	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.9	0.8	0.0
123.	*	0.8	0.6	0.6	0.6	0.6	0.3	0.4	0.4	0.5	0.4	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.9	0.8	0.0
124.	*	0.8	0.6	0.6	0.6	0.6	0.3	0.4	0.4	0.5	0.4	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.9	0.8	0.0

125.	*	0.8	0.7	0.6	0.6	0.6	0.3	0.4	0.4	0.5	0.5	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.8	0.8	0.0
126.	*	0.8	0.7	0.6	0.6	0.6	0.4	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.9	0.8	0.9	0.8	0.8	0.8	0.0
127.	*	0.9	0.8	0.6	0.6	0.6	0.4	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.9	0.9	0.9	0.9	0.8	0.8	0.0
128.	*	0.8	0.8	0.6	0.6	0.5	0.4	0.3	0.4	0.4	0.5	0.5	0.6	0.6	0.9	0.9	0.9	0.9	0.8	0.8	0.0
129.	*	0.8	0.8	0.6	0.6	0.5	0.4	0.3	0.4	0.4	0.4	0.6	0.6	0.6	0.8	0.9	0.9	0.9	0.9	0.8	0.0
130.	*	0.8	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.7	0.6	0.6	0.8	0.9	0.8	0.9	0.9	0.8	0.0
131.	*	0.8	0.8	0.7	0.6	0.5	0.4	0.4	0.3	0.4	0.4	0.7	0.6	0.7	0.9	0.9	0.8	0.9	0.9	0.8	0.0
132.	*	0.8	0.8	0.7	0.7	0.5	0.4	0.4	0.3	0.4	0.4	0.7	0.7	0.7	0.9	0.9	0.8	0.9	0.8	0.8	0.0
133.	*	0.8	0.8	0.7	0.7	0.5	0.4	0.4	0.3	0.4	0.4	0.7	0.7	0.7	0.9	0.9	0.8	0.9	0.8	0.8	0.0
134.	*	0.8	0.7	0.7	0.7	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.6	0.6	1.0	1.0	1.0	0.9	0.9	0.8	0.0
135.	*	0.8	0.7	0.8	0.6	0.5	0.4	0.4	0.4	0.3	0.4	0.6	0.6	0.7	1.0	1.0	1.0	0.9	0.9	1.0	0.0
136.	*	0.8	0.7	0.8	0.6	0.5	0.4	0.4	0.4	0.3	0.4	0.6	0.6	0.7	1.0	0.9	1.0	0.9	0.9	1.0	0.0
137.	*	0.8	0.7	0.8	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.6	0.7	1.0	0.9	1.0	1.0	0.9	1.0	0.0
138.	*	0.9	0.8	0.8	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.6	0.7	1.0	0.9	1.0	1.0	0.9	1.0	0.0
139.	*	0.9	0.8	0.8	0.6	0.5	0.4	0.4	0.4	0.4	0.3	0.6	0.6	0.7	1.0	1.0	1.0	1.0	0.9	1.0	0.0
140.	*	0.9	0.8	0.8	0.6	0.5	0.4	0.4	0.4	0.4	0.3	0.6	0.5	0.7	1.0	1.0	1.0	1.0	0.9	1.0	0.0
141.	*	0.9	0.8	0.8	0.6	0.4	0.4	0.4	0.4	0.4	0.4	0.6	0.5	0.7	1.0	1.0	0.9	0.9	0.9	1.0	0.0
142.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.5	0.7	0.9	1.0	0.9	0.9	0.9	1.0	0.0
143.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.7	0.5	0.7	1.0	1.0	1.0	0.9	1.0	1.0	0.0

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
144.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.5	0.7	1.0	1.0	1.0	0.9	1.0	1.0	0.0
145.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.6	0.6	0.7	1.0	1.0	1.0	0.9	1.0	1.0	0.0
146.	*	1.0	0.8	0.7	0.5	0.5	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	1.0	0.9	1.0	0.9	1.0	1.0	0.0
147.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	1.0	0.9	1.0	0.9	1.0	1.0	0.0
148.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.6	0.7	1.0	1.0	0.9	0.9	1.0	1.0	0.0
149.	*	0.9	0.8	0.8	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	1.0	1.0	0.9	1.0	1.0	1.0	0.1
150.	*	0.9	0.8	0.8	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	0.9	1.0	0.9	1.0	1.0	1.0	0.1
151.	*	1.0	0.9	0.8	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	0.9	1.0	0.9	1.0	1.0	1.0	0.1
152.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	1.1	1.1	1.0	1.0	1.0	1.0	0.1
153.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	1.1	1.1	1.0	1.1	1.1	1.0	0.1
154.	*	1.1	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.7	1.1	1.0	1.0	1.1	1.1	1.1	0.1
155.	*	1.1	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.6	1.1	1.0	1.0	1.1	1.1	1.1	0.1
156.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.6	1.1	1.0	1.1	1.1	1.1	1.1	0.2
157.	*	1.0	0.9	0.7	0.6	0.6	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.6	1.1	1.0	1.1	1.1	1.1	1.1	0.2
158.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.5	0.5	0.6	1.0	1.0	1.1	1.1	1.1	1.1	0.2
159.	*	1.0	0.8	0.7	0.6	0.5	0.4	0.4	0.4	0.4	0.4	0.4	0.5	0.6	1.0	1.0	1.1	1.1	1.1	1.1	0.2
160.	*	1.0	0.8	0.7	0.6	0.5	0.3	0.4	0.4	0.4	0.4	0.4	0.5	0.6	1.0	1.0	1.1	1.1	1.1	1.1	0.3
161.	*	1.0	0.7	0.7	0.6	0.5	0.3	0.3	0.3	0.4	0.4	0.4	0.5	0.6	1.0	1.0	1.0	1.1	1.1	1.1	0.3

162.	*	1.0	0.7	0.7	0.5	0.5	0.3	0.3	0.3	0.3	0.3	0.4	0.5	0.6	1.0	1.0	1.0	1.0	1.0	1.0	0.3
163.	*	1.0	0.7	0.6	0.5	0.4	0.3	0.3	0.3	0.3	0.3	0.4	0.5	0.6	1.0	1.0	1.0	1.0	1.0	0.9	0.3
164.	*	1.0	0.7	0.6	0.5	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.5	0.6	1.0	1.0	1.0	1.0	0.9	0.9	0.4
165.	*	0.9	0.7	0.6	0.5	0.4	0.3	0.3	0.3	0.3	0.3	0.3	0.5	0.6	1.0	0.9	0.9	0.9	0.9	0.9	0.5
166.	*	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.3	0.3	0.3	0.3	0.5	0.5	0.9	0.9	0.9	0.9	0.9	0.9	0.6
167.	*	0.8	0.7	0.5	0.5	0.4	0.2	0.2	0.2	0.2	0.3	0.3	0.4	0.5	0.9	0.9	0.9	0.9	0.9	0.9	0.6
168.	*	0.8	0.7	0.5	0.4	0.4	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.5	0.9	0.9	0.9	0.9	0.9	0.9	0.7
169.	*	0.8	0.7	0.5	0.4	0.4	0.2	0.2	0.2	0.2	0.2	0.3	0.3	0.5	0.9	0.9	0.9	0.9	0.9	0.8	0.8
170.	*	0.8	0.6	0.5	0.4	0.4	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.5	0.8	0.8	0.8	0.8	0.7	0.7	0.8
171.	*	0.8	0.5	0.5	0.4	0.4	0.2	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.8	0.7	0.7	0.7	0.7	0.7	0.9
172.	*	0.8	0.5	0.4	0.4	0.3	0.1	0.2	0.2	0.2	0.2	0.2	0.3	0.4	0.7	0.7	0.7	0.7	0.7	0.7	0.9
173.	*	0.6	0.5	0.4	0.5	0.3	0.1	0.1	0.1	0.2	0.2	0.2	0.3	0.3	0.7	0.7	0.7	0.7	0.7	0.7	0.9
174.	*	0.6	0.5	0.4	0.4	0.3	0.1	0.1	0.1	0.1	0.1	0.2	0.2	0.3	0.7	0.7	0.7	0.7	0.7	0.6	1.1
175.	*	0.6	0.5	0.4	0.4	0.2	0.1	0.1	0.1	0.1	0.1	0.2	0.2	0.3	0.7	0.6	0.6	0.6	0.6	0.6	1.1
176.	*	0.6	0.5	0.4	0.4	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.3	0.6	0.6	0.6	0.6	0.5	0.5	1.3
177.	*	0.6	0.4	0.3	0.4	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.3	0.5	0.5	0.5	0.5	0.5	0.5	1.3
178.	*	0.5	0.4	0.3	0.4	0.2	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.3	0.5	0.5	0.5	0.5	0.5	0.4	1.3
179.	*	0.5	0.4	0.3	0.3	0.2	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.4	0.4	0.4	0.4	0.4	0.4	1.4
180.	*	0.5	0.3	0.3	0.3	0.2	0.0	0.0	0.1	0.1	0.1	0.0	0.1	0.2	0.4	0.4	0.4	0.4	0.4	0.4	1.4
181.	*	0.5	0.3	0.3	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.4	0.4	0.4	0.4	0.4	0.4	1.4
182.	*	0.5	0.3	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.4	0.4	0.4	0.4	0.4	0.3	1.4
183.	*	0.4	0.3	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.3	0.3	0.3	0.3	0.3	0.3	1.5
184.	*	0.3	0.3	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.2	1.5
185.	*	0.3	0.3	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.3	0.3	0.2	0.2	0.2	0.2	1.7
186.	*	0.3	0.2	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2	1.7
187.	*	0.3	0.2	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.2	0.2	0.2	0.1	0.1	0.1	1.7
188.	*	0.3	0.2	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.7
189.	*	0.3	0.2	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.8
190.	*	0.3	0.2	0.2	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.7
191.	*	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.8
192.	*	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.8
193.	*	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	1.8
194.	*	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.0	1.8

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
195.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.8
196.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.8
197.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
198.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
199.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
200.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
201.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
202.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
203.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.7
204.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
205.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
206.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
207.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
208.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
209.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
210.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
211.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
212.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
213.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
214.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
215.	0.2	0.2	0.2	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
216.	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
217.	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
218.	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
219.	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.6
220.	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
221.	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
222.	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
223.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
224.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
225.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
226.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5
227.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.4
228.	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
229.	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
230.	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
231.	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.5
232.	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.5

233.	*	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
234.	*	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
235.	*	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
236.	*	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
237.	*	0.3	0.3	0.3	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
238.	*	0.3	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
239.	*	0.3	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
240.	*	0.3	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.4
241.	*	0.3	0.3	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
242.	*	0.3	0.3	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
243.	*	0.3	0.3	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
244.	*	0.3	0.3	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
245.	*	0.3	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
246.	*	0.3	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
247.	*	0.3	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
248.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
249.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
250.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.2
251.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	1.1
252.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
253.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
254.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
255.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
256.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
257.	*	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
258.	*	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
259.	*	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
260.	*	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
261.	*	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
262.	*	0.2	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
263.	*	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.2
264.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.2
265.	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.2
266.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.2
267.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.2
268.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
269.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1

270.	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
271.	*	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
272.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
273.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
274.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
275.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
276.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
277.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
278.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
279.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
280.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
281.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.3	0.0	0.0	0.0	0.0	0.0	0.0	1.1
282.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
283.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
284.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
285.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
286.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
287.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
288.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
289.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
290.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
291.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.1
292.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
293.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
294.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
295.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
296.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
297.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
298.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
299.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
300.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
301.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
302.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
303.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
304.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
305.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2
306.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.2

307.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.3
308.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.3
309.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
310.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
311.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
312.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
313.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
314.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.3	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
315.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.4
316.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
317.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
318.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
319.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
320.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
321.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
322.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
323.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
324.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
325.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.3	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
326.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
327.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
328.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
329.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
330.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
331.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
332.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.5
333.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
334.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
335.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.8
336.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.8
337.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.8
338.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
339.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
340.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
341.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
342.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
343.	*	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.6
344.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
345.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	1.7
346.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.1	1.6
347.	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.1	0.1	1.6

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
348.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.1	0.1	0.1	1.6
349.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.1	0.1	0.1	1.4
350.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.2	1.4
351.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.2	1.4
352.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.2	1.4
353.	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.2	0.2	0.2	0.1	0.1	0.2	0.2	0.2	0.2	1.4
354.	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.1	0.2	0.2	0.2	0.2	0.2	1.3
355.	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.1	0.2	0.2	0.2	0.2	0.3	1.3
356.	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.3	0.1	0.2	0.2	0.2	0.3	0.3	1.3
357.	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.3	0.1	0.2	0.2	0.2	0.3	0.3	1.2
358.	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.3	0.3	0.2	0.2	0.3	0.3	0.3	1.1
359.	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.4	0.3	0.3	0.3	0.3	0.3	1.1
360.	0.2	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.3	0.3	0.5	0.5	0.4	0.4	0.4	0.4	1.1
MAX	1.2	1.0	0.9	0.7	0.6	0.6	0.6	0.6	0.6	0.8	1.0	1.0	1.1	1.3	1.1	1.1	1.1	1.1	1.1	1.8
DEGR.	97	97	94	94	91	72	79	85	75	74	79	75	77	70	59	49	153	153	36	335

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

MODEL RESULTS

REMARKS : In search of the angle corresponding to the maximum concentration, only the first angle, of the angles with same maximum concentrations, is indicated as maximum.

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
0.	1.0	0.9	0.9	0.9	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.5
1.	1.1	0.9	0.9	0.9	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.5
2.	1.0	0.9	0.9	0.9	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.5
3.	1.0	0.9	0.9	0.9	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.6
4.	0.9	0.9	0.9	0.9	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.6
5.	0.8	0.9	0.8	0.9	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.6
6.	0.8	0.8	0.7	0.8	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.6
7.	0.8	0.8	0.7	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.6
8.	0.7	0.8	0.7	0.8	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6

9.	*	0.7	0.8	0.7	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5
10.	*	0.7	0.7	0.7	0.8	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.4
11.	*	0.7	0.7	0.7	0.8	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.4
12.	*	0.7	0.6	0.6	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
13.	*	0.6	0.6	0.6	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
14.	*	0.5	0.6	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
15.	*	0.4	0.5	0.5	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
16.	*	0.4	0.5	0.5	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
17.	*	0.4	0.5	0.5	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
18.	*	0.4	0.5	0.5	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
19.	*	0.4	0.4	0.5	0.7	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.4
20.	*	0.4	0.4	0.4	0.7	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.4
21.	*	0.3	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5
22.	*	0.3	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.6	0.5
23.	*	0.3	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.6	0.5
24.	*	0.3	0.4	0.4	0.6	0.6	0.5	0.5	0.5	0.5	0.5	0.6	0.5
25.	*	0.3	0.4	0.4	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.5
26.	*	0.3	0.3	0.4	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.5
27.	*	0.3	0.3	0.4	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.5
28.	*	0.3	0.3	0.3	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.6	0.5
29.	*	0.2	0.3	0.3	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
30.	*	0.2	0.3	0.3	0.6	0.5	0.5	0.5	0.5	0.5	0.5	0.4	0.5
31.	*	0.2	0.3	0.3	0.6	0.5	0.6	0.5	0.5	0.5	0.5	0.4	0.5
32.	*	0.2	0.3	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.5	0.4	0.5
33.	*	0.2	0.3	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
34.	*	0.2	0.3	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
35.	*	0.2	0.2	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
36.	*	0.2	0.2	0.4	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
37.	*	0.2	0.2	0.4	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
38.	*	0.2	0.2	0.4	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.4	0.5
39.	*	0.2	0.2	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.5	0.5
40.	*	0.2	0.2	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.5	0.5
41.	*	0.2	0.2	0.3	0.5	0.5	0.6	0.5	0.5	0.5	0.6	0.5	0.5

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
42.	*	0.2	0.2	0.3	0.5	0.5	0.6	0.6	0.5	0.6	0.6	0.5	0.5
43.	*	0.3	0.2	0.3	0.5	0.5	0.6	0.6	0.6	0.7	0.7	0.6	0.6
44.	*	0.3	0.2	0.3	0.4	0.5	0.6	0.6	0.6	0.7	0.6	0.6	0.6
45.	*	0.3	0.2	0.3	0.4	0.5	0.6	0.6	0.6	0.7	0.5	0.6	0.7

46.	*	0.3	0.3	0.3	0.4	0.5	0.6	0.6	0.6	0.7	0.5	0.6	0.7
47.	*	0.3	0.3	0.3	0.4	0.5	0.6	0.6	0.7	0.7	0.5	0.6	0.7
48.	*	0.3	0.3	0.4	0.4	0.5	0.6	0.6	0.7	0.7	0.5	0.6	0.7
49.	*	0.3	0.3	0.4	0.3	0.5	0.6	0.6	0.7	0.7	0.6	0.6	0.7
50.	*	0.3	0.3	0.4	0.3	0.5	0.6	0.6	0.7	0.7	0.6	0.6	0.7
51.	*	0.3	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.7	0.6	0.6	0.7
52.	*	0.3	0.3	0.4	0.4	0.5	0.6	0.7	0.7	0.7	0.6	0.6	0.7
53.	*	0.3	0.3	0.4	0.4	0.6	0.8	0.8	0.8	0.7	0.7	0.6	0.7
54.	*	0.3	0.3	0.4	0.4	0.6	0.8	0.8	0.8	0.6	0.7	0.7	0.8
55.	*	0.3	0.3	0.4	0.4	0.6	0.8	0.8	0.8	0.6	0.7	0.8	0.8
56.	*	0.3	0.3	0.4	0.4	0.6	0.8	0.8	0.8	0.6	0.7	0.8	0.8
57.	*	0.2	0.3	0.4	0.4	0.5	0.8	0.8	0.8	0.7	0.7	0.8	0.8
58.	*	0.2	0.3	0.4	0.4	0.5	0.8	0.8	0.8	0.7	0.7	0.8	0.8
59.	*	0.2	0.3	0.4	0.4	0.5	0.8	0.8	0.7	0.7	0.7	0.8	0.8
60.	*	0.2	0.3	0.4	0.4	0.4	0.8	0.8	0.7	0.7	0.7	0.8	0.8
61.	*	0.2	0.3	0.4	0.4	0.4	0.8	0.8	0.6	0.7	0.7	0.8	0.8
62.	*	0.2	0.3	0.4	0.4	0.5	0.8	0.8	0.7	0.7	0.7	0.8	0.8
63.	*	0.2	0.3	0.4	0.4	0.5	0.8	0.7	0.7	0.7	0.7	0.8	0.8
64.	*	0.2	0.3	0.4	0.4	0.5	0.7	0.8	0.8	0.8	0.7	0.8	0.8
65.	*	0.2	0.3	0.4	0.4	0.5	0.7	0.7	0.8	0.8	0.8	0.9	0.9
66.	*	0.2	0.3	0.4	0.4	0.5	0.7	0.8	0.8	0.8	0.9	0.9	0.9
67.	*	0.2	0.3	0.4	0.4	0.5	0.7	0.8	0.8	0.8	0.9	0.9	0.9
68.	*	0.2	0.3	0.4	0.3	0.5	0.7	0.8	0.8	0.8	0.9	0.9	0.9
69.	*	0.2	0.3	0.4	0.3	0.5	0.8	0.8	0.8	0.8	0.9	0.9	0.9
70.	*	0.2	0.2	0.4	0.3	0.5	0.8	0.8	0.8	0.8	0.9	0.9	0.9
71.	*	0.2	0.2	0.4	0.3	0.5	0.8	0.8	0.8	0.8	0.9	0.9	0.9
72.	*	0.2	0.2	0.4	0.3	0.5	0.8	0.8	0.8	0.8	0.9	0.9	0.9
73.	*	0.2	0.2	0.4	0.3	0.5	0.8	0.8	0.8	0.8	0.8	0.9	0.9
74.	*	0.2	0.2	0.3	0.3	0.4	0.8	0.9	0.9	0.9	0.8	0.8	0.8
75.	*	0.2	0.2	0.3	0.3	0.4	0.8	0.9	0.9	0.9	0.9	0.9	0.9
76.	*	0.1	0.2	0.3	0.3	0.4	0.8	0.9	0.9	0.9	0.9	0.9	0.9
77.	*	0.1	0.2	0.3	0.3	0.4	0.8	0.9	0.9	0.9	0.9	0.9	0.9
78.	*	0.1	0.2	0.3	0.3	0.4	0.8	0.9	0.9	0.9	0.9	0.9	0.9
79.	*	0.1	0.1	0.3	0.3	0.4	0.7	0.9	0.9	0.9	0.9	0.9	0.9
80.	*	0.0	0.1	0.3	0.3	0.4	0.7	0.9	0.9	0.9	0.9	0.9	0.9
81.	*	0.0	0.1	0.3	0.3	0.4	0.7	0.9	0.9	0.9	0.9	0.9	0.9
82.	*	0.0	0.1	0.3	0.2	0.4	0.7	0.8	0.9	0.9	0.9	0.9	0.9
83.	*	0.0	0.1	0.2	0.2	0.4	0.7	0.8	0.8	0.9	0.9	0.9	0.9
84.	*	0.0	0.0	0.2	0.2	0.3	0.7	0.8	0.8	0.8	0.8	0.8	0.8
85.	*	0.0	0.0	0.2	0.2	0.3	0.7	0.8	0.8	0.8	0.8	0.8	0.8
86.	*	0.0	0.0	0.2	0.1	0.3	0.6	0.8	0.8	0.8	0.8	0.8	0.8
87.	*	0.0	0.0	0.2	0.1	0.3	0.6	0.7	0.8	0.8	0.7	0.7	0.7
88.	*	0.0	0.0	0.2	0.1	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7
89.	*	0.0	0.0	0.1	0.1	0.3	0.6	0.7	0.7	0.7	0.7	0.7	0.7
90.	*	0.0	0.0	0.1	0.1	0.2	0.6	0.7	0.7	0.7	0.7	0.7	0.7
91.	*	0.0	0.0	0.1	0.1	0.1	0.5	0.7	0.7	0.7	0.7	0.7	0.7
92.	*	0.0	0.0	0.1	0.1	0.1	0.5	0.7	0.7	0.7	0.7	0.7	0.7

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
93.	0.0	0.0	0.1	0.1	0.1	0.4	0.6	0.7	0.7	0.7	0.7	0.7
94.	0.0	0.0	0.1	0.0	0.1	0.4	0.5	0.6	0.6	0.5	0.5	0.5
95.	0.0	0.0	0.1	0.0	0.1	0.4	0.5	0.5	0.5	0.5	0.5	0.5
96.	0.0	0.0	0.1	0.0	0.1	0.3	0.5	0.5	0.5	0.5	0.5	0.5
97.	0.0	0.0	0.1	0.0	0.1	0.3	0.5	0.5	0.5	0.5	0.5	0.5
98.	0.0	0.0	0.1	0.0	0.1	0.3	0.4	0.5	0.5	0.5	0.5	0.5
99.	0.0	0.0	0.1	0.0	0.1	0.3	0.4	0.4	0.4	0.4	0.4	0.4
100.	0.0	0.0	0.1	0.0	0.0	0.2	0.4	0.4	0.4	0.4	0.4	0.4
101.	0.0	0.0	0.1	0.0	0.0	0.2	0.4	0.4	0.4	0.4	0.4	0.4
102.	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.4	0.4	0.4	0.4	0.4
103.	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.3	0.3	0.4	0.4
104.	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.3	0.3	0.3	0.3
105.	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.3	0.3	0.3	0.3
106.	0.0	0.0	0.1	0.0	0.0	0.2	0.3	0.3	0.3	0.3	0.3	0.3
107.	0.0	0.0	0.1	0.0	0.0	0.1	0.3	0.3	0.3	0.3	0.3	0.3
108.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.3	0.3	0.3	0.3	0.3
109.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.3	0.3
110.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
111.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
112.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
113.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
114.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
115.	0.0	0.0	0.1	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.2	0.2
116.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.2
117.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.2
118.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.2	0.2	0.2	0.2
119.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
120.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
121.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
122.	0.0	0.0	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
123.	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
124.	0.0	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
125.	0.0	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
126.	0.0	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
127.	0.0	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
128.	0.0	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
129.	0.0	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1

130.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
131.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
132.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
133.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
134.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
135.	*	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
136.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
137.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
138.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
139.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
140.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
141.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
142.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
143.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
144.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
145.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
146.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
147.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
148.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
149.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
150.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
151.	*	0.1	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
152.	*	0.2	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
153.	*	0.2	0.1	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
154.	*	0.2	0.2	0.2	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1
155.	*	0.2	0.2	0.2	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
156.	*	0.2	0.2	0.3	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
157.	*	0.2	0.2	0.3	0.1	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1
158.	*	0.2	0.3	0.3	0.1	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1
159.	*	0.2	0.3	0.3	0.3	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1
160.	*	0.3	0.3	0.3	0.3	0.1	0.0	0.0	0.1	0.1	0.1	0.1	0.1
161.	*	0.3	0.3	0.3	0.3	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.1
162.	*	0.3	0.4	0.3	0.3	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.1
163.	*	0.3	0.4	0.3	0.3	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.1
164.	*	0.4	0.4	0.5	0.3	0.2	0.0	0.0	0.1	0.1	0.1	0.1	0.1
165.	*	0.4	0.4	0.5	0.3	0.2	0.1	0.0	0.1	0.1	0.1	0.1	0.1
166.	*	0.4	0.5	0.5	0.4	0.2	0.1	0.0	0.1	0.1	0.1	0.1	0.1

167.	*	0.5	0.6	0.5	0.4	0.2	0.1	0.0	0.1	0.1	0.1	0.1	0.1
168.	*	0.8	0.7	0.8	0.5	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1
169.	*	0.8	0.8	0.8	0.6	0.3	0.1	0.2	0.1	0.1	0.1	0.1	0.1
170.	*	0.9	0.9	0.8	0.6	0.3	0.1	0.2	0.1	0.1	0.1	0.1	0.1
171.	*	0.9	0.9	0.8	0.8	0.4	0.1	0.2	0.1	0.1	0.1	0.1	0.1
172.	*	0.9	0.9	0.9	0.8	0.4	0.1	0.2	0.1	0.1	0.1	0.1	0.1
173.	*	1.0	1.0	1.0	0.8	0.5	0.3	0.2	0.2	0.1	0.1	0.1	0.1
174.	*	1.0	1.0	1.0	0.9	0.5	0.3	0.2	0.2	0.1	0.1	0.1	0.1
175.	*	1.0	1.0	1.0	0.9	0.6	0.3	0.2	0.2	0.1	0.1	0.1	0.1
176.	*	1.2	1.1	1.0	1.0	0.7	0.3	0.2	0.2	0.1	0.1	0.1	0.1
177.	*	1.2	1.2	1.2	1.0	0.7	0.3	0.3	0.2	0.2	0.1	0.1	0.1
178.	*	1.2	1.4	1.2	1.1	0.7	0.3	0.4	0.2	0.2	0.1	0.1	0.1
179.	*	1.3	1.4	1.4	1.1	0.7	0.4	0.4	0.2	0.2	0.1	0.1	0.1
180.	*	1.4	1.4	1.4	1.1	0.9	0.5	0.4	0.3	0.2	0.2	0.1	0.1
181.	*	1.5	1.5	1.4	1.2	0.9	0.5	0.4	0.3	0.2	0.2	0.1	0.1
182.	*	1.5	1.6	1.5	1.3	1.0	0.5	0.4	0.4	0.2	0.2	0.1	0.1
183.	*	1.6	1.6	1.6	1.3	1.0	0.7	0.3	0.4	0.2	0.2	0.2	0.1
184.	*	1.7	1.6	1.6	1.4	1.0	0.7	0.3	0.4	0.3	0.2	0.2	0.1
185.	*	1.7	1.6	1.6	1.4	1.0	0.7	0.4	0.4	0.3	0.2	0.2	0.1
186.	*	1.7	1.8	1.7	1.5	1.1	0.7	0.4	0.4	0.3	0.2	0.2	0.2
187.	*	1.7	1.8	1.7	1.5	1.2	0.7	0.4	0.4	0.4	0.3	0.2	0.2
188.	*	1.7	1.8	1.7	1.5	1.3	0.7	0.5	0.4	0.4	0.3	0.2	0.2
189.	*	1.8	1.8	1.7	1.5	1.3	0.7	0.5	0.4	0.4	0.3	0.2	0.2
190.	*	1.9	1.9	1.8	1.5	1.2	0.7	0.5	0.4	0.4	0.3	0.3	0.2
191.	*	1.8	1.9	1.7	1.7	1.2	0.8	0.6	0.4	0.4	0.4	0.3	0.2
192.	*	1.9	1.8	1.7	1.7	1.2	0.9	0.6	0.5	0.4	0.4	0.3	0.2
193.	*	1.9	1.8	1.7	1.7	1.3	0.9	0.7	0.6	0.4	0.4	0.3	0.3
194.	*	1.9	1.9	1.8	1.7	1.4	0.9	0.7	0.6	0.4	0.4	0.3	0.3

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	* CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
195.	1.9	1.9	1.8	1.7	1.4	0.9	0.7	0.6	0.4	0.4	0.4	0.3
196.	1.8	1.9	1.8	1.7	1.4	0.9	0.7	0.6	0.4	0.4	0.4	0.3
197.	1.8	1.8	1.7	1.7	1.4	1.0	0.8	0.6	0.4	0.4	0.4	0.3
198.	1.8	1.8	1.7	1.6	1.3	0.9	0.8	0.6	0.5	0.4	0.4	0.3
199.	1.7	1.8	1.7	1.6	1.4	0.9	0.7	0.6	0.5	0.4	0.4	0.4
200.	1.7	1.8	1.7	1.6	1.4	0.9	0.7	0.5	0.5	0.4	0.4	0.4
201.	1.8	1.7	1.6	1.6	1.4	0.9	0.7	0.6	0.5	0.4	0.4	0.4
202.	1.8	1.7	1.6	1.6	1.4	1.0	0.7	0.7	0.5	0.4	0.4	0.4
203.	1.7	1.7	1.6	1.6	1.4	1.0	0.7	0.7	0.5	0.5	0.4	0.4
204.	1.7	1.7	1.6	1.6	1.3	1.1	0.7	0.7	0.5	0.5	0.4	0.4
205.	1.7	1.7	1.6	1.5	1.3	1.0	0.7	0.7	0.5	0.5	0.4	0.4
206.	1.7	1.6	1.5	1.5	1.3	1.0	0.7	0.7	0.5	0.5	0.4	0.4
207.	1.7	1.6	1.5	1.5	1.3	1.0	0.7	0.7	0.5	0.5	0.4	0.4
208.	1.6	1.6	1.5	1.5	1.3	1.0	0.7	0.7	0.5	0.5	0.4	0.4
209.	1.6	1.6	1.5	1.5	1.3	1.0	0.7	0.7	0.6	0.5	0.4	0.4
210.	1.6	1.6	1.5	1.5	1.3	1.0	0.7	0.7	0.7	0.5	0.4	0.4
211.	1.6	1.5	1.5	1.5	1.3	1.0	0.8	0.6	0.7	0.5	0.5	0.4
212.	1.6	1.5	1.5	1.5	1.3	1.0	0.8	0.6	0.7	0.5	0.5	0.4
213.	1.5	1.5	1.5	1.5	1.2	1.0	0.8	0.6	0.7	0.5	0.5	0.4
214.	1.5	1.5	1.5	1.4	1.2	1.0	0.8	0.6	0.6	0.5	0.5	0.4
215.	1.5	1.5	1.5	1.3	1.2	0.9	0.8	0.6	0.6	0.5	0.5	0.4
216.	1.5	1.6	1.4	1.3	1.1	0.9	0.8	0.6	0.6	0.5	0.5	0.4
217.	1.5	1.5	1.4	1.3	1.1	0.9	0.8	0.6	0.6	0.5	0.5	0.4
218.	1.5	1.5	1.4	1.3	1.1	0.9	0.8	0.6	0.6	0.6	0.4	0.4
219.	1.5	1.5	1.4	1.3	1.1	0.9	0.7	0.6	0.6	0.6	0.4	0.3
220.	1.4	1.5	1.3	1.3	1.1	0.9	0.7	0.6	0.6	0.6	0.4	0.3
221.	1.4	1.3	1.3	1.3	1.1	0.9	0.7	0.6	0.6	0.6	0.4	0.3
222.	1.4	1.3	1.3	1.3	1.1	0.9	0.7	0.6	0.6	0.6	0.5	0.3
223.	1.4	1.3	1.3	1.2	1.1	0.9	0.7	0.5	0.6	0.6	0.5	0.3
224.	1.4	1.3	1.3	1.2	1.1	0.9	0.7	0.5	0.6	0.6	0.6	0.3
225.	1.4	1.3	1.3	1.1	1.1	0.9	0.7	0.5	0.6	0.6	0.6	0.3
226.	1.4	1.3	1.2	1.1	1.1	0.9	0.7	0.5	0.6	0.6	0.6	0.3
227.	1.4	1.2	1.2	1.1	1.1	0.9	0.7	0.5	0.5	0.6	0.5	0.4
228.	1.3	1.2	1.2	1.1	1.1	0.9	0.7	0.6	0.5	0.6	0.5	0.4
229.	1.3	1.2	1.2	1.1	1.1	0.9	0.7	0.6	0.5	0.6	0.5	0.4
230.	1.3	1.2	1.2	1.1	1.1	0.9	0.7	0.6	0.5	0.6	0.5	0.5
231.	1.2	1.2	1.2	1.1	1.1	0.9	0.7	0.6	0.5	0.5	0.5	0.5
232.	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.6	0.5	0.5	0.5	0.6

233.	*	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.6	0.5	0.6	0.5	0.6
234.	*	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.6	0.6	0.6	0.5	0.6
235.	*	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.7	0.6	0.6	0.5	0.6
236.	*	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.7	0.6	0.6	0.5	0.5
237.	*	1.2	1.2	1.1	1.1	1.1	0.9	0.7	0.7	0.6	0.6	0.5	0.5
238.	*	1.2	1.1	1.1	1.1	1.1	0.9	0.7	0.7	0.6	0.6	0.5	0.5
239.	*	1.2	1.1	1.1	1.1	1.1	0.9	0.8	0.7	0.6	0.6	0.5	0.5
240.	*	1.2	1.1	1.1	1.1	1.1	0.9	0.8	0.7	0.6	0.6	0.5	0.5
241.	*	1.2	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.6	0.6	0.5	0.5
242.	*	1.2	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.6	0.6	0.5	0.5
243.	*	1.2	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.6	0.6	0.6	0.6
244.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.6	0.7	0.6	0.6
245.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.6	0.7	0.7	0.6	0.6

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
246.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.7	0.7	0.6	0.6
247.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.7	0.6	0.6	0.6
248.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.7	0.6	0.6	0.6
249.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.7	0.6	0.6	0.6
250.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.7	0.7	0.6	0.7	0.7
251.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.7	0.7	0.7	0.7	0.7
252.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.7	0.7	0.7	0.7	0.7
253.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.7	0.8	0.7	0.7	0.7
254.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.7	0.8	0.7	0.7	0.7
255.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.7	0.8	0.7	0.7	0.7
256.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.8	0.8	0.7	0.7	0.8
257.	*	1.1	1.1	1.1	1.0	1.0	0.8	0.9	0.8	0.8	0.7	0.8	0.8
258.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.7	0.8	0.8
259.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.8	0.8
260.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.8	0.8
261.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.8	0.8	0.8	0.8	0.8
262.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.8	0.9	0.8	0.8	0.8
263.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.8	0.9	0.8	0.8	0.7
264.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.8	0.9	0.8	0.8	0.7
265.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.8	0.8	0.8	0.8	0.8
266.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.7	0.8
267.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.7	0.8
268.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.8	0.7	0.8
269.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.7	0.7	0.8

270.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.7	0.8	0.8
271.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.8	0.8	0.7	0.8	0.8
272.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.8	0.7	0.8	0.8
273.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.7	0.7	0.8	0.8
274.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.7	0.7	0.8	0.8
275.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.7	0.7	0.7	0.8
276.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.7	0.7	0.7	0.9
277.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.7	0.7	0.7	0.8	0.9
278.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.6	0.7	0.7	0.8	0.9
279.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.9	0.6	0.7	0.7	0.8	0.9
280.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.6	0.7	0.8	0.8	0.8
281.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.6	0.7	0.8	0.9	0.8
282.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.6	0.8	0.8	0.9	0.8
283.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.8	0.6	0.8	0.9	0.8	0.8
284.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.7	0.6	0.8	1.0	0.8	0.8
285.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.7	0.6	0.8	0.9	0.8	0.8
286.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.7	0.8	0.9	0.9	0.8	0.8
287.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.6	0.8	1.0	0.8	0.8	0.8
288.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.6	0.9	0.9	0.8	0.8	0.8
289.	*	1.1	1.1	1.1	1.0	1.0	0.9	0.6	0.9	0.9	0.8	0.8	0.8
290.	*	1.1	1.1	1.1	1.0	0.9	0.9	0.6	0.9	0.9	0.8	0.8	0.8
291.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.6	0.9	0.8	0.8	0.8	0.8
292.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.7	0.9	0.8	0.8	0.8	0.8
293.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.8
294.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.8	0.8	0.8	0.8	0.8	0.8
295.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.8	0.8	0.7	0.8	0.8	0.8
296.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.8	0.8	0.7	0.7	0.8	0.9

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	*	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
297.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.8	0.8	0.7	0.7	0.7	0.8
298.	*	1.1	1.1	1.1	1.0	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.8
299.	*	1.2	1.1	1.1	1.0	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.8
300.	*	1.2	1.1	1.1	1.0	0.9	0.8	0.8	0.7	0.7	0.7	0.7	0.8
301.	*	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.7	0.7	0.7	0.7	0.8
302.	*	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.7	0.7	0.7	0.8	0.8
303.	*	1.2	1.1	1.1	1.0	0.9	0.9	0.8	0.7	0.7	0.7	0.8	0.8
304.	*	1.2	1.1	1.1	1.0	0.9	0.8	0.8	0.7	0.7	0.7	0.8	0.8
305.	*	1.2	1.2	1.1	1.1	0.9	0.9	0.8	0.7	0.7	0.7	0.8	0.8
306.	*	1.2	1.2	1.1	1.1	0.9	0.9	0.8	0.7	0.7	0.7	0.8	0.8

307.	*	1.4	1.2	1.1	1.1	0.8	0.8	0.6	0.7	0.7	0.7	0.8	0.8
308.	*	1.4	1.2	1.1	1.1	0.8	0.8	0.6	0.7	0.7	0.6	0.7	0.7
309.	*	1.4	1.2	1.1	1.0	0.8	0.8	0.6	0.7	0.7	0.6	0.7	0.7
310.	*	1.4	1.2	1.1	1.0	0.8	0.7	0.7	0.7	0.7	0.6	0.7	0.7
311.	*	1.4	1.2	1.1	1.0	0.7	0.7	0.7	0.7	0.7	0.6	0.7	0.7
312.	*	1.4	1.2	1.1	1.0	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
313.	*	1.4	1.2	1.1	1.0	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7
314.	*	1.4	1.3	1.1	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7
315.	*	1.4	1.3	1.1	1.1	0.8	0.7	0.7	0.7	0.7	0.7	0.7	0.7
316.	*	1.4	1.3	1.1	1.1	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7
317.	*	1.4	1.3	1.1	1.1	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7
318.	*	1.3	1.3	1.1	1.1	0.8	0.8	0.7	0.7	0.7	0.7	0.7	0.7
319.	*	1.3	1.3	1.1	1.0	0.9	0.8	0.7	0.7	0.7	0.7	0.7	0.7
320.	*	1.3	1.3	1.1	1.0	0.9	0.8	0.7	0.7	0.7	0.7	0.6	0.7
321.	*	1.3	1.3	1.0	0.9	0.8	0.8	0.7	0.7	0.7	0.7	0.6	0.7
322.	*	1.3	1.3	1.1	1.0	0.8	0.7	0.7	0.7	0.7	0.7	0.6	0.7
323.	*	1.4	1.3	1.1	1.0	0.8	0.8	0.7	0.7	0.7	0.7	0.6	0.7
324.	*	1.4	1.3	1.1	1.0	0.8	0.8	0.7	0.7	0.7	0.7	0.6	0.7
325.	*	1.4	1.3	1.1	1.0	0.9	0.8	0.7	0.7	0.7	0.7	0.6	0.7
326.	*	1.4	1.3	1.1	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.6	0.6
327.	*	1.4	1.3	1.2	1.0	1.0	0.8	0.7	0.7	0.7	0.7	0.6	0.6
328.	*	1.5	1.3	1.2	1.0	1.1	0.9	0.7	0.7	0.7	0.7	0.6	0.6
329.	*	1.6	1.2	1.2	1.0	1.1	0.8	0.8	0.7	0.7	0.7	0.6	0.6
330.	*	1.6	1.3	1.2	1.0	1.1	0.8	0.8	0.7	0.7	0.7	0.6	0.6
331.	*	1.6	1.4	1.2	1.0	1.1	0.8	0.8	0.7	0.7	0.7	0.6	0.6
332.	*	1.7	1.4	1.1	1.0	1.0	0.8	0.8	0.7	0.7	0.7	0.6	0.6
333.	*	1.7	1.4	1.1	1.2	1.0	0.8	0.8	0.7	0.7	0.7	0.6	0.6
334.	*	1.6	1.4	1.2	1.2	0.9	0.8	0.8	0.7	0.7	0.8	0.6	0.6
335.	*	1.6	1.4	1.2	1.0	1.0	0.8	0.8	0.7	0.7	0.8	0.7	0.6
336.	*	1.6	1.4	1.2	1.2	1.1	0.8	0.8	0.7	0.8	0.8	0.6	0.6
337.	*	1.6	1.4	1.3	1.2	1.1	0.8	0.8	0.8	0.8	0.7	0.6	0.6
338.	*	1.6	1.3	1.3	1.1	1.1	0.8	0.8	0.8	0.8	0.7	0.6	0.6
339.	*	1.6	1.3	1.3	1.1	1.1	0.8	0.9	0.8	0.8	0.7	0.6	0.6
340.	*	1.6	1.4	1.2	1.2	1.1	0.8	0.9	0.8	0.8	0.7	0.6	0.6
341.	*	1.4	1.4	1.2	1.2	1.0	0.9	0.9	0.8	0.8	0.6	0.6	0.6
342.	*	1.5	1.3	1.2	1.1	1.0	0.9	0.9	0.8	0.8	0.6	0.6	0.6
343.	*	1.4	1.3	1.2	1.1	1.0	0.9	0.8	0.8	0.7	0.6	0.6	0.6
344.	*	1.4	1.3	1.1	0.9	1.0	0.9	0.8	0.8	0.7	0.6	0.6	0.6
345.	*	1.4	1.3	1.2	0.8	1.0	0.9	0.8	0.8	0.6	0.6	0.6	0.6
346.	*	1.4	1.3	1.2	0.9	1.1	0.9	0.8	0.8	0.6	0.6	0.6	0.6
347.	*	1.4	1.3	1.1	1.0	1.0	0.9	0.8	0.8	0.6	0.6	0.6	0.6

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

WIND ANGLE RANGE: 0.-360.

WIND ANGLE (DEGR)	CONCENTRATION (PPM) REC41	REC42	REC43	REC44	REC45	REC46	REC47	REC48	REC49	REC50	REC51	REC52
348.	1.3	1.2	1.1	1.0	1.0	0.9	0.8	0.8	0.6	0.6	0.6	0.5
349.	1.3	1.2	1.1	1.0	1.0	0.9	0.8	0.6	0.6	0.6	0.6	0.5
350.	1.3	1.2	1.1	1.1	1.0	0.9	0.8	0.6	0.6	0.6	0.6	0.5
351.	1.3	1.2	1.2	1.1	1.0	0.9	0.8	0.6	0.6	0.6	0.5	0.5
352.	1.3	1.2	1.2	1.1	1.0	0.9	0.7	0.6	0.6	0.6	0.5	0.5
353.	1.2	1.2	1.2	1.1	1.0	0.8	0.7	0.6	0.6	0.6	0.5	0.5
354.	1.1	1.1	0.9	1.1	1.0	0.8	0.6	0.6	0.6	0.5	0.5	0.5
355.	1.1	1.1	1.0	1.1	1.0	0.7	0.6	0.6	0.6	0.5	0.5	0.5
356.	1.1	1.0	1.0	0.9	0.9	0.7	0.6	0.6	0.6	0.5	0.5	0.5
357.	1.1	1.0	1.0	0.9	0.9	0.7	0.6	0.6	0.5	0.5	0.5	0.5
358.	1.0	1.1	1.0	0.9	0.8	0.7	0.6	0.6	0.5	0.5	0.5	0.5
359.	1.0	1.0	0.9	0.8	0.8	0.7	0.6	0.6	0.5	0.5	0.5	0.5
360.	1.0	0.9	0.9	0.9	0.8	0.6	0.6	0.5	0.5	0.5	0.5	0.5
MAX	1.9	1.9	1.8	1.7	1.4	1.1	0.9	0.9	1.0	1.0	0.9	0.9
DEGR.	190	190	190	193	194	204	251	288	287	284	65	65

THE HIGHEST CONCENTRATION OF 1.90 PPM OCCURRED AT RECEPTOR REC41.

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

DATE : 8/ 9/20
TIME : 1:18:10

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

LINK #	CO/LINK (PPM) ANGLE (DEGREES) REC1	REC2	REC3	REC4	REC5	REC6	REC7	REC8	REC9	REC10	REC11	REC12	REC13	REC14	REC15	REC16	REC17	REC18	REC19	REC20
	213	204	197	191	199	192	199	186	184	184	179	180	192	162	155	163	164	161	159	157
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.1	0.1	0.1	0.1	0.1	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

10	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	*	0.1	0.2	0.2	0.2	0.1	0.2	0.1	0.2	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2
15	*	0.1	0.1	0.1	0.1	0.2	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
16	*	0.1	0.1	0.1	0.1	0.2	0.2	0.4	0.3	0.3	0.2	0.2	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.2
17	*	0.2	0.2	0.2	0.2	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18	*	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.4	0.5	0.6	0.6	0.6	0.8	0.2	0.2	0.1	0.0	0.0	0.0	0.0
19	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1
20	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	*	0.2	0.2	0.2	0.2	0.3	0.3	0.4	0.4	0.4	0.3	0.3	0.3	0.2	0.2	0.1	0.3	0.4	0.4	0.5	0.6
22	*	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	*	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1
24	*	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
25	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
26	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0	0.0	0.0	0.0
27	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
28	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0

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JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

DATE : 8/ 9/20
TIME : 1:18:10

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

		CO/LINK (PPM)																			
		ANGLE (DEGREES)																			
		REC21	REC22	REC23	REC24	REC25	REC26	REC27	REC28	REC29	REC30	REC31	REC32	REC33	REC34	REC35	REC36	REC37	REC38	REC39	REC40
LINK #	*	97	97	94	94	91	72	79	85	75	74	79	75	77	70	59	49	153	153	36	335
1	*	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0
2	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.1	0.0	0.0	0.0	0.0	0.0
4	*	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0
5	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	*	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	*	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

11	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4	0.4	0.0	0.0
15	*	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0	0.1	0.5
16	*	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.0	0.0	0.2	0.7
17	*	0.2	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.2	0.1	0.1	0.0	0.0	0.1	0.0
18	*	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1
19	*	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	*	0.0	0.1	0.1	0.1	0.1	0.2	0.2	0.2	0.2	0.1	0.1	0.1	0.2	0.5	0.5	0.5	0.7	0.7	0.6	0.3
22	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	*	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	*	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.2	0.2	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
25	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
26	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
27	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
28	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30	*	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.0	0.1	0.0	0.0	0.1	0.2

JOB: 2027 Baltimore3 Howard and Conway RUN: 2027 Baltimore3 Howard and Conway

DATE : 8/ 9/20
TIME : 1:18:10

RECEPTOR - LINK MATRIX FOR THE ANGLE PRODUCING
THE MAXIMUM CONCENTRATION FOR EACH RECEPTOR

CO/LINK (PPM)
ANGLE (DEGREES)

LINK #	REC41 190	REC42 190	REC43 190	REC44 193	REC45 194	REC46 204	REC47 251	REC48 288	REC49 287	REC50 284	REC51 65	REC52 65
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.3
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.8	0.6	0.5	0.3	0.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0
15	0.3	0.5	0.5	0.6	0.5	0.3	0.2	0.0	0.0	0.0	0.0	0.0
16	0.3	0.3	0.3	0.3	0.2	0.2	0.2	0.1	0.1	0.1	0.0	0.0
17	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.5	0.5	0.5	0.6	0.6
18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1	0.1	0.1	0.0	0.0
19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21	0.4	0.4	0.4	0.4	0.3	0.3	0.2	0.1	0.1	0.1	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30	0.1	0.1	0.1	0.1	0.1	0.1	0.0	0.0	0.0	0.0	0.0	0.0

ATTACHMENT B – MESOSCALE EMISSIONS ANALYSIS SAMPLE WORKSHEET

1) Sample Mesoscale MOVES Emissions Factors and Results for Each Region

			Anne Arundel County Emission Factors 2045 (gram/Mile)								
MOVES Road Type Code	**MOVES Road Type**	**MOVES Speed Bin**	**VOC**	**NOx**	**CO**	**PM2.5**	**PM10**	**SO2**	**CO2**	**CO2e**	**Energy Consumption (MMBTU)**
4	Interstate/Ramp	4	0.16	0.91	2.99	0.07	0.32	0.00	1167.73	1225.91	0.02
		5	0.13	0.82	2.92	0.04	0.24	0.00	1033.58	1081.25	0.01
		6	0.11	0.75	2.88	0.03	0.19	0.00	956.37	996.24	0.01
		7	0.09	0.75	2.86	0.03	0.16	0.00	938.54	974.82	0.01
		8	0.08	0.67	2.59	0.02	0.13	0.00	832.42	860.94	0.01
		10	0.06	0.66	2.57	0.02	0.08	0.00	804.71	825.69	0.01
		11	0.05	0.65	2.43	0.01	0.06	0.00	782.96	800.98	0.01
		12	0.05	0.65	2.27	0.01	0.05	0.00	761.77	777.38	0.01
		13	0.04	0.63	2.10	0.01	0.04	0.00	750.44	764.18	0.01
		14	0.04	0.64	2.07	0.01	0.04	0.00	771.48	784.51	0.01
5	Arterial/Connector	4	0.11	0.60	1.34	0.04	0.26	0.00	896.49	930.91	0.01
		5	0.10	0.57	1.53	0.03	0.20	0.00	821.52	853.45	0.01
		6	0.09	0.55	1.60	0.03	0.17	0.00	777.81	808.25	0.01
		7	0.08	0.54	1.69	0.02	0.14	0.00	755.00	784.45	0.01
		8	0.07	0.50	1.68	0.02	0.12	0.00	673.26	698.34	0.01
		9	0.06	0.47	1.67	0.02	0.09	0.00	642.23	664.03	0.01
		10	0.05	0.46	1.67	0.01	0.08	0.00	618.12	637.36	0.01

			Prince George's Emission Factors 2045 (gram/Mile)								
MOVES Road Type Code	**MOVES Road Type**	**MOVES Speed Bin**	**VOC**	**NOx**	**CO**	**PM2.5**	**PM10**	**SO2**	**CO2**	**CO2e**	**Energy Consumption (MMBTU)**
4	Interstate/Ramp	5	0.131	0.773	3.095	0.036	0.231	0.003	998.532	1047.146	0.014
		7	0.094	0.701	2.939	0.024	0.144	0.002	884.203	919.297	0.013
		8	0.075	0.615	2.503	0.020	0.116	0.002	768.651	795.211	0.011
		9	0.064	0.604	2.413	0.017	0.090	0.002	745.868	767.927	0.011
		10	0.055	0.594	2.316	0.014	0.070	0.002	726.675	745.145	0.010
		11	0.048	0.586	2.140	0.012	0.054	0.002	702.503	717.958	0.010
		13	0.037	0.565	1.813	0.009	0.034	0.002	668.094	679.278	0.010
		14	0.035	0.575	1.811	0.008	0.030	0.002	691.022	701.764	0.010
5	Arterial/Connector	5	0.100	0.525	1.575	0.030	0.189	0.002	778.743	811.839	0.011
		7	0.084	0.508	1.736	0.023	0.137	0.002	715.647	746.255	0.010
		8	0.073	0.466	1.722	0.019	0.111	0.002	644.219	670.240	0.009
		9	0.064	0.446	1.707	0.016	0.090	0.002	613.823	636.400	0.009
		10	0.057	0.430	1.700	0.013	0.073	0.002	590.221	610.116	0.008
		11	0.045	0.491	1.645	0.011	0.052	0.002	612.931	627.436	0.009
		13	0.031	0.532	1.486	0.007	0.028	0.002	624.805	633.077	0.009
		14	0.030	0.545	1.515	0.007	0.024	0.002	651.847	659.966	0.009

2) MOVES Road Type Code

FT	Road Type
1,12	Interstates
2	Freeways
3	Principal Arterials
4	Minor Arterials
5	Collectors
6,7,8,9,10	Ramps
13	Transit Station Access/Egress Links
34,35,36	Transit Links-Zero Vehicle Volumes

3) Sample Mesoscale Emission Worksheet Screenshot with Traffic Forecasts and Correlated MOVES Emission Factors

TAZ	A	B	ROADTYPE	MOVES ROAD TYPE ID	FFSPEED	Speed bin	VMT	Emission Factors 2045 (Gram/Mile)							
								VOC	NOx	CO	PM2.5	PM10	SO2	CO2	CO2e
								87	3	2	110	100	31	90	98
354	3017	10174	Access Link	5	30	7	905.20	0.081	0.544	1.690	0.025	0.144	0.002	754.999	784.448
317	3252	6733	Access Link	5	25	6	15.30	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
887	3253	15613	Access Link	5	25	6	4.10	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
336	3254	10052	Access Link	5	25	6	43.50	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
338	3255	10053	Access Link	5	25	6	21.90	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
330	3504	6791	Access Link	5	30	7	0.80	0.081	0.544	1.690	0.025	0.144	0.002	754.999	784.448
302	5772	5923	Principal Arterial	5	27	6	1042.40	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
302	5772	6630	Collector	5	20	5	1343.00	0.096	0.567	1.534	0.033	0.199	0.003	821.525	853.453
303	5794	6650	Principal Arterial	5	35	8	6855.40	0.070	0.496	1.681	0.020	0.116	0.002	673.263	698.345
201	5813	5825	Minor Arterial	5	24	6	652.40	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
202	5813	5842	Minor Arterial	5	24	6	334.30	0.087	0.549	1.599	0.028	0.172	0.002	777.807	808.249
321	6656	6728	Ramp	4	50	11	27759.80	0.052	0.654	2.433	0.015	0.063	0.002	782.958	800.981
320	6657	6658	Ramp	4	20	5	597.10	0.126	0.816	2.920	0.038	0.244	0.003	1033.585	1081.245
320	6658	6763	Ramp	4	20	5	2347.40	0.126	0.816	2.920	0.038	0.244	0.003	1033.585	1081.245
308	6680	6676	Ramp	4	30	7	6339.20	0.095	0.755	2.856	0.026	0.155	0.002	938.543	974.825
308	6680	6716	Interstate	4	53	12	15287.10	0.046	0.645	2.266	0.013	0.050	0.002	761.766	777.376
308	6682	6715	Ramp	4	30	7	8165.00	0.095	0.755	2.856	0.026	0.155	0.002	938.543	974.825
308	6689	6715	Interstate	4	53	12	12779.00	0.046	0.645	2.266	0.013	0.050	0.002	761.766	777.376
300	6708	6619	Freeway	4	29	7	3001.80	0.095	0.755	2.856	0.026	0.155	0.002	938.543	974.825

*Emission (tons) = EF (Gram/Mile) * VMT /(453.59*2000)*

TAZ	A	B	ROADTYPE	MOVES ROAD TYPE ID	FFSPEED	Speed bin	VMT	Emission (tons)							
								VOC	NOx	CO	PM2.5	PM10	SO2	CO2	CO2e
								87	3	2	110	100	31	90	98
354	3017	10174	Access Link	5	30	7	905.20	0.000	0.001	0.002	0.000	0.000	0.000	0.753	0.783
317	3252	6733	Access Link	5	25	6	15.30	0.000	0.000	0.000	0.000	0.000	0.000	0.013	0.014
887	3253	15613	Access Link	5	25	6	4.10	0.000	0.000	0.000	0.000	0.000	0.000	0.004	0.004
336	3254	10052	Access Link	5	25	6	43.50	0.000	0.000	0.000	0.000	0.000	0.000	0.037	0.039
338	3255	10053	Access Link	5	25	6	21.90	0.000	0.000	0.000	0.000	0.000	0.000	0.019	0.020
330	3504	6791	Access Link	5	30	7	0.80	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.001
302	5772	5923	Principal Arterial	5	27	6	1042.40	0.000	0.001	0.002	0.000	0.000	0.000	0.894	0.929
302	5772	6630	Collector	5	20	5	1343.00	0.000	0.001	0.002	0.000	0.000	0.000	1.216	1.263
303	5794	6650	Principal Arterial	5	35	8	6855.40	0.001	0.004	0.013	0.000	0.001	0.000	5.088	5.277
201	5813	5825	Minor Arterial	5	24	6	652.40	0.000	0.000	0.001	0.000	0.000	0.000	0.559	0.581
202	5813	5842	Minor Arterial	5	24	6	334.30	0.000	0.000	0.001	0.000	0.000	0.000	0.287	0.298
321	6656	6728	Ramp	4	50	11	27759.80	0.002	0.020	0.074	0.000	0.002	0.000	23.959	24.510
320	6657	6658	Ramp	4	20	5	597.10	0.000	0.001	0.002	0.000	0.000	0.000	0.680	0.712
320	6658	6763	Ramp	4	20	5	2347.40	0.000	0.002	0.008	0.000	0.001	0.000	2.674	2.798
308	6680	6676	Ramp	4	30	7	6339.20	0.001	0.005	0.020	0.000	0.001	0.000	6.558	6.812
308	6680	6716	Interstate	4	53	12	15287.10	0.001	0.011	0.038	0.000	0.001	0.000	12.837	13.100
308	6682	6715	Ramp	4	30	7	8165.00	0.001	0.007	0.026	0.000	0.001	0.000	8.447	8.774
308	6689	6715	Interstate	4	53	12	12779.00	0.001	0.009	0.032	0.000	0.001	0.000	10.731	10.951
300	6708	6619	Freeway	4	29	7	3001.80	0.000	0.002	0.009	0.000	0.001	0.000	3.106	3.226

ATTACHMENT C – CONSTRUCTION EMISSIONS ANALYSIS SAMPLE WORKSHEET

1) Construction Equipment MOVES-estimated Emissions Factors

Construction Equipment Emissions Factor-BMC Region

Anne Arundel County									
Construction Equipment Type	Load Factor	Horsepower (hp)	Emission Factor (grams/hp-hour)						
			VOC	NOx	CO	$PM_{2.5}$	PM_{10}	SO_2	CO_2
Asphalt paver, 130 HP	0.59	130	0.06	1.09	0.32	0.07	0.07	0.00	536.66
Backhoe loader w/ attachment	0.21	110	0.73	4.45	2.36	0.47	0.48	0.01	624.43
Centrif. water pump, 6"	0.43	33	0.29	3.51	1.05	0.18	0.19	0.00	589.53
Chain saws, 36"	0.59	9	73.06	1.53	266.03	8.97	9.75	0.00	686.00
Chipping machine	0.43	400	0.61	1.03	10.85	0.06	0.07	0.00	699.11
Compressor,600 cfm	0.43	300	0.15	2.49	0.72	0.11	0.11	0.00	530.60
Concrete pump, small	0.43	48	0.29	3.51	1.05	0.18	0.19	0.00	589.53
Crane, 90-ton	0.43	158	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Crane, hydraulic, 33 ton	0.43	173	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Crane, SP, 5 ton	0.43	49	0.12	2.69	0.40	0.05	0.05	0.00	590.01
Crane, 40 ton	0.43	152	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Diesel hammer, 41k ft-lb	0.43	39	0.18	3.04	0.65	0.11	0.12	0.00	589.84
Drill rig & augers	0.43	210	0.42	5.62	1.27	0.29	0.30	0.00	529.83
Dozer, 300 HP	0.59	300	0.06	1.06	0.40	0.06	0.06	0.00	536.67
Front end loader, 1.5 cy, crl	0.59	95	1.04	4.72	5.15	0.82	0.85	0.01	692.98
Front end loader, TM, 2.5cy	0.59	154	0.73	4.45	2.36	0.47	0.48	0.01	624.43
Gas engine vibrator	0.59	6	6.77	1.77	249.33	0.10	0.11	0.01	1047.06
Gas welding machine	0.21	23	4.85	1.72	250.08	0.11	0.12	0.01	1046.33
Grader, 30,000 lb	0.59	213	0.04	0.65	0.21	0.04	0.04	0.00	536.72
Hydraulic excavator, 3.5 cy	0.59	425	0.05	0.81	0.31	0.05	0.05	0.00	536.70
Pneumatic wheel roller	0.59	110	0.06	1.08	0.31	0.07	0.07	0.00	536.65
Roller, vibratory	0.59	20	0.35	3.77	1.50	0.17	0.17	0.01	595.14
Rollers, steel wheel	0.59	74	0.12	2.90	0.85	0.09	0.09	0.00	595.79
Tandem roller, 10 ton	0.59	74	0.12	2.90	0.85	0.09	0.09	0.00	595.79

Construction Equipment Emissions Factor-MWCOG Region

Prince George's County									
Construction Equipment Type	Load Factor	Horsepower (hp)	Emission Factor (grams/hp-hour)						
			VOC	NOx	CO	$PM_{2.5}$	PM_{10}	SO_2	CO_2
Asphalt paver, 130 HP	0.59	130	0.59	1.09	0.32	0.07	0.07	0.00	536.66
Backhoe loader w/ attachment	0.21	110	0.73	4.45	2.36	0.47	0.48	0.01	624.43
Centrif. water pump, 6"	0.43	33	0.29	3.51	1.05	0.18	0.19	0.00	589.53
Chain saws, 36"	0.59	9	73.07	1.53	266.03	8.97	9.75	0.00	686.00
Chipping machine	0.43	400	0.22	3.76	1.05	0.15	0.15	0.00	530.42
Compressor,600 cfm	0.43	300	0.15	2.49	0.72	0.11	0.11	0.00	530.60
Concrete pump, small	0.43	48	0.29	3.51	1.05	0.19	0.18	0.00	589.53
Crane, 90-ton	0.43	158	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Crane, hydraulic, 33 ton	0.43	173	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Crane, SP, 5 ton	0.43	49	0.12	2.69	0.40	0.05	0.05	0.00	590.01
Crane, 40 ton	0.43	152	0.07	1.14	0.23	0.06	0.06	0.00	530.85
Diesel hammer, 41k ft-lb	0.43	39	0.18	3.04	0.65	0.11	0.12	0.00	589.84
Drill rig & augers	0.43	210	0.42	5.62	1.27	0.29	0.30	0.00	529.84
Dozer, 300 HP	0.59	300	0.06	1.06	0.40	0.06	0.06	0.00	536.67
Front end loader, 1.5 cy, crl	0.59	95	1.04	4.72	5.15	0.82	0.85	0.01	692.97
Front end loader, TM, 2.5cy	0.59	154	0.73	4.45	2.36	0.47	0.48	0.01	624.43
Gas engine vibrator	0.59	6	5.52	2.68	249.35	0.10	0.11	0.01	1047.06
Gas welding machine	0.21	23	4.86	1.71	250.09	0.11	0.12	0.01	1046.33
Grader, 30,000 lb	0.59	213	0.04	0.65	0.21	0.04	0.04	0.00	536.72
Hydraulic excavator, 3.5 cy	0.59	425	0.05	0.81	0.31	0.05	0.05	0.00	536.70
Pneumatic wheel roller	0.59	110	0.06	1.08	0.31	0.07	0.07	0.00	536.65
Roller, vibratory	0.59	20	0.35	3.77	1.50	0.17	0.17	0.01	595.14
Rollers, steel wheel	0.59	74	0.12	2.90	0.85	0.09	0.09	0.00	595.79
Tandem roller, 10 ton	0.59	74	0.12	2.90	0.85	0.09	0.09	0.00	595.79

2) Sample Calculation - Construction Equipment Emission Rate Calculation for TMF in BMC Region

TMF - Anne Arundel County																			
Equipment Type	Number of Units	Days	Hours	Load Factor	Horsepower (hp)	Emission Factor (grams/hp-hour)							Emission Rate (tons)						
						VOC	NOx	CO	$PM_{2.5}$	PM_{10}	SO_2	CO_2	VOC	NOx	CO	$PM_{2.5}$	PM_{10}	SO_2	CO_2
Construction Equipment Emissions																			
Asphalt paver, 130 HP	1	111	666	0.59	130	0.059	1.091	0.319	0.072	0.074	0.004	536.7	0.00	0.06	0.02	0.00	0.00	0.00	30.19
Backhoe loader w/ attachment	1	31	186	0.21	110	0.735	4.450	2.363	0.469	0.484	0.005	624.4	0.00	0.02	0.01	0.00	0.00	0.00	2.95
Centrif. water pump, 6"	1	64	384	0.43	33	0.291	3.509	1.052	0.183	0.189	0.005	589.5	0.00	0.02	0.01	0.00	0.00	0.00	3.54
Chain saws, 36"	1	6	36	0.59	9	73.060	1.528	266.029	8.968	9.748	0.004	686.0	0.02	0.00	0.06	0.00	0.00	0.00	0.14
Chipping machine	1	3	18	0.43	400	0.607	1.030	10.855	0.064	0.069	0.004	699.1	0.00	0.00	0.04	0.00	0.00	0.00	2.38
Compressor,600 cfm	1	378	2268	0.43	300	0.152	2.490	0.724	0.110	0.114	0.004	530.6	0.05	0.80	0.23	0.04	0.04	0.00	170.97
Concrete pump, small	1	1135	6810	0.43	48	0.291	3.509	1.052	0.183	0.189	0.005	589.5	0.04	0.54	0.16	0.03	0.03	0.00	91.26
Crane, 90-ton	1	5615	33690	0.43	158	0.069	1.139	0.232	0.056	0.057	0.004	530.8	0.17	2.87	0.59	0.14	0.14	0.01	1338.17
Crane, hydraulic, 33 ton	1	40	240	0.43	173	0.069	1.139	0.232	0.056	0.057	0.004	530.8	0.00	0.02	0.00	0.00	0.00	0.00	10.44
Crane, SP, 5 ton	1	877	5262	0.43	49	0.122	2.685	0.398	0.045	0.047	0.004	590.0	0.01	0.33	0.05	0.01	0.01	0.00	72.04
Crane, 40 ton	1	2580	15480	0.43	152	0.069	1.139	0.232	0.056	0.057	0.004	530.8	0.08	1.27	0.26	0.06	0.06	0.00	591.52
Diesel hammer, 41k ft-lb	1	250	1500	0.43	39	0.180	3.037	0.654	0.112	0.116	0.004	589.8	0.00	0.08	0.02	0.00	0.00	0.00	16.34
Drill rig & augers	1	64	384	0.43	210	0.417	5.617	1.273	0.293	0.302	0.005	529.8	0.02	0.21	0.05	0.01	0.01	0.00	20.23
Dozer, 300 HP	1	101	606	0.59	300	0.057	1.062	0.400	0.056	0.058	0.004	536.7	0.01	0.13	0.05	0.01	0.01	0.00	63.40
Front end loader, 1.5 cy, crl	1	101	606	0.59	95	1.044	4.722	5.151	0.823	0.848	0.006	693.0	0.04	0.18	0.19	0.03	0.03	0.00	25.92
Front end loader, TM, 2.5cy	1	257	1542	0.59	154	0.735	4.450	2.363	0.469	0.484	0.005	624.4	0.11	0.69	0.36	0.07	0.07	0.00	96.35
Gas engine vibrator	1	920	5520	0.59	6	6.770	1.770	249.333	0.102	0.111	0.006	1047.1	0.15	0.04	5.37	0.00	0.00	0.00	22.53
Gas welding machine	1	615	3690	0.21	23	4.848	1.715	250.076	0.108	0.118	0.006	1046.3	0.10	0.03	4.91	0.00	0.00	0.00	20.54
Grader, 30,000 lb	1	507	3042	0.59	213	0.038	0.646	0.207	0.038	0.039	0.004	536.7	0.02	0.27	0.09	0.02	0.02	0.00	225.97
Pneumatic wheel roller	1	111	666	0.59	110	0.064	1.083	0.314	0.070	0.072	0.004	536.6	0.00	0.05	0.01	0.00	0.00	0.00	25.55
Roller, vibratory	1	101	606	0.59	20	0.354	3.766	1.502	0.166	0.172	0.005	595.1	0.00	0.03	0.01	0.00	0.00	0.00	4.69
Rollers, steel wheel	1	78	468	0.59	74	0.125	2.901	0.852	0.088	0.090	0.004	595.8	0.00	0.07	0.02	0.00	0.00	0.00	13.41
Tandem roller, 10 ton	1	72	432	0.59	74	0.125	2.901	0.852	0.088	0.090	0.004	595.8	0.00	0.06	0.02	0.00	0.00	0.00	12.38
Total Emissions													0.84	7.78	12.52	0.44	0.45	0.02	2860.91

3) Sample Calculation - Construction Vehicle Emission Rate Calculation for TMF in BMC Region

TMF - Anne Arundel County																	
Off Site Vehicle	Truck Millage	Emission Factor (lb/mi)								Emission Factor (tons)							
		VOC	NO_X	CO	$PM_{2.5}$	PM_{10}	SO_2	eCO_2	CO_2	VOC	NO_X	CO	$PM_{2.5}$	PM_{10}	SO_2	eCO_2	CO_2
Trucks	988313	0.0006	0.0049	0.0022	0.0003	0.0008	0.0000	2.9779	2.9722	0.31	2.43	1.11	0.16	0.37	0.01	1471.6	1468.7
Cars	3368900	0.0001	0.0002	0.0039	0.0000	0.0002	0.0000	0.8202	0.8189	0.16	0.37	6.55	0.05	0.26	0.01	1381.6	1379.4
Total motor vehicle emissions										0.47	2.80	7.66	0.21	0.64	0.01	2853.1	2848.1

Assumption

1. Offsite vehicles speed: 25 mph
2. Roadway type: Urban unrestricted
3. Off site trucks includes material delivery trucks, concrete trucks and dump trucks running 20 miles round trip
4. Passenger Car millage 20 miles round trip

TMF- Anne Arundel County																	
On Site Vehicle	Days	Total Hours	Emission Factor (lb/hr)								Emission Factor (tons)							
			VOC	NO_X	CO	$PM_{2.5}$	PM_{10}	SO_2	eCO_2	CO_2	VOC	NO_X	CO	$PM_{2.5}$	PM_{10}	SO_2	eCO_2	CO_2
Trucks	2782	8	0.01	0.08	0.04	0.01	0.02	0.00	43.61	43.48	0.14	0.86	0.39	0.07	0.19	0.00	485.3	483.8
Total motor vehicle emissions											0.14	0.86	0.39	0.07	0.19	0.00	485.3	483.8

Assumption

1. On site vehicles speed: 5 mph
2. On site trucks includes tractor trucks and water trucks running 8 hours a day

4) Total Construction Emissions (Equipment and Vehicle) for Each Construction Element Under Each Alternative

Total Construction Emissions (Equipment and Vehicle)-BMC (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-01	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.86	8.70	7.59	0.50	0.83	0.03	4,466.6
	Tunnel	6.13	50.25	23.16	3.16	7.38	0.13	30,082.3
	Total	***12.32***	***103.87***	***74.66***	***6.41***	***13.76***	***0.27***	***58,109.4***
J-02	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.74	7.44	6.50	0.42	0.71	0.02	3,823.4
	Tunnel	6.13	50.25	23.16	3.16	7.38	0.13	30,082.3
	Total	***12.20***	***102.62***	***73.56***	***6.34***	***13.64***	***0.27***	***57,466.2***
J-03	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.74	7.44	6.50	0.42	0.71	0.02	3,823.4
	Tunnel	6.13	50.25	23.16	3.16	7.38	0.13	30,082.3
	Total	***12.20***	***102.62***	***73.56***	***6.34***	***13.64***	***0.27***	***57,466.2***

Total Construction Emissions (Equipment and Vehicle)-BMC (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-04	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.82	8.25	7.21	0.47	0.79	0.03	4,237.9
	Tunnel	6.65	54.45	25.10	3.42	8.00	0.14	32,602.2
	Total	***13.31***	***113.26***	***77.97***	***6.97***	***14.89***	***0.29***	***62,288.4***
J-05	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.69	7.00	6.11	0.40	0.67	0.02	3,594.8
	Tunnel	6.65	54.45	25.10	3.42	8.00	0.14	32,602.2
	Total	***13.19***	***112.01***	***76.88***	***6.90***	***14.77***	***0.29***	***61,645.2***
J-06	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.33	19.69	9.01	1.24	2.82	0.05	12,085.8
	Viaduct	0.69	7.00	6.11	0.40	0.67	0.02	3,594.8
	Tunnel	6.65	54.45	25.10	3.42	8.00	0.14	32,602.2
	Total	***13.19***	***112.01***	***76.88***	***6.90***	***14.77***	***0.29***	***61,645.2***

Total Construction Emissions (Equipment and Vehicle)-BMC (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-01	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.59	5.98	5.22	0.34	0.57	0.02	3,073.0
	Tunnel	7.05	57.80	26.65	3.63	8.49	0.15	34,607.0
	Total	***13.27***	***111.18***	***76.90***	***6.88***	***14.97***	***0.29***	***62,751.2***
J1-02	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.46	4.65	4.06	0.26	0.44	0.01	2,387.0
	Tunnel	7.05	57.80	26.65	3.63	8.49	0.15	34,607.0
	Total	***13.13***	***109.84***	***75.73***	***6.81***	***14.84***	***0.28***	***62,065.1***
J1-03	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Cherry Hill)	1.41	12.94	11.32	0.75	1.33	0.02	4,730.5
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.46	4.65	4.06	0.26	0.44	0.01	2,387.0
	Tunnel	7.05	57.80	26.65	3.63	8.49	0.15	34,607.0
	Total	***13.13***	***109.84***	***75.73***	***6.81***	***14.84***	***0.28***	***62,065.1***

Total Construction Emissions (Equipment and Vehicle)-BMC

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-04	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.55	5.55	4.84	0.32	0.53	0.02	2,847.9
	Tunnel	7.57	62.03	28.60	3.90	9.11	0.16	37,138.1
	Total	***14.26***	***120.59***	***80.23***	***7.45***	***16.10***	***0.31***	***66,945.0***
J1-05	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.42	4.20	3.67	0.24	0.40	0.01	2,158.3
	Tunnel	7.57	62.03	28.60	3.90	9.11	0.16	37,138.1
	Total	***14.13***	***119.25***	***79.06***	***7.37***	***15.97***	***0.30***	***66,255.4***
J1-06	TMF	1.44	11.43	20.57	0.71	1.28	0.04	6,199.3
	Maintenance of Way Facility	0.13	0.83	2.98	0.05	0.12	0.00	530.8
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	14.1
	Station (Camden Yard)	1.94	18.56	13.09	1.07	1.89	0.03	6,618.3
	Shaft	2.63	22.16	10.14	1.40	3.17	0.06	13,596.5
	Viaduct	0.42	4.20	3.67	0.24	0.40	0.01	2,158.3
	Tunnel	7.57	62.03	28.60	3.90	9.11	0.16	37,138.1
	Total	***14.13***	***119.25***	***79.06***	***7.37***	***15.97***	***0.30***	***66,255.4***

Total Construction Emissions (Equipment and Vehicle) – MWCOG (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-01	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.44	4.42	3.85	0.25	0.42	0.01	2,252.8
	Tunnel	3.07	26.18	11.81	1.60	3.72	0.06	15,345.2
	Total	***5.45***	***48.66***	***26.52***	***2.93***	***6.31***	***0.12***	***26,952.1***
J-02	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.37	3.78	3.30	0.21	0.36	0.01	1,928.4
	Tunnel	3.07	26.18	11.81	1.60	3.72	0.06	15,345.2
	Total	***5.39***	***48.03***	***25.97***	***2.89***	***6.25***	***0.12***	***26,627.7***
J-03	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.37	3.78	3.30	0.21	0.36	0.01	1,928.4
	Tunnel	3.07	26.18	11.81	1.60	3.72	0.06	15,345.2
	Total	***5.39***	***48.03***	***25.97***	***2.89***	***6.25***	***0.12***	***26,627.7***

Total Construction Emissions (Equipment and Vehicle) – MWCOG (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-04	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.41	4.19	3.65	0.24	0.40	0.01	2,137.4
	Tunnel	3.32	28.37	12.80	1.74	4.04	0.07	16,630.6
	Total	***5.95***	***53.50***	***28.21***	***3.21***	***6.88***	***0.13***	***29,082.7***
J-05	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.35	3.55	3.10	0.20	0.34	0.01	1,813.0
	Tunnel	3.32	28.37	12.80	1.74	4.04	0.07	16,630.6
	Total	***5.89***	***52.86***	***27.66***	***3.18***	***6.82***	***0.13***	***28,758.3***
J-06	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.23	11.42	5.03	0.70	1.49	0.03	6,936.2
	Viaduct	0.35	3.55	3.10	0.20	0.34	0.01	1,813.0
	Tunnel	3.32	28.37	12.80	1.74	4.04	0.07	16,630.6
	Total	***5.89***	***52.86***	***27.66***	***3.18***	***6.82***	***0.13***	***28,758.3***

Total Construction Emissions (Equipment and Vehicle) – MWCOG (to be continued)

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-01	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.30	3.04	2.65	0.17	0.29	0.01	1,549.9
	Tunnel	3.53	30.11	13.59	1.84	4.28	0.07	17,653.3
	Total	***5.93***	***52.65***	***27.72***	***3.18***	***6.92***	***0.13***	***29,424.3***
J1-02	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.23	2.36	2.06	0.13	0.22	0.01	1,203.9
	Tunnel	3.53	30.11	13.59	1.84	4.28	0.07	17,653.3
	Total	***5.86***	***51.97***	***27.13***	***3.14***	***6.86***	***0.13***	***29,078.3***
J1-03	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Cherry Hill)	0.71	6.62	5.81	0.38	0.67	0.01	2,407.6
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.23	2.36	2.06	0.13	0.22	0.01	1,203.9
	Tunnel	3.53	30.11	13.59	1.84	4.28	0.07	17,653.3
	Total	***5.86***	***51.97***	***27.13***	***3.14***	***6.86***	***0.13***	***29,078.3***

Total Construction Emissions (Equipment and Vehicle) - MWCOG

Alternatives	*Elements*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-04	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.28	2.82	2.46	0.16	0.27	0.01	1,436.4
	Tunnel	3.79	32.32	14.58	1.98	4.60	0.08	18,944.4
	Total	***6.44***	***57.50***	***29.42***	***3.46***	***7.49***	***0.14***	***31,562.5***
J1-05	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.21	2.13	1.86	0.12	0.20	0.01	1,088.5
	Tunnel	3.79	32.32	14.58	1.98	4.60	0.08	18,944.4
	Total	***6.37***	***56.81***	***28.83***	***3.42***	***7.43***	***0.14***	***31,214.6***
J1-06	TMF	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Maintenance of Way Facility	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Road Replacement	0.00	0.03	0.02	0.00	0.00	0.00	10.3
	Station (Camden Yard)	0.98	9.49	6.71	0.54	0.95	0.02	3,368.2
	Shaft	1.39	12.85	5.66	0.78	1.68	0.04	7,803.2
	Viaduct	0.21	2.13	1.86	0.12	0.20	0.01	1,088.5
	Tunnel	3.79	32.32	14.58	1.98	4.60	0.08	18,944.4
	Total	***6.37***	***56.81***	***28.83***	***3.42***	***7.43***	***0.14***	***31,214.6***

5) Total Construction Emissions (Equipment and Vehicle) Per Construction Year

Total Construction Emissions (Equipment and Vehicle) by Construction Year – BMC (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-01	1	1.34	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	2.96	25.22	16.45	1.56	3.36	0.07	14,395.7
	3	2.83	23.85	16.18	1.47	3.19	0.06	13,432.8
	4	2.83	23.85	16.18	1.47	3.19	0.06	13,432.8
	5	1.52	12.58	9.79	0.78	1.69	0.03	6,930.2
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***12.32***	***103.87***	***74.66***	***6.41***	***13.76***	***0.27***	***58,109.4***
J-02	1	1.34	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	2.92	24.80	16.09	1.53	3.32	0.07	14,181.3
	3	2.79	23.43	15.82	1.45	3.15	0.06	13,218.4
	4	2.79	23.43	15.82	1.45	3.15	0.06	13,218.4
	5	1.52	12.58	9.79	0.78	1.69	0.03	6,930.2
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***12.20***	***102.62***	***73.56***	***6.34***	***13.64***	***0.27***	***57,466.2***
J-03	1	1.34	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	2.92	24.80	16.09	1.53	3.32	0.07	14,181.3
	3	2.79	23.43	15.82	1.45	3.15	0.06	13,218.4
	4	2.79	23.43	15.82	1.45	3.15	0.06	13,218.4
	5	1.52	12.58	9.79	0.78	1.69	0.03	6,930.2
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***12.20***	***102.62***	***73.56***	***6.34***	***13.64***	***0.27***	***57,466.2***

Total Construction Emissions (Equipment and Vehicle) by Construction Year – BMC (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-04	1	1.34	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	3.12	26.71	16.94	1.65	3.54	0.07	15,054.0
	3	3.08	26.04	16.99	1.60	3.48	0.07	14,511.2
	4	3.08	26.04	16.99	1.60	3.48	0.07	14,511.2
	5	1.70	14.21	10.41	0.88	1.88	0.04	7,664.9
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.31***	***113.26***	***77.97***	***6.97***	***14.89***	***0.29***	***62,288.4***
J-05	1	1.34	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	3.08	26.29	16.58	1.62	3.50	0.07	14,839.6
	3	3.03	25.62	16.63	1.58	3.44	0.07	14,296.8
	4	3.03	25.62	16.63	1.58	3.44	0.07	14,296.8
	5	1.70	14.21	10.41	0.88	1.88	0.04	7,664.9
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.19***	***112.01***	***76.88***	***6.90***	***14.77***	***0.29***	***61,645.2***
J-06	1	1.49	11.22	6.97	0.71	1.56	0.03	6,786.8
	2	3.08	26.29	16.58	1.62	3.50	0.07	14,839.6
	3	3.03	25.62	16.63	1.58	3.44	0.07	14,296.8
	4	3.03	25.62	16.63	1.58	3.44	0.07	14,296.8
	5	1.70	14.21	10.41	0.88	1.88	0.04	7,664.9
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.34***	***112.01***	***76.88***	***6.90***	***14.77***	***0.29***	***61,645.2***

Total Construction Emissions (Equipment and Vehicle) by Construction Year – BMC (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-01	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.17	26.80	16.81	1.66	3.63	0.07	15,440.6
	3	3.05	25.46	16.55	1.58	3.48	0.07	14,476.5
	4	3.05	25.46	16.55	1.58	3.48	0.07	14,476.5
	5	1.68	13.84	10.37	0.86	1.87	0.04	7,684.4
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.27***	***111.18***	***76.90***	***6.88***	***14.97***	***0.29***	***62,751.2***
J1-02	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.13	26.36	16.42	1.64	3.59	0.07	15,211.9
	3	3.01	25.02	16.16	1.55	3.44	0.06	14,247.8
	4	3.01	25.02	16.16	1.55	3.44	0.06	14,247.8
	5	1.68	13.84	10.37	0.86	1.87	0.04	7,684.4
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.13***	***109.84***	***75.73***	***6.81***	***14.84***	***0.28***	***62,065.1***
J1-03	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.13	26.36	16.42	1.64	3.59	0.07	15,211.9
	3	3.01	25.02	16.16	1.55	3.44	0.06	14,247.8
	4	3.01	25.02	16.16	1.55	3.44	0.06	14,247.8
	5	1.68	13.84	10.37	0.86	1.87	0.04	7,684.4
	6	0.48	4.09	5.55	0.24	0.44	0.01	1,846.7
	7	0.35	3.07	3.53	0.18	0.32	0.01	1,284.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***13.13***	***109.84***	***75.73***	***6.81***	***14.84***	***0.28***	***62,065.1***

Total Construction Emissions (Equipment and Vehicle) by Construction Year - BMC

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-04	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.33	28.30	17.30	1.75	3.82	0.07	16,102.0
	3	3.29	27.66	17.37	1.71	3.76	0.07	15,559.8
	4	3.29	27.66	17.37	1.71	3.76	0.07	15,559.8
	5	1.85	15.48	10.99	0.96	2.07	0.04	8,420.8
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***14.26***	***120.59***	***80.23***	***7.45***	***16.10***	***0.31***	***66,945.0***
J1-05	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.28	27.85	16.91	1.73	3.77	0.07	15,872.2
	3	3.25	27.22	16.98	1.68	3.72	0.07	15,330.0
	4	3.25	27.22	16.98	1.68	3.72	0.07	15,330.0
	5	1.85	15.48	10.99	0.96	2.07	0.04	8,420.8
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***14.13***	***119.25***	***79.06***	***7.37***	***15.97***	***0.30***	***66,255.4***
J1-06	1	1.49	12.45	7.54	0.78	1.74	0.03	7,542.2
	2	3.28	27.85	16.91	1.73	3.77	0.07	15,872.2
	3	3.25	27.22	16.98	1.68	3.72	0.07	15,330.0
	4	3.25	27.22	16.98	1.68	3.72	0.07	15,330.0
	5	1.85	15.48	10.99	0.96	2.07	0.04	8,420.8
	6	0.57	5.03	5.84	0.30	0.53	0.01	2,161.3
	7	0.44	4.01	3.83	0.24	0.42	0.01	1,599.0
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***14.13***	***119.25***	***79.06***	***7.37***	***15.97***	***0.30***	***66,255.4***

Total Construction Emissions (Equipment and Vehicle) by Construction Year – MWCOG (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-01	1	0.62	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.39	12.66	6.74	0.76	1.62	0.03	7,180.4
	3	1.29	11.31	6.19	0.68	1.49	0.03	6,269.8
	4	1.29	11.31	6.19	0.68	1.49	0.03	6,269.8
	5	0.63	5.47	2.94	0.33	0.73	0.01	2,961.4
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.45***	***48.66***	***26.52***	***2.93***	***6.31***	***0.12***	***26,952.1***
J-02	1	0.62	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.37	12.44	6.55	0.75	1.60	0.03	7,072.3
	3	1.27	11.10	6.01	0.67	1.47	0.03	6,161.7
	4	1.27	11.10	6.01	0.67	1.47	0.03	6,161.7
	5	0.63	5.47	2.94	0.33	0.73	0.01	2,961.4
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.39***	***48.03***	***25.97***	***2.89***	***6.25***	***0.12***	***26,627.7***
J-03	1	0.62	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.37	12.44	6.55	0.75	1.60	0.03	7,072.3
	3	1.27	11.10	6.01	0.67	1.47	0.03	6,161.7
	4	1.27	11.10	6.01	0.67	1.47	0.03	6,161.7
	5	0.63	5.47	2.94	0.33	0.73	0.01	2,961.4
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.39***	***48.03***	***25.97***	***2.89***	***6.25***	***0.12***	***26,627.7***

Total Construction Emissions (Equipment and Vehicle) by Construction Year – MWCOG (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J-04	1	0.62	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.47	13.42	6.99	0.81	1.71	0.03	7,516.3
	3	1.41	12.44	6.61	0.75	1.64	0.03	6,820.0
	4	1.41	12.44	6.61	0.75	1.64	0.03	6,820.0
	5	0.72	6.32	3.26	0.38	0.83	0.01	3,335.7
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.95***	***53.50***	***28.21***	***3.21***	***6.88***	***0.13***	***29,082.7***
J-05	1	0.62	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.45	13.21	6.80	0.80	1.69	0.03	7,408.1
	3	1.39	12.23	6.42	0.74	1.62	0.03	6,711.8
	4	1.39	12.23	6.42	0.74	1.62	0.03	6,711.8
	5	0.72	6.32	3.26	0.38	0.83	0.01	3,335.7
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.89***	***52.86***	***27.66***	***3.18***	***6.82***	***0.13***	***28,758.3***
J-06	1	0.69	5.71	2.51	0.35	0.75	0.02	3,468.1
	2	1.45	13.21	6.80	0.80	1.69	0.03	7,408.1
	3	1.39	12.23	6.42	0.74	1.62	0.03	6,711.8
	4	1.39	12.23	6.42	0.74	1.62	0.03	6,711.8
	5	0.72	6.32	3.26	0.38	0.83	0.01	3,335.7
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.97***	***52.86***	***27.66***	***3.18***	***6.82***	***0.13***	***28,758.3***

Total Construction Emissions (Equipment and Vehicle) by Construction Year – MWCOG (to be continued)

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-01	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.50	13.57	6.95	0.82	1.76	0.04	7,764.3
	3	1.40	12.16	6.39	0.73	1.64	0.03	6,804.9
	4	1.40	12.16	6.39	0.73	1.64	0.03	6,804.9
	5	0.71	6.13	3.24	0.37	0.83	0.01	3,346.1
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.93***	***52.65***	***27.72***	***3.18***	***6.92***	***0.13***	***29,424.3***
J1-02	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.48	13.34	6.75	0.81	1.74	0.03	7,648.9
	3	1.37	11.94	6.19	0.72	1.62	0.03	6,689.6
	4	1.37	11.94	6.19	0.72	1.62	0.03	6,689.6
	5	0.71	6.13	3.24	0.37	0.83	0.01	3,346.1
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.86***	***51.97***	***27.13***	***3.14***	***6.86***	***0.13***	***29,078.3***
J1-03	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.48	13.34	6.75	0.81	1.74	0.03	7,648.9
	3	1.37	11.94	6.19	0.72	1.62	0.03	6,689.6
	4	1.37	11.94	6.19	0.72	1.62	0.03	6,689.6
	5	0.71	6.13	3.24	0.37	0.83	0.01	3,346.1
	6	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	7	0.12	1.10	0.97	0.06	0.11	0.00	401.3
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***5.86***	***51.97***	***27.13***	***3.14***	***6.86***	***0.13***	***29,078.3***

Total Construction Emissions (Equipment and Vehicle) by Construction Year - MWCOG

Alternatives	*Construction Year*	*Emission (tons)*						
		VOC	*NO_x*	*CO*	*$PM_{2.5}$*	*PM_{10}*	*SO_2*	*CO_2*
J1-04	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.58	14.34	7.20	0.87	1.85	0.04	8,101.7
	3	1.52	13.30	6.80	0.80	1.78	0.03	7,357.5
	4	1.52	13.30	6.80	0.80	1.78	0.03	7,357.5
	5	0.80	6.97	3.55	0.42	0.93	0.02	3,721.3
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***6.44***	***57.50***	***29.42***	***3.46***	***7.49***	***0.14***	***31,562.5***
J1-05	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.56	14.11	7.00	0.85	1.83	0.04	7,985.8
	3	1.50	13.07	6.60	0.79	1.76	0.03	7,241.6
	4	1.50	13.07	6.60	0.79	1.76	0.03	7,241.6
	5	0.80	6.97	3.55	0.42	0.93	0.02	3,721.3
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***6.37***	***56.81***	***28.83***	***3.42***	***7.43***	***0.14***	***31,214.6***
J1-06	1	0.69	6.42	2.83	0.39	0.84	0.02	3,901.6
	2	1.56	14.11	7.00	0.85	1.83	0.04	7,985.8
	3	1.50	13.07	6.60	0.79	1.76	0.03	7,241.6
	4	1.50	13.07	6.60	0.79	1.76	0.03	7,241.6
	5	0.80	6.97	3.55	0.42	0.93	0.02	3,721.3
	6	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	7	0.16	1.58	1.12	0.09	0.16	0.00	561.4
	8	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	Total	***6.37***	***56.81***	***28.83***	***3.42***	***7.43***	***0.14***	***31,214.6***