

TEST SPECIFICATION #7115  
FOR  
SWITCHYARD IMPACT TESTS (RPI-AAR PHASE 15)

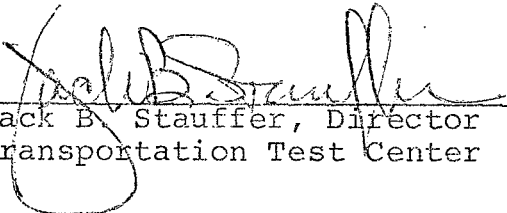
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September 19, 1975

Revised:


November 4, 1975

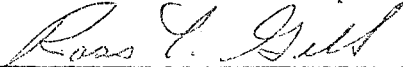
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## TRANSPORTATION TEST CENTER

### COMMONLY USED ACRONYMS

AAR	Association of American Railroads
COTR	Contracting Officer's Technical Representative
CP	Check Pilot
CSB	Center Services Building
CTE	Chief Test Engineer
DOT	Department of Transportation
FRA	Federal Railroad Administration
HA	Hazard Area
HEO	Hazards Evaluation Officer
MOU	Memo-of-Understanding
OCC	Operations Control Center
O&M	Operations and Maintenance
OTP	Operation Test Procedure
PM	Program Manager
PMB	Project Management Building
PSO	Power Station Operator
RDL	Rail Dynamics Laboratory
RPI	Railway Progress Institute
RTTT	Rapid Transit Test Track
SMB	Storage & Maintenance Building
SO	Safety Officer
SOA	Sponsoring Operating Administration
SOP	Standard Operating Procedures
TC	Test Controller

COMMONLY USED ACRONYMS (Continued)

TDT        Train Dynamics Track  
TMB        Transit Maintenance Building  
TSO        Track Security Officer  
TSC        Transportation Systems Center  
TSE        Test Support Engineer  
TTC        Transportation Test Center  
UMTA       Urban Mass Transportation Administration  
VO        Vehicle Operator

1.0 GENERAL

1.1 INTRODUCTION

1.2 TEST OBJECTIVES

1.3 REFERENCE DOCUMENTS

1.4 PROGRAM PARTICIPANTS AND RESPONSIBILITIES

# T E S T   S P E C I F I C A T I O N

## SWITCHYARD IMPACT TESTS

### 1.0 GENERAL

#### 1.1 INTRODUCTION

A research project began at Washington University, St. Louis, Missouri on March 1, 1974 with the principle objective to develop a rational basis for designing devices suitable for the protection of hazardous material tank cars from head puncture in switchyard impact and on line derailment situations. The first goal of this project was to acquire an understanding of head puncture mechanisms and, through this understanding, to estimate the direction and magnitude of coupler forces (as time functions) in critical situations. Studies of accident reports lead to the conclusion that puncture mechanisms involve excessive pitching, motion of cars excited by longitudinal coupler forces. A mathematical model, capable of simulating such pitching motion, has been developed. Following a series of test runs, three actual accidents, known as the East St. Louis, Decatur and Houston accidents, were simulated. On the basis of this simulation, it was concluded the sequence of events in the East St. Louis accident was different from the previously assumed events. This underlines the importance of quantitative studies of each accident occurrences.

The quantitative approach requires that the dynamic parameters of train consists be known with reasonable accuracy. Some of the parameters can be measured readily, others, such as



the response of draft gears and ladings to forces applied in rapid succession, require additional experimental and theoretical work. Simulation of the East St. Louis, Decatur and Houston accidents was based on best available estimate of the parameters. In order to verify the model a series of impact tests are to be conducted under controlled conditions.

## 1.2 TEST OBJECTIVES

The series of impacts will consist of two parts; tests and analysis. The analytical part will be accomplished by Washington University. RPI/AAR will provide inputs as mutually deemed appropriate.

The major portion of the program will be conducted at the Transportation Test Center (TTC), Pueblo, Colorado. This portion will be a series of impact tests involving the striking of an empty hopper car with Class 112A or 114A tank cars loaded with water to simulate LPG. A maximum of eleven series of tests will be conducted. Some may be eliminated, depending on results from others. In most of these eleven series, impacts will be at increasing increments of speed until either a puncture occurs or the damage is destructive.

All data will be reduced and used to study the specific problem of head punctures occasioned by on-track impacts of loaded tank cars into an empty hopper car and to determine

the probable effectiveness of the shelf coupler, the head shield, or both in combination, toward preventing punctures. The influence of the number of impacting cars and cars backing up the impacted car will also be studied.

### 1.3 REFERENCE DOCUMENTS

The following reference documents were used to compile this Test Specification for performance of this test program:

- a. Switchyard Impact Tests - Full Scale by RPI/AAR, July 18, 1975.
- b. Test Plan for Switchyard Impact Tests (RPI/AAR Phase 15) May 20, 1975 (TTC Document).
- c. Full Scale Controlled Velocity Switchyard Impact Tests. Test and Instrumentation Specification August 6, 1975 (Washington University Document).
- d. Minutes of Meeting on Full Scale Switchyard Impact Tests, TTC August 5 and 6, 1975.

### 1.4 PROGRAM PARTICIPANTS AND RESPONSIBILITIES

1.4.1 The following personnel will be participating in this test project:

RPI/AAR (Railroad Tank Car Safety Research and Test Project

Earl Phillips

Larry Schlink

John Everett

E. J. Kunz

L. L. Olson

FRA-Washington:

L. Peterson, RRD-30

D. Levine, RRD-33

D. Dancer, RRD-33

TTC-FRA-Pueblo:

J. Stauffer

H. Smith

R. Gill

TTC-O&M:

Keith Kieres

J. Johnson

Transportation Systems Center:

Pin Tong

Washington University:

B. Szabo

W. Diboll

D. Peters

1.4.2 Organizational Responsibilities:

<u>Responsibilities</u>	<u>Organization</u>	<u>Individual</u>
Overall test planning, management and fueling	FRA/RPI/AAR	D. Levine, FRA L. Schlink, RPI/AAR
Technical support and design of experiments	Washington U.	D. Peters
Technical Advisor to FRA	TSC	P. Tong
Conduct of tests	TTC	R. Gill

1.4.2 Continued

- a. Don Levine will be FRA Test Director for the Phase 15 Switchyard Impact Tests and will serve as point of contact between the SOA (FRA) and the TTC Test Controller. David Dancer, FRA, will serve as his alternate. In addition, Mr. Levine, or his alternate will be responsible for insuring that DOT/FRA and RPI/AAR objectives and goals for the conduct of these tests are indeed fulfilled.
- b. L. J. Schlink will be the RPI/AAR Phase leader, and it will be his responsibility to insure that the RPI/AAR commitments to this program are fulfilled in an orderly manner, test data suitable to the RPI/AAR is obtained, and any conflict regarding the conduction of the test and changes in the test program are resolved to the mutual satisfaction of the RPI/AAR and the DOT.  
J. E. Everett, E. L. Kunz, and/or L. L. Olson will serve as alternates.
- c. David Peters, representing Washington University, will provide technical support and planning for the tests. He will be responsible for insuring that the design of the tests and the acquisition and analysis of the data are performed in such a manner that the test results provide accurate and relevant information for improving tank car safety.

- d. Ross Gill, Rail Operations Test Controller, will be the Transportation Test Center Test Controller (TC) and will be the TTC interface on these tests for all program participants.
- e. Harry Smith, TTC Hazards Evaluation Officer, will ensure that the TTC Safety Policies and Procedures are complied with.
- f. Keith Kieres, Kentron Hawaii, Ltd. (KHL), will act as Chief Test Engineer (CTE). The Test Project Manager will be named at a later date.
- g. Ron Begier, Kentron Hawaii, Ltd., will be the TTC Test Support Engineer (TSE).

#### 1.4.3 Pre-test Acceptance

In order to provide complete agreement by all parties prior to the conduct of tests representatives of the cognizant organizations will be at TTC 24 hours prior to the commencement of a test series (preliminary tests also) for final inspection of equipment and instrumentation set up. The TTC will notify all parties 7 days in advance of such tests as best can be projected. Should personnel from participating parties not be available, notification in writing or telephone must be conveyed to TTC. The following groups should be represented:

- RPI/AAR - Any Phase 15 team member.
- FRA - Representatives from OR&D Office of Rail Safety Research.
- TTC - Test team as required for conduct of tests.
- Washington University - D. Peters, of Washington University

#### 1.4.4 Distribution List

All modification or changes to this Specification will be distributed by TTC to the following personnel:

Mr. Dave Dancer  
Federal Railroad Administration  
Rail Vehicle Safety Research Div., RRD-33  
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Washington, D.C. 20590 7 copies

Mr. Pin Tong  
Transportation Systems Center  
Mail Code 612  
Kendall Square  
Cambridge, MA 02142 2 copies

Dr. W. J. Harris, Jr.  
Vice President  
Research and Test Department  
Association of American Railroads  
American Railroads Building  
1920 L Street, N.W.  
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Mr. Ross T. Gill  
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Transportation Test Center  
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Mr. E. L. Kunz  
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Ruston, Louisiana 71270 1 copy

Mr. Earl A. Phillips  
AAR Technical Center  
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Chicago, Illinois 60616 1 copy

#### 1.4.5 Major Responsibility Outline

##### DOT-TTC

##### RPI/AAR

- |   |   |
|---|---|
| a. The Test Site  | a. Provide 28 Tank Cars.  |
| b. Pre-Test Measurements  | b. Preparation of the 28 Tank Cars (re-spring trucks, apply shelf couplers and head shields). |
| c. Test Instrumentation and all Photo Coverage.   | c. Procurements and disposal of empty hopper cars which will be impacted.                     |
| d. Conduction of Test   | d. Movement of tank and hopper cars to Avondale.  |
| e. Repairing Test Site between and after all tests.   | e. Movement of tank cars from Avondale to repair shops.                                       |
| f. Tank car and back-up car lading.   | f. Two Technician/Engineers for duration of testing.  |
| g. Furnish 3 loaded back cars and their disposal.   | g. Periodic Fatigue Inspection of tank cars used in testing.                                  |
| h. Filling, emptying and transferring Tank Car Lading.  |   |
| i. Transportation of all cars from North Avondale into the Test Center.                                 |   |
| j. Return of tank cars to North Avondale in suitable condition for rail transportation to repair shops. |   |
| k. Suitable locomotive for conducting tests.  |   |
| l. Suitable equipment for handling and removing damaged cars.   |   |
| m. Disposal of tank car lading.   |   |
| n. Provisions for pressurizing tank cars.   |   |
| o. Recording and reduction of Test Data.  |   |
| p. Means for assuring coupler impacts head in Test Series No. 8.  |   |
| q. Arrangements for scraping cars.  |   |



1.4.6 Checklist - Phase 15

ITEM	RESPONSIBILITY	DATE	REMARKS
1. Overall Test Coordinator	D. Dancer (LJS)		
2. Prepare Test Program	LJS (DMD)		
3. Prepare Test Schedule	LJS (DMD)		
4. Instrumentation Plan & Sketch	FRA		
5. Drawings & Specifications for Tank Cars	LJS JEE		
6. Drawings & Specifications for Hopper Cars	LJS (JEE)		
7. Prepare List of RPI-AAR Mat'ls & Equipment for Test Site	LJS (JEE)		Dynamometer Coupler
8. Ship Materials & Equipment to Test Site	(Later)		
9. Procurement of 28 Hopper Cars	EAP (LJS)		Contract arrangements
10. Advise Transition temperatures	RPI-AAR		
11. Heating Tank Cars Loaded with Water	FRA (RTG)		
12. Inspect Hopper Cars after arrival at No. Avondale	RPI-AAR		See Section 11.
13. Procurement and Disposal of 5 Back-Up Hopper Cars	FRA		
14. Order "E" Shelf Couplers	EAP		
15. Order "F" Shelf Couplers	EAP		
16. Manufacture Head Shields	(later)		
17. Write Procedure for Pressurizing Tank Cars	CER		
18. Provide Appropriate Equipment for Pressurizing Tank Cars	FRA		
19. Velocity Control	LJS		Check FRA Procedure
20. Inspection of 26 Tank Cars Before Release to North Avondale	UTC (LJS) GAT (JEE)		
21. Free Car Movements			

1.4.6 Checklist - Phase 15 (Continued)

ITEM	RESPONSIBILITY	DATE	REMARKS
22. Arrange Shipment of 28 Tank Cars to North Avondale	UTC (LJS) GAT (JEE)		
23. Coordinate Hopper Car Movement to North Avondale with Shipper	LLO (LJS) (JEE)		
24. Personnel Clearances and Visitors Arrangements, All Tests	EAP (DMD)		Notify EAP who will be there and when -contact: R. Gill or K. Grunwald
25. Notify Interested Parties Who Wish to Witness Test(s)	EAP (DMD)		T. Chastain; N. Morella; H. L. Scott, Jr. (NW)
26. Movement of Tank and Hopper Cars from North Avondale to Test Site	FRA		
27. Represent RPI-AAR at Test Site	AAR (LLO) ACF (ELK) GAT (JEE) UTC (LJS)		
28. Inspection of 26 Tank Cars After Arrival at Test Site	RPI-AAR		
29. Instrument Cars	FRA		
30. Pre-Test Measurements	FRA		
31. Tank Car Lading	FRA		
32. Furnish and ship - one (1) Dynamometer Coupler (E)	UTC (LJS)		FRA to return to Miner Enterprises
33. Lading for Back-Up Hopper Cars	FRA		Five (5) hopper cars to be loaded at TTC.
34. Fill, Empty, Transfer and/or Dispose of Test Lading	FRA		
35. Locomotive for Test	FRA		
36. Suitable Track	FRA		
37. Equipment for Handling and Removing Damaged Cars	FRA		
38. Velocity Measurements Before and After All Impacts	FRA		
39. Coupler Force(s) All Tests	FRA		

1.4.6 Checklist - Phase 15 (Continued)

ITEM	RESPONSIBILITY	DATE	REMARKS
40. Conduct Test	FRA		
41. Movies of All Tests	FRA		
42. Repair Test Site	FRA		
43. Design Means for Discontinuity Tear	RPI-AAR (FRA)		Contingency Test
44. Provide Means for Discontinuity Tear	FRA		Contingency Test
45. Record & Reduce Test Data	FRA		
46. Post Test Inspection			
47. Procurement of Parts Required to Return Tank Cars	FRA (RPI-AAR)		Includes gondolas or flat cars as may be necessary
48. Cost of Parts Required to Return Tank Cars	FRA		Includes gondolas or flat cars as may be necessary
49. Cut Stencil for Tank Cars "Home for Repairs. Do Not Load Until Repaired."	RPI-AAR		Rule 95 B.g. (3)
50. Stencil Tank Cars "Home for Repairs. Do Not Load Until Repaired."	FRA		Rule 95 B.g.(3)
51. Shipment of Tank Cars from Test Site to North Avondale	FRA		
52. Shipment of Tank Cars from North Avondale to Repair Shops	GAT (JEE) UTC (LJS)		
53. Preparation and Movement of Hopper Cars for Disposal After Test	FRA		
54. Disposal of Hopper Cars After Test	RPI-AAR		Proceeds of sale to AAR.
55. Write Test Report	RPI-AAR, FRA		Individual Reports
56. 2 - 20,000 gal. 111-A Cars with Bottom Outlets	RPI-AAR		Additional Impacting Cars.
57. Mechanical Trip Valve	FRA		May be Used When No Back-Up Hopper Cars Involved.

2.0 TEST REQUIREMENTS

## 2.0 TEST REQUIREMENTS

Conditions common to all tests are:

2.1 All struck and striking cars to be resprung and rebuilt to mechanical and structural condition as necessary for test purposes.

### 2.2 Struck Cars:

- a. Cars to be 50-ton steel open top hopper cars.
- b. Cars to have a light weight not greater than 44,000 pounds.
- c. Car truck centers to be approximately 30 feet.
- d. Cars to be equipped with conventional draft gear and standard E couplers.
- e. Couplers will be extended on butt end to normal operating length, in accordance with AAR "Manual of Standards and Recommended Practices" Spec. M-204A-68 Fig. 8, so the draft gear will bottom prior to the horn hitting the striker plate.
- f. All cars to be of the same type for all tests.

### 2.3 Striking Cars:

- a. Cars to be nominal 33,000 gallon class DOT 112A or DOT 114A tank cars. Where three striking tank cars are required, only the lead car must conform to 2.3 requirements.
- b. The diameter and thickness to be the same for all cars.
- c. The same type or same AAR rated draft gear in each car is preferred.
- d. Cars to be generally identical for all tests.
- e. Cars to be equipped with grade "C" couplers.

## 2.4 Test Conditions

- a. Strking couplers to be "in-line" laterally, knuckles to be opened by decoupling from struck cars. Insure coupler pin is free to fall on impact.
- b. The internal pressure in the striking tank car(s) for test series, all tests, to be 100 psig.
- c. The striking car(s) to be loaded with water to a volume established by preliminary tests.
- d. Water in striking car to be such that the head temperature on the outside of the car will be at least 60° F. immediately before impact for test series 1 thru 11.

## T E S T M A T R I X

Refer to Operational Sequence Diagram, Figure B-2, Blocks 27, 28, and 29.

Series	Impacting Cars	Back Up Cars	Head Shields	Type Coupler Tank Car	R E M A R K S
Preliminary Tests	1	0	NO	E	Effects of surging, liquid lading 62.7, 75 and 94.6% full, 4, 6 & 8 mph impacts.  Braking of cars to occur after data acquisition. 100 psi in tank. Coupler lever to be tied to prevent coupling.
1	1	0	NO	E (Std)	(Uncoupling effect) Impact at 4 mph and increase in 2 mph increments to destructive damage. Duplicate velocities up to uncoupling velocity.
2	1	3	NO	E (Std)	Starting at speed at which no coupling occurs, repeat with backup cars placed in positions determined from series #1, to include maximum coupler elevation on 3rd impact, (override).
3	1	3	YES	E (Std)	Effectiveness of Head Shield (if shields available at this time)
4	1	3	NO	F (Std)	Effectiveness of F Standard Coupler
5	1	3	NO	E Shelf	Effectiveness of E Shelf Coupler
6	1	3	NO	F Top Shelf	Effectiveness of F Top Shelf (DOT Request)
7	1	3	YES	E (Std)	Contingency Test
8	1	3	YES	E Shelf	Effectiveness of Shield and E Shelf Coupler Combination
9	3	3	YES	E (Std)	Effect of Impacting Car Consist
10	3	3	NO	E (Std)	Effect of Impacting Car Consist
11	1	0	NO	E (Std)	Cut lever on and off. Knuckles open and closed. Four mph in 2 mph increments to 10 mph maximum or failure to couple.

Figure A-1

PRE-TEST MEASUREMENT SCHEDULE

PRE-TEST MEASUREMENT	TANK CAR #1	TANK CAR #2	HOPPER CAR #1	HOPPER CAR #2	HOPPER CAR #3
Delivery to TTC	29 July 1975	10 Sept 1975	25 Aug 1975	25 Aug 1975	25 Aug 1975
Total Weight Truck Weight	27 Aug 1975	2 Sept 1975	2 Sept 1975	2 Sept 1975	2 Sept 1975
Length Between Coupler Faces Length Between Truck Centers Vertical Play at Sill Vertical Play at Coupler Coupler Height Above Rail	8-10 Sept 1975	8-10 Sept 1975	8-10 Sept 1975	8-10 Sept 1975	8-10 Sept 1975
Travel of Truck Center Plate and Pins to Release Vertical Spring Rates and Deflection Curves	29 Sept-3 Oct	NR	6-10 Oct 1975	NR	NR
Force Deflection Plot during and after Bottoming of Truck Springs to 400 kips	22-26 Sept 1975	NR	29 Sept-3 Oct	NR	NR
Locate Center of Gravity Determine Moment of Inertia	NR	NR	17-19 Sept 1975	NR	NR
Frequency and Damping of Car on Trucks	NR	NR	13-15 Oct 1975	NR	NR
Travel of Truck Bolsters to Spring Bottom and Up to Hitting Side Frame	22-26 Sept 1975	NR	29 Sept-3 Oct	NR	NR
Car to Car Impacts	16-17 Oct 1975	16-17 Oct 1975	14-15 Oct 1975	14-15 Oct 1975	NR

Figure A-2



FULL SCALE CONTROLLED VELOCITY SWITCHYARD IMPACTS TEST SCHEDULE

PRELIMINARY TESTS: 20 - 31 October 1975  
DATA REDUCTION: 3 - 14 November 1975

TEST SERIES &  
DATA REDUCTION  
(two weeks each)

TEST SERIES 1: 17 November - 12 December 1975  
TEST SERIES 2: 15 December - 16 January 1976  
TEST SERIES 3: 19 January - 13 February 1976  
TEST SERIES 4: 16 February - 12 March 1976  
TEST SERIES 5: 15 March - 9 April 1976  
TEST SERIES 6: 12 April - 7 May 1976  
TEST SERIES 7: 10 May - 4 June 1976  
TEST SERIES 8: 7 June - 2 July 1976  
TEST SERIES 9: 6 July - 30 July 1976  
TEST SERIES 10: 2 August - 27 August 1976  
TEST SERIES 11: 30 August - 17 September 1976

DRAFT REPORT: 20 September - 10 October 1976

NOTE: Required cars furnished by RPI/AAR to be on site one week prior to start dates shown for each test.

# OPERATIONAL SEQUENCE DIAGRAM

ALL CARS AS THEY ARRIVE

---

WEIGHT, LENGTH BETWEEN COUPLER FACES, LENGTH BETWEEN TRUCK CENTERS, COUPLER HEIGHT ABOVE RAILS, VERTICAL COUPLER SLACK.

FIRST HOPPER CAR

---

TRUCK WEIGHT, BODY WEIGHT, CENTER OF GRAVITY, MOMENT OF INERTIA, STRAIN GAUGE TRUCK BOLSTER, STRAIN GAUGE COUPLER SHANK, STRAIN GAUGE CENTER SILL, ACCELEROMETER ON CENTER SILL.

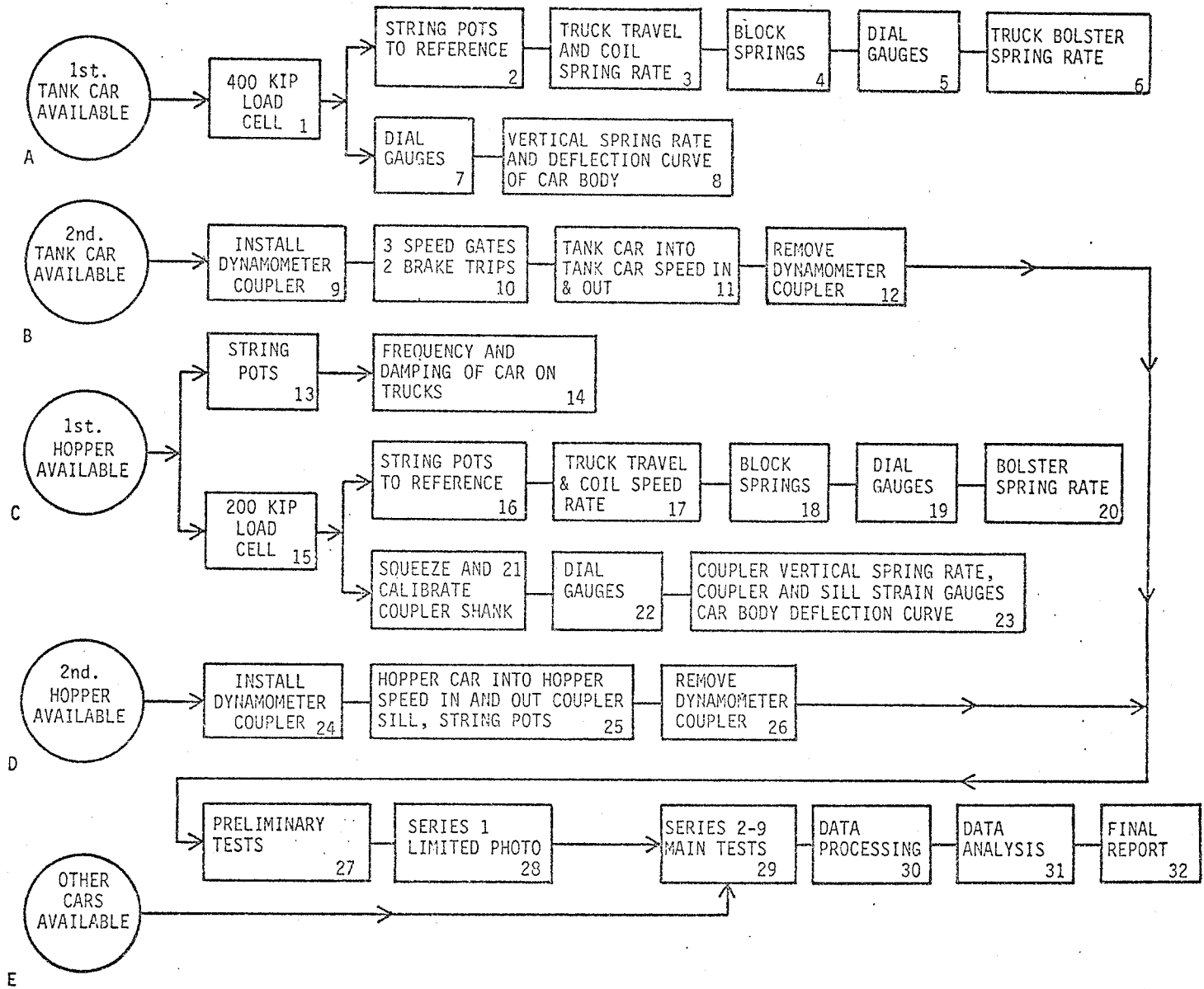


Figure B-2

3.0 PHOTO COVERAGE REQUIREMENTS

3.1 PRELIMINARY TESTS

3.2 TEST SERIES 1

3.3 TEST SERIES 2 THROUGH 9

### 3.0 PHOTOGRAPHIC INSTRUMENTATION TEST COVERAGE

#### 3.1 PRELIMINARY TESTS

Preliminary test will be covered by still photographs to document the pertinent facts for this test. Two cameras, 1 - 500 FPS and 1 - Real Time, will be placed to monitor sloshing effect; 90° to impact, to cover tank car and hopper car for a minimum of 25 feet after impact.

#### 3.2 TEST SERIES 1

- a. Four high speed movie cameras (500 FPS) to be placed as shown in Figure C-1.
- b. Two CCTV cameras to be used to monitor and record data for instant replay as shown in Figure C-1.
- c. Each pair of tests at a common impact speed will be photographed on the same roll of film where possible.
- d. Color negatives will be taken for color prints, and 35mm color slides will be taken to document pre-test work, camera and other instrumentation device locations.

#### 3.3 TEST SERIES 2 THROUGH 9

- a. Test series 2 through 9 will have full camera and CCTV coverage as shown in Figure C-1.
- b. Final camera positions will be determined by inspection of the test vehicles on sight.
- c. Light colored paint and possible use of auxiliary lights will be used to enhance the photography for close-in coupler height impacts.

CAMERA LOCATION MATRIX

← Motion

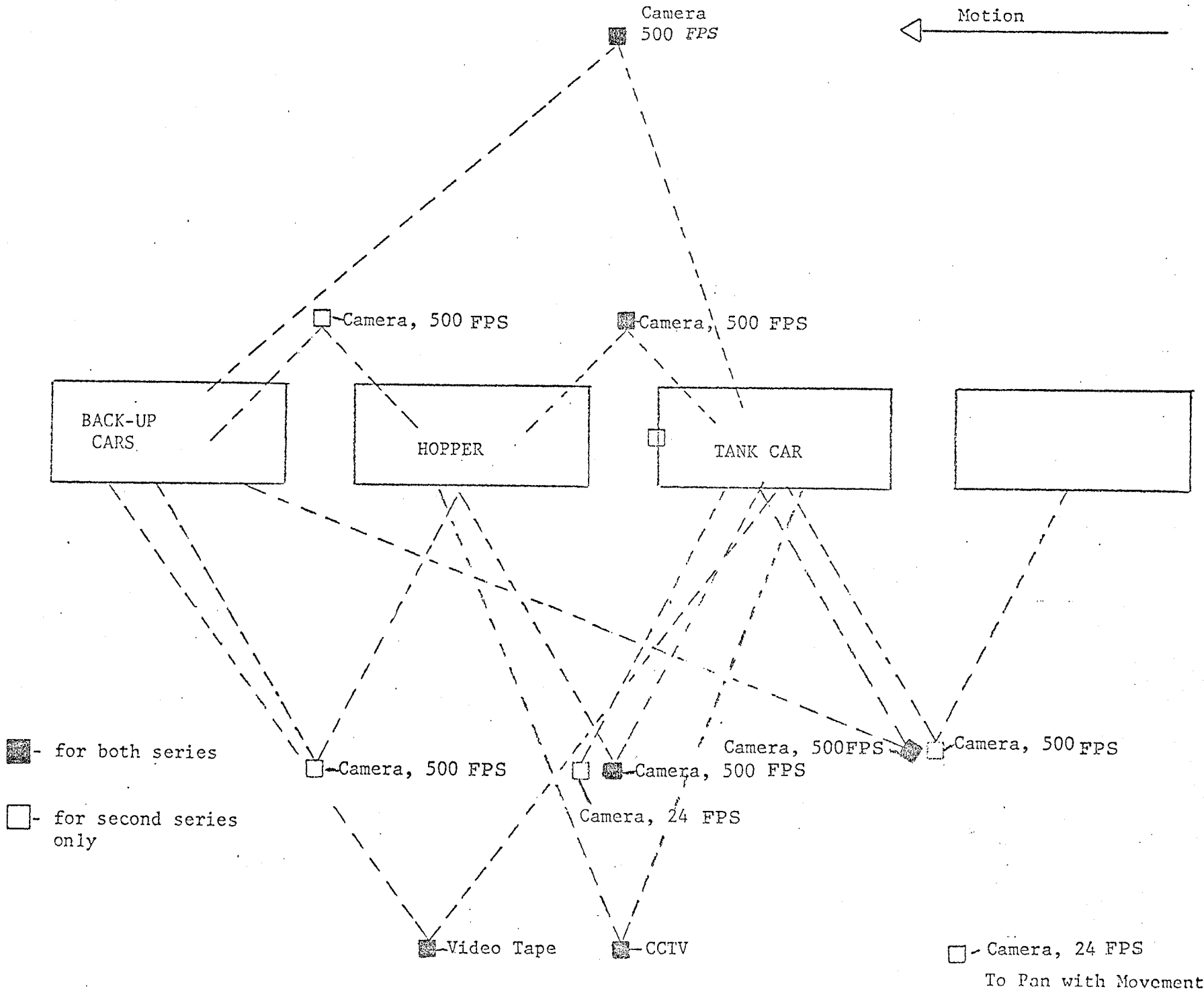


Figure C-1

#### 4.0 INSTRUMENTATION REQUIREMENTS

#### 4.0 INSTRUMENTATION REQUIREMENTS

- 4.1 Impact end of hopper car to have dynamometer coupler for preliminary tests and a strain gauged coupler for the main series of tests. Coupler strain gauges to be recessed to prevent destruction. Coupler travel will be adjusted to normal condition to ensure that draft gear bottoming occurs before the horn hits the striker plate.
- 4.2 Hopper car center sill to be strain gauged at impact end. Strain gauges must be located behind draft lugs but in front of truck bolster pin. Six gauges are required, two to measure strain on upper surface of sill, two to measure strain on lower flanges, and two to measure strain on neutral axis.
- 4.3 One accelerometer to be mounted on impact end of hopper center sill and near strain gauge locations to determine the initial shock spectrum of impacts.
- 4.4 A string pot will be used to measure longitudinal displacement of hopper car coupler at impact end.
- 4.5 String pot type displacement gauges will be used to measure vertical and pitching motions of the hopper car with respect to the side frames.
- 4.6 Two strain gauges to measure truck bolster bending on impact end of hopper car.
- 4.7 Dial gauges and calibrated load cells to be used for pre-test deflection measurements.

- 4.8 Impact velocity will be accurately controlled and velocities of cars before and after impact will be measured by speed gates.
- 4.9 A list of instrumentation types, locations, and channels are given in Appendix A.



5.0 PRE-TEST MEASUREMENT REQUIREMENTS

5.1 FORCE CALIBRATION

5.2 PRELIMINARY TEST/EFFECT OF SLOSHING

5.3 INSPECTION REQUIREMENT FOR ALL RPI/AAR  
FURNISHED HOPPOR CARS

## 5.0 PRE-TEST MEASUREMENT REQUIREMENTS

- a. Total weight (all cars).
- b. Truck weight and body weight (tank and hopper cars).
- c. Lading weight (tank cars).
- d. Length between coupler faces (all cars).
- e. Length between truck centers (all cars).
- f. Maximum possible travel of truck center plate and pins to release (one hopper car).
- g. Vertical play of coupler at end sill and at coupler knuckle (all cars) with all coupler and draft gear slack removed in buff.
- h. Coupler heights above rails (all cars) - coupler heights must be within AAR limits. For all impact testing between empty car and loaded car vertical coupler offsets must be identical  $\pm 1/2$ ".
- i. Maximum possible travel of truck bolsters down to spring bottom and up to hitting side frame (one hopper and one tank car).
- j. Experimentally locate center of gravity by three point suspension (one hopper car).
- k. Determine moment of inertia about center of gravity by swinging car in pendulum fashion and measuring frequency (one hopper car).
- l. Items j. and k. to be calculated for loaded tank car.

## 5.1 FORCE CALIBRATION

5.1.1 Measure force deflection plot of one truck on one hopper car and one tank car during and after bottoming of truck springs, as outlined in Appendix B. Truck strain gauges on hopper car to be calibrated at this time.

5.1.2 Measure vertical spring rates and deflection curves for one hopper car and one loaded tank car by lifting on coupler as outlined in Appendix C. Hopper car strain gauges in coupler shank and sill to be calibrated for bending at this time. (Distance to clear hopper car center pin may also be determined.)

5.1.3 Impact two identical tank cars and also two identical hopper cars as outlined in Appendix D. These tests will be used to calibrate longitudinal sill strain gauges using dynamometer couplers. The tests will also provide longitudinal spring rates.

5.1.4 Calibrate longitudinal force coupler shank strain gauges by appropriate squeeze test of coupler shank.

## 5.2 PRELIMINARY TEST/EFFECT OF SLOSHING

In order to determine the effect of sloshing in the impact tests, a tank car will be impacted into the hopper car under the conditions of:

- a. Tank car 62.5% full of water.
- b. Tank car 75% full of water.
- c. Tank car 94.6% full of water.

The impacts will be at 4, 6, and 8 mph and speed gate and low speed movie coverage used. The films and force data will be used to determine the effect of sloshing. Cut levers will be tied up to prevent coupling and full hopper car instrumentation will be used.

### 5.3 INSPECTION REQUIREMENT FOR ALL RPI/AAR FURNISHED HOPPER CARS

Inspect for compliance with the following:

#### I. Couplers

- a. The operating mechanism used with the Articulated Rotary Coupler is generally of the one-piece standard design as shown in Figure 5-1.

The alternate standard rod is similar to the standard in design except that it is provided with a turned-in hand grip at the extreme end of the handle.

It is important to have at least 1/4 inch and preferably not more than 1/2 inch clearance between the operating rod eye and the locklift lever (Dimension A) when the coupler is centered in the carrier and the coupler fully locked.

The portion of the rod next to the handle, as viewed from the front (Dimension C), must be parallel to the end sill to insure contact of the handle with the bracket stop surface when the coupler moves laterally toward the bracket.

The clearance B between the bracket and rod handle must be not less than 3-3/4 inches nor more than 4-1/4 inches, and the straight portion of the rod must extend at least 4-1/4 inches beyond the bracket eye.

- b. The coupler operating mechanism should open the knuckle when the handle is raised to the top position.
- c. The lock must drop freely to the locked position when the knuckle is closed slowly. The lock is in the locked position when it rests on the shelf of the knuckle tail.
- d. Determine the effectiveness of the anti-creep protection. Insert a bar between the lock and knuckle tail shelf and pry the lock upward and at the same time force the lock leg rearward by inserting a screwdriver between the lock leg and the front of the lock hole as shown in Figure 5-2.

If the lock can be raised by this method enough to permit opening of the knuckle, the coupler has insufficient anti-creep protection. Correction of insufficient anti-creep protection should be made by replacing (1) the locklift assembly, (2) the lock, or (3) the knuckle. Usually replacement of the locklift assembly is sufficient but in some cases further benefit is obtained by renewal of the lock and/or knuckle.

- e. If the distance between point of knuckle and guard arm exceed  $5\text{-}5/16$  inches as measured by the gage shown in Figure 5-3, the defective part or parts must be renewed to bring the coupler within required gage of  $5\text{-}1/8$  inches as measured by the gage shown in Figure 5-4.

- f. Type "E" knuckles must be renewed when Gage No. 44057 can be passed vertically over the knuckle nose as shown in Figure 5-5.
- g. Wear plate must not be worn more than 1/8" deep. If the coupler is not equipped with a wear plate, the shank must not be worn more than 1/4" deep.
- h. When coupler is removed from car for any reason, inspect coupler shank length and rear of keyslot to shank butt length. Coupler must meet the following requirements:

Minimum shank length as shown in Figure 5-6 per dimension A is 21".

Minimum length for average dimension per dimensions B and C shown in Figure 5-6 is 3-3/4".

- i. The maximum permissible free slack in the draft attachment is one inch. The amount of free slack can be determined by first sledging the coupler back solid and then measuring the clearance between the coupler horn and the striker face. Next, by inserting a long bar between the horn and striker face, pry the coupler out as far as possible and again measure the space between the horn and striker. The difference between these two measurements is the amount of free slack present.
- Excessive free slack (normally more than 1") indicates a part may be missing, broken or excessively worn and requires a closer inspection and/or disassembly.

## II. Yokes

Yoke must not be missing, bent, broken, cracked, etc., except for cracks through web portion from rear of key slot, one or both sides. See Figure 5-7.

## III. Draft Gears

a. Draft gears must not be missing or defective.

Draft gears will be considered defective when any part of same, except external retaining bolt or rod only, is defective. When draft gear is removed in conjunction with other work, defective retaining bolts or rods should be renewed.

b. Follower plate must not be missing or broken.

c. Support plate and fasteners must not be defective.

## IV. Car Body

Coupler carriers, center plates, center sills, center pins and rear draft lugs must not be defective.

## V. Truck Spring Assemblies

Spring Assemblies (including friction snubbers) must not be missing or defective. (Note: Cars are to be resprung prior to shipment to the Transportation Test Center).

Deviations from the above requirements are to be expected and must be handled on an individual car basis. Please note any deviations and contact the RPI-AAR representative for disposition.

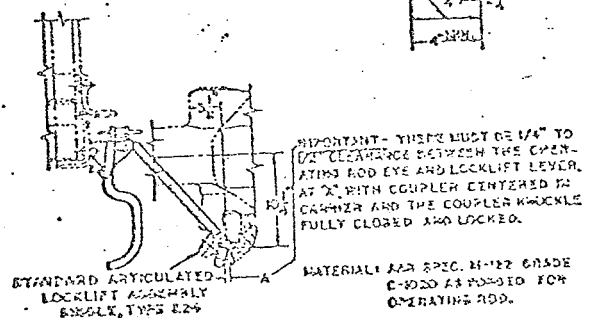
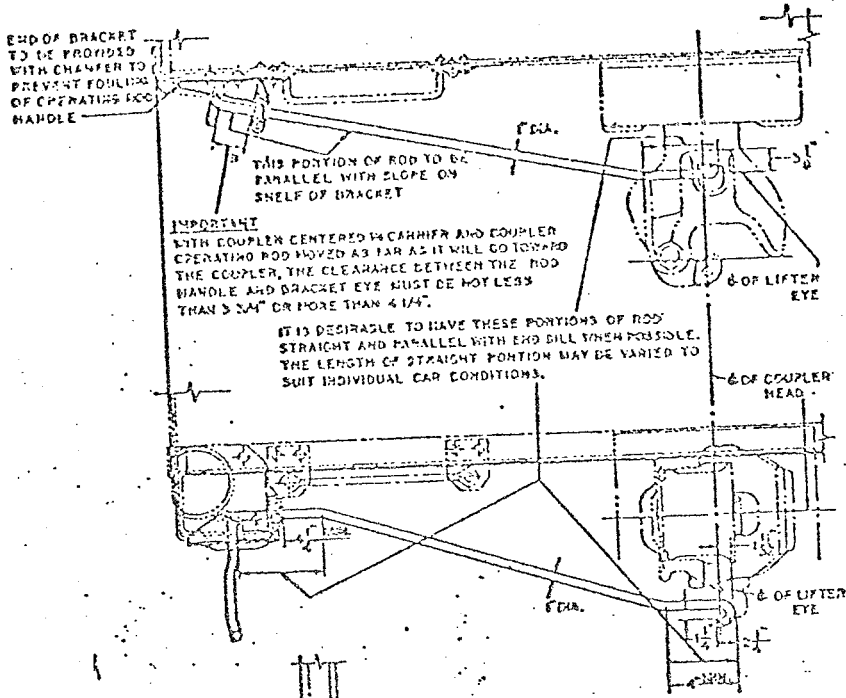


FIGURE 5-1

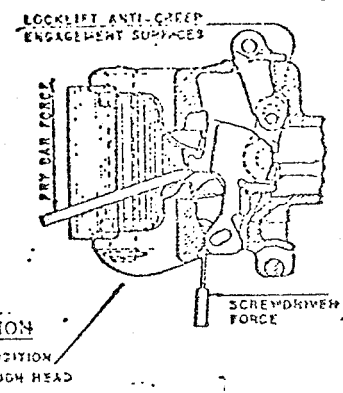


FIGURE 5-2

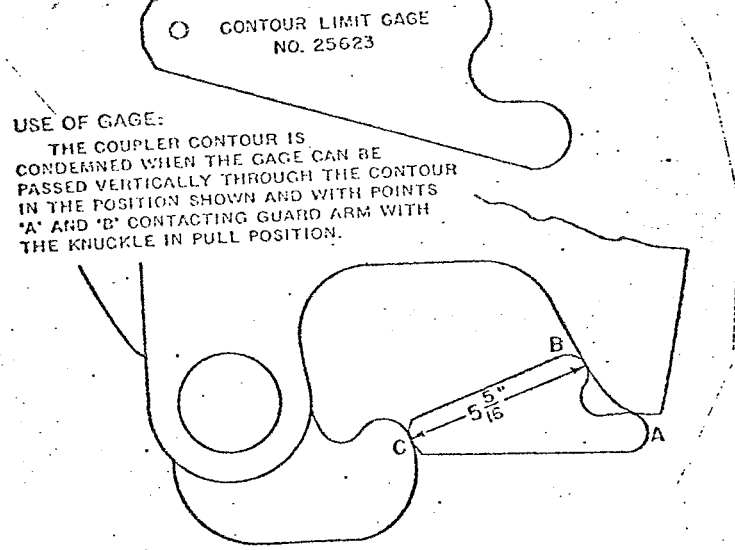


FIGURE 5-3

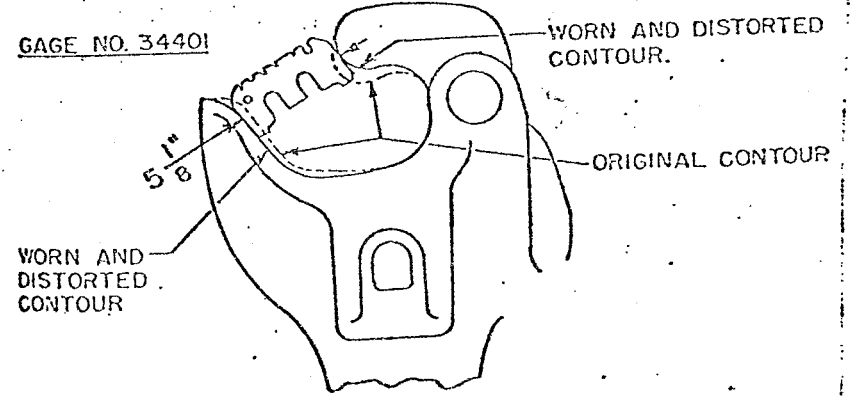


FIGURE 5-4



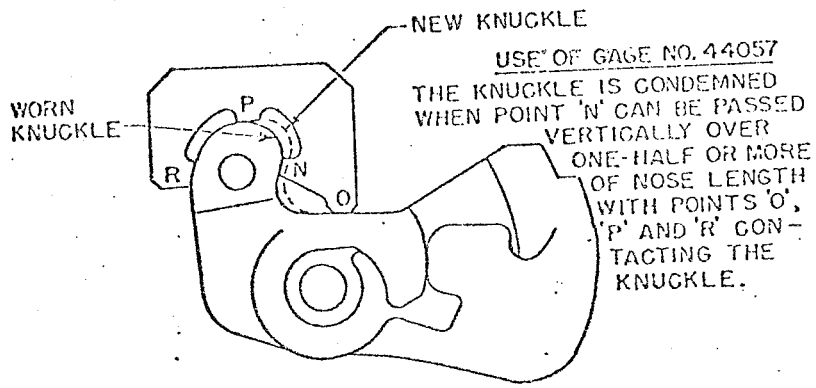
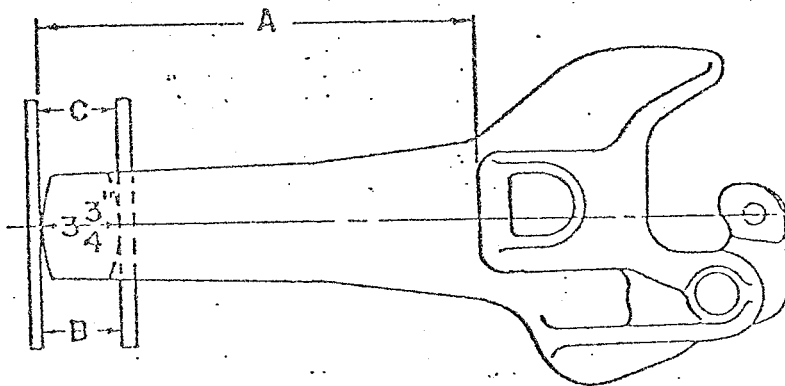


FIGURE 5-5



TO DETERMINE DISTANCE FROM KEY SLOT TO BUTT, ADD DIMENSIONS "C" AND "B" THEN DIVIDE BY TWO (2).

FIGURE 5-6

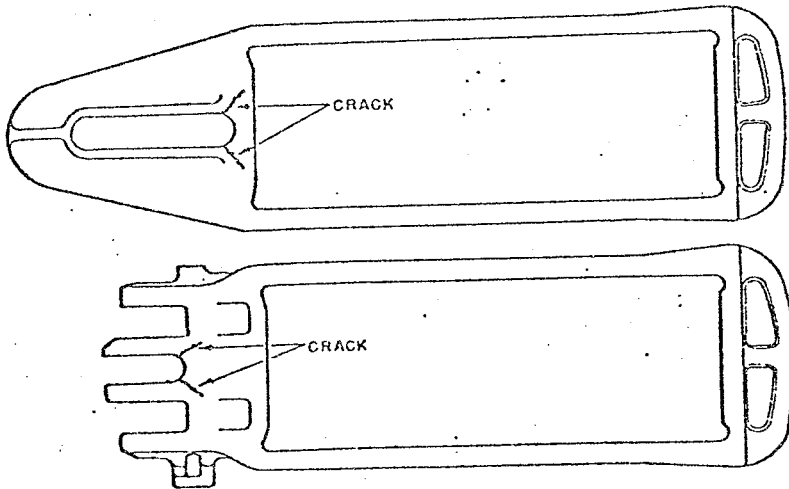


FIGURE 5-7

6.0 DATA RECORDING / REDUCTION REQUIREMENTS

6.1 DATA RECORDING / REDUCTION TECHNIQUES

6.2 HARDWARE CONFIGURATION

6.3 SOFTWARE CONFIGURATION

6.4 DESCRIPTOR MODULE

6.5 DATA ACQUISITION AND RECORDING MODULE

6.6 ENGINEERING UNIT CONVERSION MODULE

6.7 CALCULATION MODULE

6.8 SOFTWARE DOCUMENTATION

## 6.0 DATA RECORDING/REDUCTION REQUIREMENTS

- a. All measured data channels will be stored on analog tape with strip chart back-up.
- b. Data will be analyzed as outlined in Appendix E and provided in digital and graphical form.
- c. Graphs will be plotted individually and scaled according to Washington University Specifications.

### 6.1 DATA RECORDING/REDUCTION TECHNIQUES

- a. Twenty channels of data and time will be recorded.
- b. All data will be filtered to remove frequencies above 100 Hz.
- c. All data will be sampled at 500 samples/second.
- d. Approximately .8 seconds of data following impact is required. (Subsequent tests may have as many as three [3] impacts, .8 seconds of data after each is required.)
- e. The data will be recorded in real-time by hard copy on O-graph.
- f. Displays will be in the form of graphs plotted at .1 sec/in. on the X-axis and appropriate scaling on the Y-axis.

### 6.2 HARDWARE CONFIGURATION

The hardware which will be used to satisfy the requirements is detailed in the following list.

- a. Varian 620/f minicomputer and associated peripherals.
- b. Datawest Analog to Digital (A/D) hybrid system.

- c. 100 Hz 6 Pole Butterworth Filters (analog).
- d. Metraplex 120 FM demodulators.
- e. Bell and Howell CPR4010 portable record/playback unit.
- f. DATUM Model 9200 Time Code Reader.
- g. DATUM Model 9100 Time Code Generator.

Figure D-1 shows a block diagram for configuration of the above mentioned hardware.

### 6.3 SOFTWARE CONFIGURATION

A set of computer programs have been designed to control the acquisition and recording of data, and compute with required data, output values for printing and plotting. All modules are written in Varian FORTRAN IV with the exception of those routines necessary to interface with the hybrid equipment. The MOS operating system will be used to control the loading of program modules. The following four (4) paragraphs delineate the functional characteristics of the software modules necessary for data reduction. Figures D-2 and D-3 show graphically the module interdependence, input and output.

### 6.4 DESCRIPTOR MODULE

The function of the Descriptor Module is that of correlating inputs related to the data path of a measurement in such a way that validation of the data path may be done and that conversion to engineering units may be accomplished. Typical inputs will include:

- a. VCO channel number
- b. Filter number
- c. Discriminator channel number

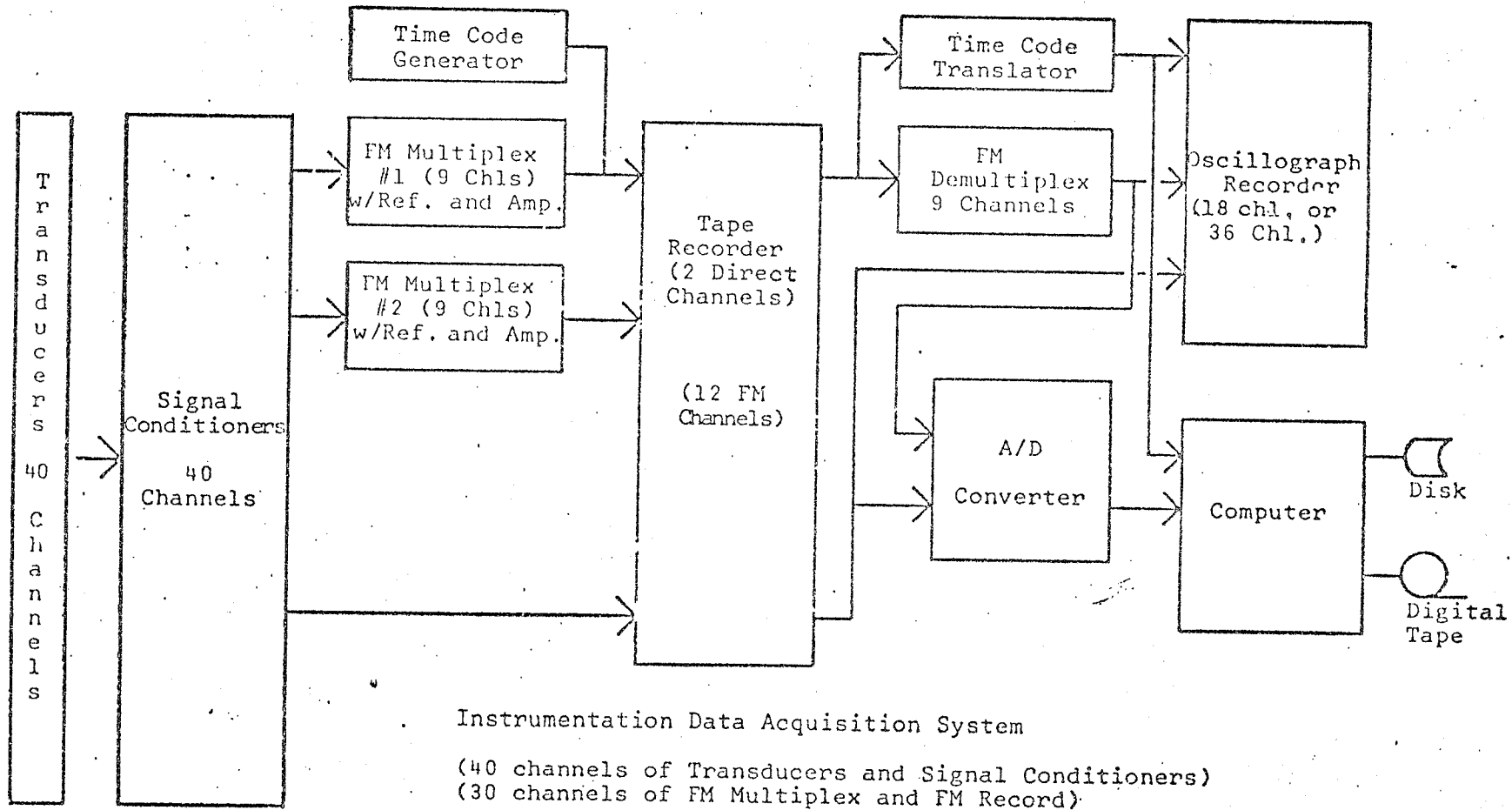


Figure D-1

Programmer: \_\_\_\_\_ Program No.: \_\_\_\_\_ Date: \_\_\_\_\_ Page: \_\_\_\_\_  
Chart ID: \_\_\_\_\_ Chart Name: \_\_\_\_\_ Program Name: \_\_\_\_\_

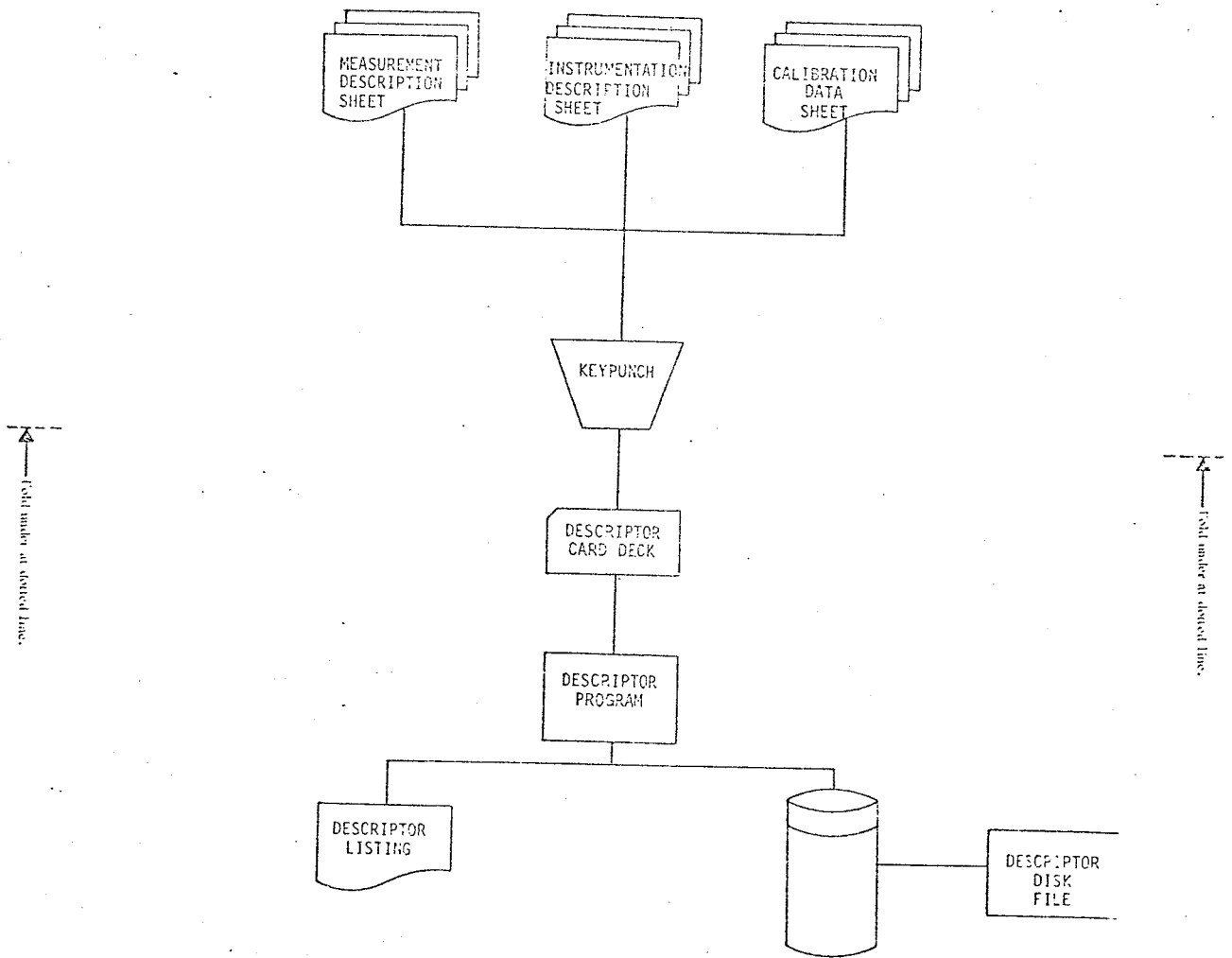


Figure D-2

Programmer: \_\_\_\_\_ Program No.: \_\_\_\_\_ Date: \_\_\_\_\_ Page: \_\_\_\_\_  
 Chart ID: \_\_\_\_\_ Chart Name: \_\_\_\_\_ Program Name: \_\_\_\_\_

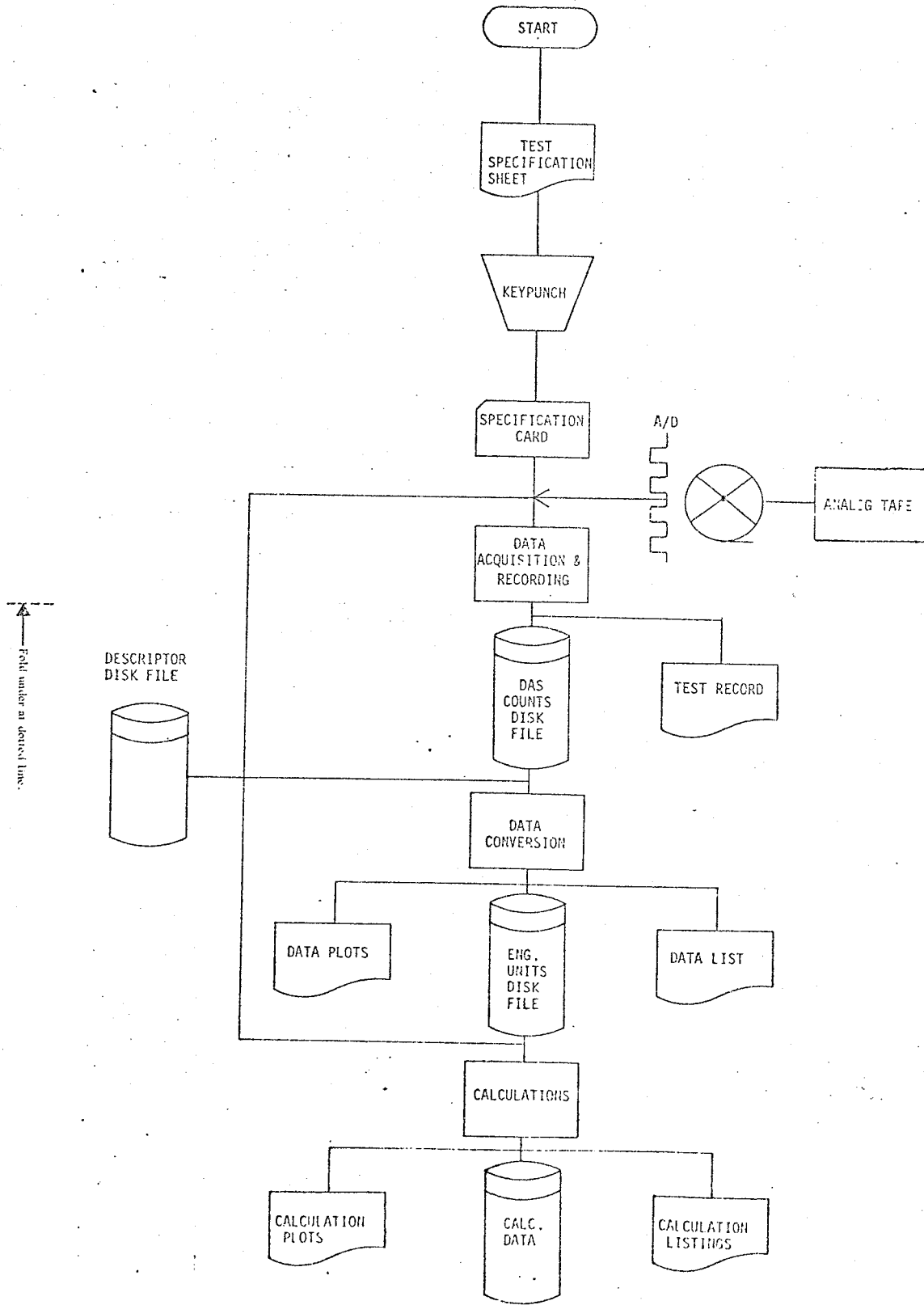


Figure D-3

- d. A/D channel number
- e. Transducer identification
- f. Transducer calibration values
- g. Calibration values for a, b, c, and d above, if appropriate.
- h. Patching information
- i. Measurement number
- j. Measurement geometrical position

The correlated data will be displayed on a computer listed by the Status-21 printer/plotter. (See attached examples in Appendix F).

#### 6.5 DATA ACQUISITION AND RECORDING MODULE

The function of the Data Acquisition and Recording Module (DARM) is that of utilizing the hybrid hardware to monitor and digitize outputs from the analog system, and to record the data on disk for subsequent processing.

The main program will be written in FORTRAN IV. The program will call an assembly language program that will access and record the data on disk. The amount of data to be recorded in any one pass of the analog tape will depend upon the sample rate desired, the number of channels of interest, and the amount of elapsed time for which data is desired.

#### 6.6 ENGINEERING UNIT CONVERSION MODULE

The function of Engineering Unit Conversion Module (EUCM) is that of converting raw data in integer Data Acquisition System (DAS) counts to computer oriented floating point numbers in engineering units for subsequent processing. A



secondary function of the module will be to provide print and plot capability for the engineering unit data. The plots will provide the scaling capability to answer requirements 6.1 f.

#### 6.7 CALCULATION MODULE

The function of the Calculation Module (CM) is that of providing simple, calculated results for printing and plotting. The structure of the module will be so optimized that response to user special calculation requirements will be based on minimum time and effort.

#### 6.8 SOFTWARE DOCUMENTATION

6.8.1 Software documentation shall consist of program module level documentation as shown below:

- a. Functional Description and Specification
- b. Maintenance Manual
- c. Demonstration test results

6.8.2 System documentation will include:

- a. User Manual
- b. Computer operations instructions

7.0 PHYSICAL PRE-TEST MEASUREMENT TECHNIQUES

- 7.1 LENGTH BETWEEN COUPLER FACES
- 7.2 LENGTH BETWEEN TRUCK CENTERS
- 7.3 VERTICAL PLAY OF COUPLER SHANK AT SILL AND KNUCKLE
- 7.4 COUPLER HEIGHT ABOVE RAIL
- 7.5 DETERMINATION OF HOPPER CAR CENTER OF GRAVITY AND PITCH MOMENT OF INERTIA
- 7.6 TRUCK STIFFNESS AND BOLSTER TRAVEL
- 7.7 VERTICAL SPRING RATE AND DEFLECTION CURVE
- 7.8 CAR TO CAR IMPACT/CALIBRATION TEST

## 7.0 PHYSICAL PRE-TEST MEASUREMENT TECHNIQUES

The Pre-Test Measurements defined are to be performed on selected tank and hopper cars associated with the Switchyard Impact Test Program. The data taken as a result of the measurements are to be recorded on Data Recording Sheets, Figure G-1. Prior to pre-test measurements RPI/AAR furnished hopper cars will be inspected jointly with the Missouri Pacific Railroad representative and Transportation Test Center in accordance with Section 5.3 of this Test Specification.

### 7.1 LENGTH BETWEEN COUPLER FACES

- a. Assure coupler knuckle is in closed position with coupler and draft gear slack removed in buff. (Compression)
- b. Measure length between the outside coupler faces (not pulling face) using plumb bobs suspended from center of coupler faces over a 100 foot steel tape measure drawn taut on the floor beneath the car.
- c. Record measurement.

### 7.2 LENGTH BETWEEN TRUCK CENTERS

- a. Measure length between leading edge of A-End (leading end) bolster and B-End bolster outside side frame, using a 100 foot steel tape measure drawn taut. Take this measurement on each side of the car. NOTE: If leading edge of bolster is deformed or otherwise unsatisfactory for using as a reference, select another reference point which can be identified on both bolsters to make measurements between.
- b. Record measurements.

### 7.3 VERTICAL PLAY OF COUPLER SHANK AT SILL AND KNUCKLE

- a. Assure all coupler and draft gear slack is removed in buff at both ends of car.

DATA RECORDING SHEET

Test Program Title: \_\_\_\_\_

Pre-Test Measurement: \_\_\_\_\_

Test Measurement: \_\_\_\_\_

Post-Test Measurement: \_\_\_\_\_

Car Number: \_\_\_\_\_

ITEM	DATA DESCRIPTION	UNITS	VALUE	WORKED	VALIDATED

- b. Scribe a reference mark on face of striker plate centered over coupler shank and on vertical center of coupler face on A-End of car.
- c. Place a reference bar across rails directly below coupler face.
- d. Measure vertical distance between reference mark on striker plate and coupler shank with steel rule.
- e. Record measurement.
- f. Using a jack under the coupler, raise the coupler shank until it hits the striker plate.
- g. Measure distance between reference mark on striker plate and coupler shank with steel rule.
- h. Record measurement.
- i. Measure distance between reference mark on coupler face and bottom of reference bar with steel rule.
- j. Record measurement.

#### 7.4 COUPLER HEIGHT ABOVE RAIL

- a. Measure distance between reference mark on coupler face and bottom of reference bar, with steel rule. (Measurements must be within AAR Specification [32 1/2" - 35 1/2" empty, and 31 1/2" - 33 1/2" loaded]. If measurements are not within tolerance the coupler must be shimmed.)
- b. Record measurements.
- c. Repeat 7.3 a. through j. on B-End of car.

#### 7.5 DETERMINATION OF HOPPER CAR CENTER OF GRAVITY AND PITCH MOMENT OF INERTIA

- a. Attach plum bob and chalk line to top of pivot pin on A frame.

- b. Attach two 10' - 7" x 3/4" diameter cables and two 16' - 5" x 1" diameter cables to A Frame pivot pin, using three washers per pin.
- c. Move hopper car in place, install tie bar and two stringers. Lift hopper car free of trucks with two - 30 ton cranes attached to car lifting points. Attach four cables to cable pads on hopper car.
- d. Lower hopper car until cables, attached to A Frame, take up car weight.
- e. Remove crane cables from hopper car.
- f. Let car settle till no movement is perceived.
- g. Mark line of plumb bob on side of car. (Verify cables do not run on side of hopper car.)
- h. Lift hopper car with two - 30 ton cranes attached to car lifting points until A Frame cables are slack.
- i. Detach A Frame cables and lower car onto trucks.
- j. Repeat 7.5 c. through i. with A Frame cables reversed.
- k. Attach four 19' - 7" x 3/4" diameter cables to A Frame pivot pins using three washers per pin.
- l. Lift hopper car with two - 30 ton cranes attached to car lifting points. Attach four cables to cable pads on hopper car.
- m. Lower hopper car until cables attached to A Frame take up car weight.
- n. Remove cable cranes from hopper car.
- o. Verify cables do not rub on sides of hopper car.

- p. Measure distance from top of A Frame pivot pin to hopper car center of gravity with steel tape as accurately as possible. Record distance.
- q. Manually swing hopper car with tie ropes until the  $\pm 5^\circ$  amplitude is achieved. Release car and let swing free.
- r. Record time for 5 cycles, 10 cycles, 15 cycles and 20 cycles, if possible. Record number of cycles to half amplitude and number of cycles to imperceptible motion.
- s. Repeat steps q. through r. two times.
- t. Lift hopper car with two - 30 ton cranes attached to car lifting points until A Frame cables are slack.
- u. Detach A Frame cables and lower car onto trucks.
- v. Record the following items on Data Recording Sheet:

(Figure G-1)

<u>ITEM</u>	<u>MEASUREMENT</u>	<u>UNIT OF MEASURE</u>
j.	Coordinate of Hopper Car Center of Gravity:	
	Inches from center of car	Inches
	Inches above railhead	Inches
p.	Distance from top of A Frame pivot point to hopper car center of gravity	Inches
r.	Time for 5 cycles	Min/sec
	Time for 10 cycles	Min/sec
	Time for 15 cycles	Min/sec
	Time for 20 cycles	Min/sec
	Number of cycles to $\pm 2\ 1/2^\circ$ amplitude	Cycles
	Number of cycles to imperceptible motion	Cycles
s.	Time for 5 cycles	Min/sec
	Time for 10 cycles	Min/sec
	Time for 15 cycles	Min/sec
	Time for 20 cycles	Min/sec
	Number of cycles to $\pm 2\ 1/2^\circ$ amplitude	Cycles
	Number of cycles to imperceptible motion	Cycles
	Time for 5 cycles	Min/sec
	Time for 10 cycles	Min/sec
	Time for 15 cycles	Min/sec
	Time for 20 cycles	Min/sec
	Number of cycles to $\pm 2\ 1/2^\circ$ amplitude	Cycles
	Number of cycles to imperceptible motion	Cycles

## 7.6 TRUCK STIFFNESS AND BOLSTER TRAVEL

- a. Defined are the pre-test measurements to be performed on one tank car truck and one hopper car truck. The strain gauge channels of the hopper car truck are calibrated during the hopper car truck pre-test measurements. Data will be recorded on Data Recording Sheet (Figure G-1).
- b. Assemble truck loading fixture near west end of bridge structure in Test Pit #2 (RDL).
- c. Place truck to be tested on bridge structure and roll under loading fixture so the center plate is centered under the load pad of the loading fixture.
- d. Place chocks fore and aft of truck wheel to prevent truck from moving along track.
- e. Attach position transducer assembly to rail head and truck bolster.
- f. Apply load to truck until springs are completely compressed, recording deflection of bolster and side frame at 10,000 pound increments starting at 0 pounds as indicated from load cell instrumentation. Spring group compression is detected by position transducers on each side of truck and side frame deflection is detected by dial indicating gauges on each side frame.
- g. Record deflection of side frame and spring group when springs are completely compressed.
- h. Unload truck until spring load is completely removed recording deflection of spring group and side frame at 10,000 pound increments as indicated from load cell instrumentation.



- i. Using 20 ton overhead hoist and sling, lift bolster until contact is made with both side frames.
- j. Record position transducer readings.
- k. Remove springs from spring nest. Tag springs by location for reinstallation into same location at later time.
- l. Install steel blocks.
- m. Lower truck bolster onto steel block and remove sling.
- n. Apply load to truck at 10,000 pound increments starting at maximum load applied during Spring Group Stiffness Test, and increase to 100,000 pounds beyond starting load, recording load increase to 100,000 pounds beyond starting load, recording load from load cell instrumentation and deflection of bolster and side frames from dial indicating gauges. Plot load vs. side frame deflection during loading of truck to determine maximum load without yield of the truck side frame.
- o. Unload truck until load is completely removed recording deflection of bolster and side frame at 10,000 pound increments down to starting load as indicated from load cell instrumentation.
- p. Repeat steps f. through o. for hopper car truck, recording strain gauge readings as well as load cell, position transducer, and dial indicating gauge values.

#### 7.7 VERTICAL SPRING RATE AND DEFLECTION CURVE

- a. Position dial indicator gauges to measure movement of car body at six points (Appendix C)

- b. Position jack under coupler.
- c. Chock truck at non-lifted end of car.
- d. Block springs to reduce car movement on springs.
- e. Attach strain gauge instrumentation to hopper car strain gauges.
- f. Calibrate strain gauge instrumentation (hopper car test only).
- g. Apply upward force on car coupler in 5,000 pound increments until no load is applied to nearest center plate. Vertical upward force in all tank cars shall not exceed 50,000#.
- h. Record movement of car body from dial indicators and strain of sill and shank strain gauges.
- i. Record height of body bolster center plate when car center plate clears truck center plate.
- j. Continue lifting coupler until center pin clears center plate and record height.
- k. Plot deflection curve of hopper car and full tank car.

#### 7.8 CAR TO CAR IMPACT/CALIBRATION TEST

- a. Prepare two hopper cars. One with strain gauges on coupler shank and sill and the other to have a dynamometer coupler.
- b. Two fully loaded tank cars. One with a dynamometer coupler.
- c. Connect car-borne sensors to wayside recording instrumentation.
- d. Connect speed traps to wayside recording instrumentation.
- e. Calibrate car-borne sensors.

- f. Calibrate wayside instrumentation.
- g. Using locomotive or pusher, impact one hopper car at 4 and 6 mph into a standing identical hopper car with no brakes applied.
- h. Record all standard hopper car instrumentation and dynamometer signals.
- i. After cars have separated (both couplers are open), wayside brake trips will be used to stop the cars.
- j. Impact one fully loaded tank car at 2 and 4 mph into a standing identical fully loaded tank car with no brakes applied.
- k. Record dynamometer signal.
- l. After cars have separated, wayside brake trips will be used to stop the cars.

8.0 INSTRUMENTATION TECHNIQUES

8.1 STRAIN GAUGES

8.2 DISPLACEMENT TRANSDUCERS

8.3 ACCELEROMETERS

8.4 LOAD CELLS

8.5 IMPACT SWITCH

8.6 INTERFACE CABLING - CONNECTION

8.7 SPECIAL INSTRUMENTATION

8.7.1 Electronic Speed Gates

8.7.2 Dynamometer Coupler

8.8 PHOTO INSTRUMENTATION

8.9 DATA ACQUISITION SYSTEM

8.9.1 Signal Conditioning Equipment

8.9.2 Multiplexing Equipment

8.9.3 Magnetic Tape Recorders

8.9.4 Strip Chart Recorders

8.9.5 Time Code Generation

## 8.0 INSTRUMENTATION TECHNIQUES

### 8.1 STRAIN GAUGES

- a. Two hopper cars will be instrumented with twelve strain gauges each at the impact end only. One hopper car will act as a back-up or stand-by unit to be used in the event of failure or damage to the primary car. All strain gauges are of the weldable type consisting of a precision foil sensor bonded to a 300 series stainless steel carrier. These are extremely rugged type sensors designed especially for field test environments on massive steel structures. They are easily installed, with minimal surface preparation, by means of a miniature, portable spot welder. Suitable physical/environmental protection will be provided for each strain gauge.
- b. The twelve strain gauges on each car will be mounted and connected as pairs, in a two-active arm bridge configuration. One pair will be mounted on the upper surface of the truck bolster to monitor vertical bending forces. (See Figure E-2) Three pairs will be mounted on the sill to measure impact bending forces. Two pairs will be mounted on the coupler shank just behind the coupler to measure longitudinal and bending forces applied to the coupler. All strain gauges will be statically calibrated during pre-test measurements.

### 8.2 DISPLACEMENT TRANSDUCERS

Nine position-displacement transducers (string pots) will be installed on the hopper car to monitor linear displacements

(See Figure E-4). Four pairs of the transducers will be mounted to measure body to side frame deflection at each corner of the hopper car. The remaining transducer will be mounted to measure the longitudinal displacement of the the impacted coupler relative to the hopper car body.

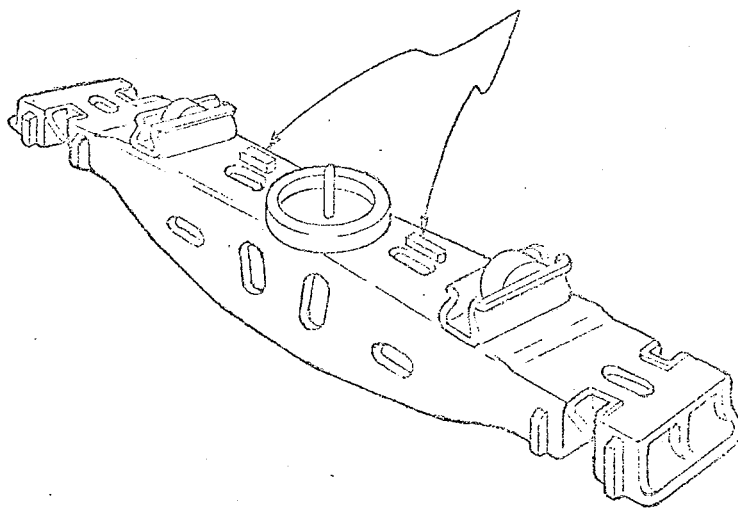
### 8.3 ACCELEROMETERS

A single piezoresistive accelerometer capable of measuring accelerations of  $\pm 50$  G will be mounted in a protective housing on the upper forward surface of the hopper car sill. It will be positioned precisely to monitor longitudinal impact accelerations. (See Figure E-4)

### 8.4 LOAD CELLS

Calibrated load cells will be used for pre-test measurements of truck spring and bolster stiffness. A single 200,000 pound load cell will be employed to measure the force applied to produce "bottoming-out" of the truck springs. Truck bolster strain gauge readings will be correlated with the load cell readings in step increments for calibration purposes. The load will then be removed and the spring groups replaced by structural blocks. A maximum force of 200 Kips will then be reapplied in incremental steps of 10,000 pounds to determine truck side frame and bolster spring rate beyond spring bottoming conditions. Again, truck bolster strain gauge readings will be taken and correlated with load cell force measurements for calibration of the truck bolster strain gauge system.

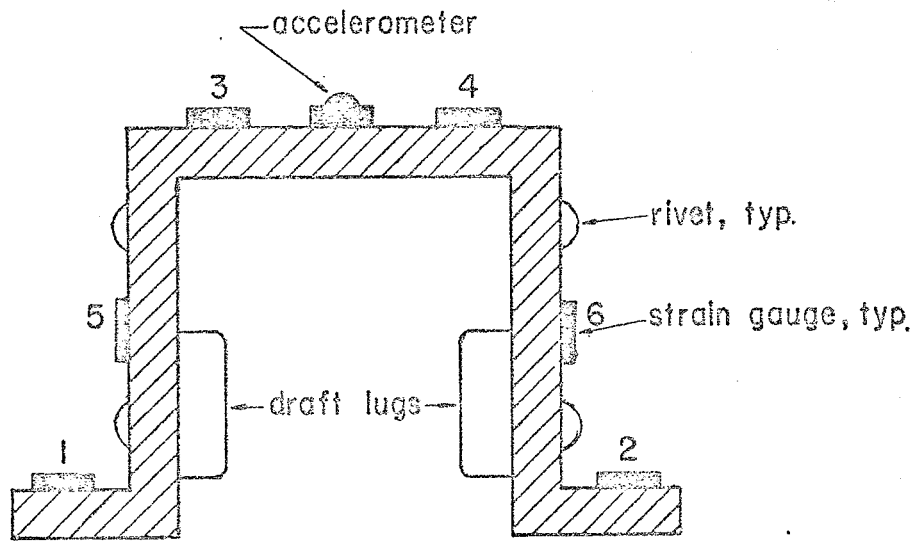
STRAIN GAUGES ADDED  
TO CREATE CHANNEL 1



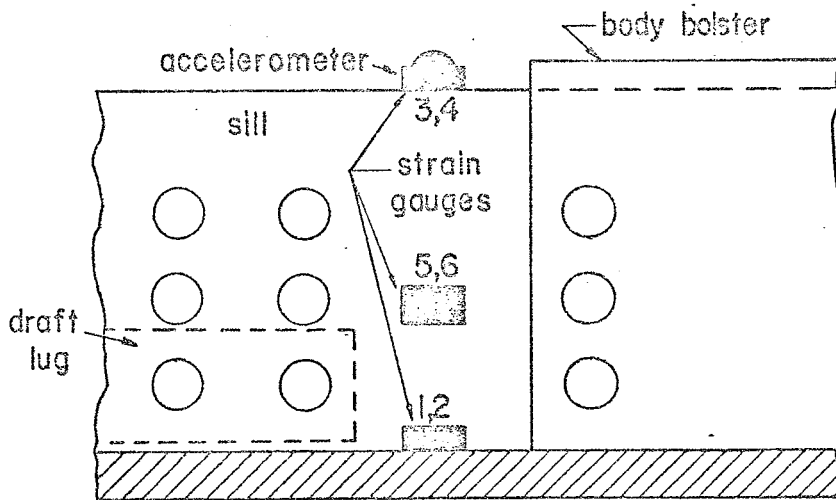
TRUCK BOLSTER

LOCATION OF STRAIN GAUGES  
ON HOPPER CAR TRUCK (IMPACT END)

Figure E-1



END VIEW



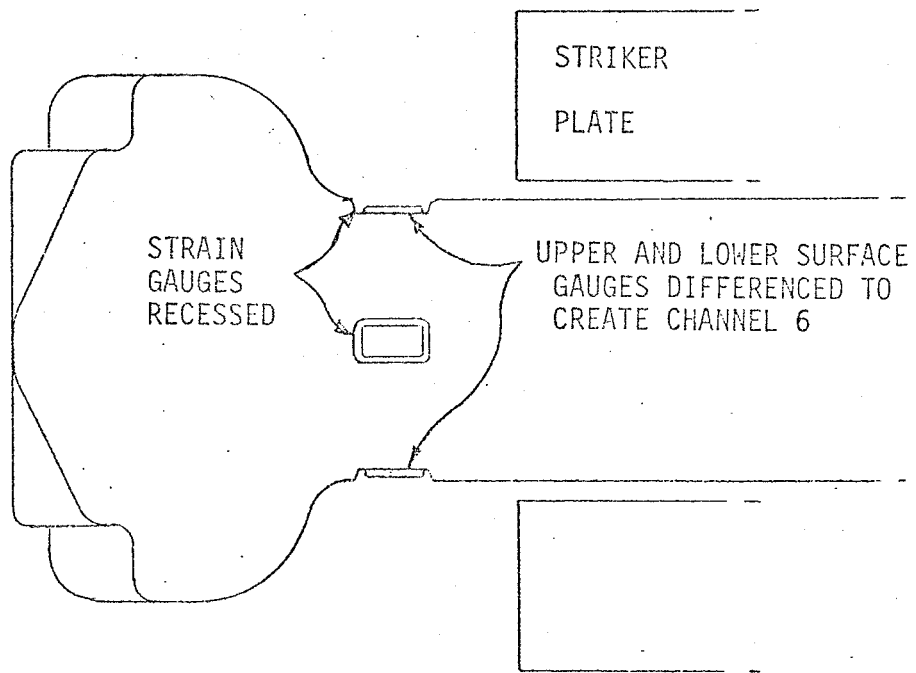
SIDE VIEW

gauges 1 through 6 added for channel ② (1+2+3+4+5+6)  
 gauges 1 through 4 subtracted for channel ③ (3+4-1-2)  
 accelerometer is channel ④

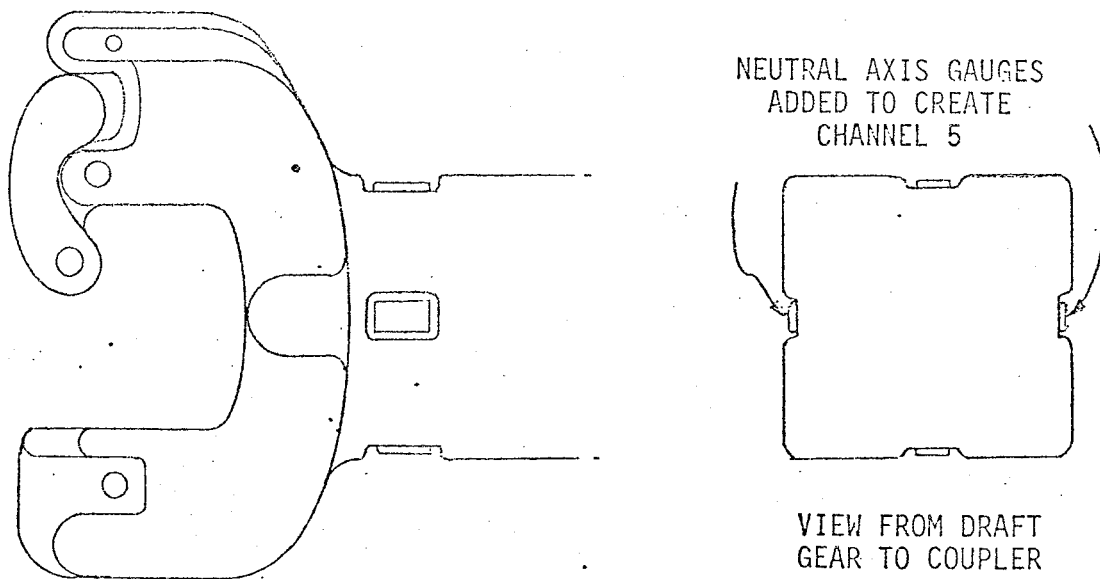
Fig. E-2 - Location of Strain Gauges and Accelerometer on Sill



LOCATION OF GAUGES ON COUPLER SHANK

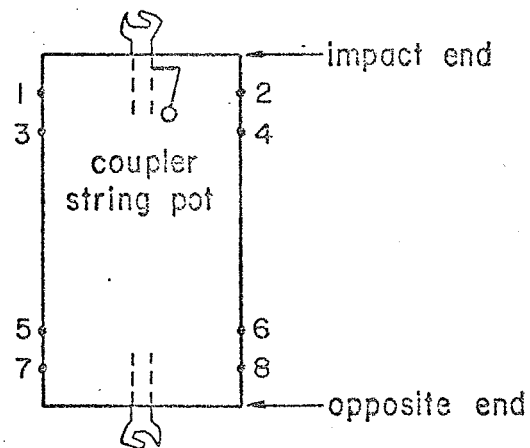
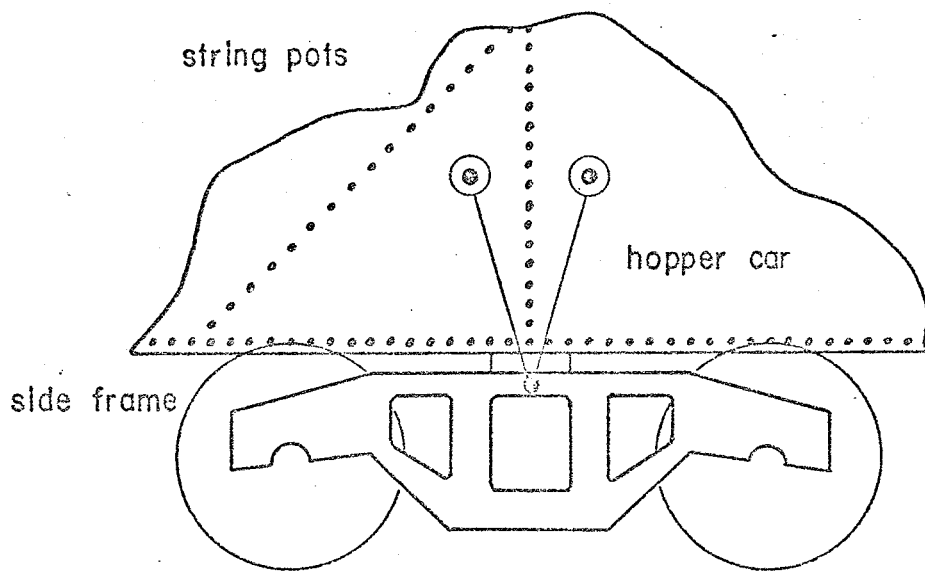


SIDE VIEW



TOP VIEW

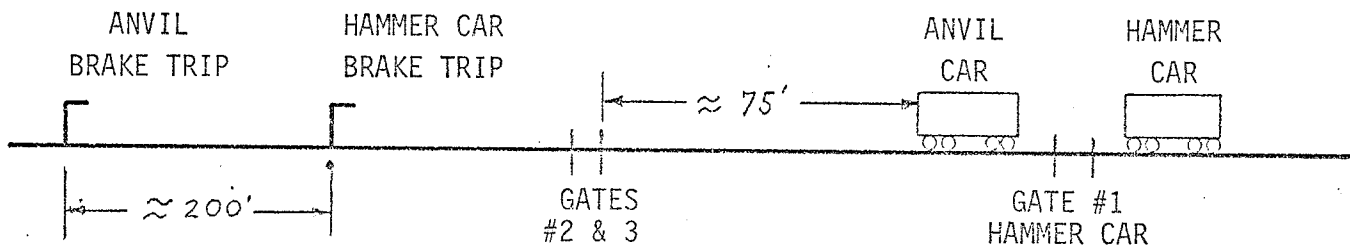
Figure E-3



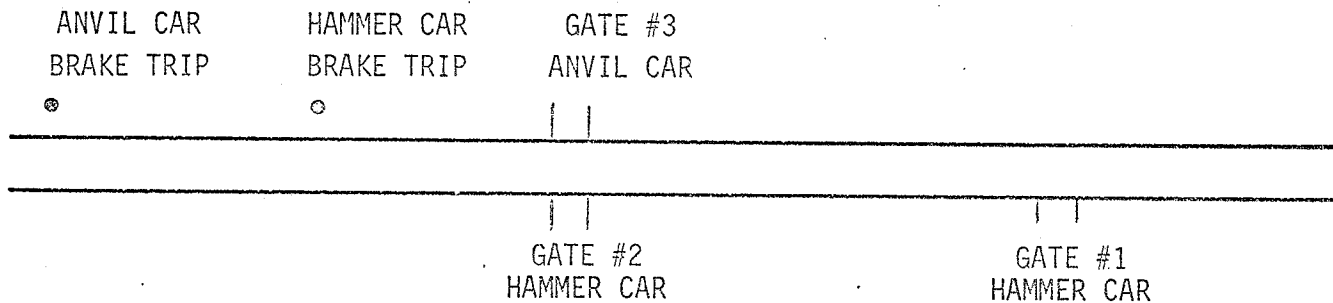
deflections	1 plus 2	form	channel	(7)
deflections	3 plus 4	form	channel	(8)
deflections	5 plus 6	form	channel	(9)
deflections	7 plus 8	form	channel	(10)
deflections	coupler	form	channel	(11)

Fig. E-4 Location of string pots

SPEED GATES AND BRAKE TRIPS



SIDE VIEW



TOP VIEW

Figure E-5

## 8.5 IMPACT SWITCH

A microswitch will be mounted in the vicinity of the coupler on the impact end of the hopper car. This switch will be positioned, with an expendable "cat Whisker" type operator, in such a manner that it will be operated at the instant of first contact between the couplers of the tank car and the hopper car. This operation will then produce a pulse type reference marker to be recorded on the magnetic tape and strip chart recorders.

## 8.6 INTERFACE CABLING - CONNECTION

- a. Three 20 pair, individually shielded pair instrumentation cables approximately 500 foot long will be laid between a wayside junction terminal box located beside the track in the impact zone and a similar junction terminal box inside the data trailer located about 500 feet back from the impact zone. This arrangement will then provide a total of 60 individually shielded pairs from trackside to the data trailer. The junction boxes will be of the weatherproof type with suitable connectors to adapt to either end of the 500 foot cables. Sufficient terminal strips will be mounted inside the junction boxes to facilitate any additional inter-face wiring and cabling required to complete connections to the transducers or the signal conditioner inputs.
- b. Individual shielded cables will be used to connect the signal conditioning equipment in the data trailer to the junction box cabling to the trackside junction box.

## 8.7 SPECIAL INSTRUMENTATION

### 8.7.1 Electronic Speed Gates

- a. An electronic speed gate has been developed and tested at the TTC especially for precision measurement of rail car velocities in impact test configurations. This speed gate consists primarily of an industrial type limit switch with a one-way, "cat whisker" type operator on an adjustable mounting bracket attached to a rail tie in such a position as to be triggered by the over hanging outside edge or a rail car wheel. A "one-shot" multivibrator and a flip-flop integrated circuit along with a voltage regulator complete the electronic package for each speed gate.
- b. The method used by this type speed gate to determine a rail car's velocity is to accurately detect a wheel passing the location of the limit switch. Thus, on the forward truck of a rail car, two wheel crossings would occur, and the exact distance of spacing between the two wheel is known. Therefore, if each wheel detection is recorded and presented simultaneously with an accurate timing signal such as IRIG-B time code, then the data reduction simply becomes  $V = \frac{dn}{dt}$  where velocity equals the distance (wheel spacing) divided by the time (in milliseconds) between the two wheel detection pulses.

c. Three such speed gates will be employed in the Impact Zone. They will be positioned in such a manner as to precisely determine (by time-data reduction) the exact speed of: (1) the tank car immediately prior to impact; (2) the tank car after impact (at some point to be determined); and (3) the hopper car after impact. Refer to Figure F-1 for Speed Calculations.

#### 8.7.2 Dynamometer Coupler

An AAR instrumented and certified strain gauge dynamometer coupler will be installed alternately on a hopper car and a tank car for preliminary car-into-car impacts (See Appendix D). Longitudinal force measurements will be obtained from this coupler.

#### 8.8 PHOTO INSTRUMENTATION

- a. A remote camera control system has been designed, developed and tested at the TTC for use with impact test projects. With this system, long-line remote control of up to twelve high speed cameras, including start, stop, timing synchronization, etc. can easily and reliably be accomplished. This system will be used to control seven high speed motion picture cameras for the dynamic test series.
- b. Timing synchronization will be provided each camera from the central IRIG-B timing signal source. This will permit exact correlation of each photo frame with all recorded data from the transducers.

SPEED TRAP SPECIFICATION DATA

Miles Per Hour	Feet Per Second	SWITCH INTERVAL - TIME (SECONDS)				
		1 ft	2 ft	3 ft	4 ft	5 ft
2	2.93	0.341	0.683	1.024	1.365	1.706
4	5.87	0.170	0.341	0.511	0.681	0.852
6	8.80	0.114	0.227	0.341	0.445	0.568
8	11.73	0.085	0.171	0.256	0.341	0.426
10	14.67	0.068	0.136	0.204	0.273	0.341
12	17.60	0.057	0.114	0.170	0.227	0.284
14	20.53	0.049	0.097	0.146	0.195	0.244
16	23.47	0.043	0.085	0.128	0.170	0.213
18	26.40	0.038	0.076	0.114	0.152	0.189
20	29.33	0.034	0.068	0.102	0.136	0.170
22	32.27	0.031	0.062	0.093	0.124	0.155
24	35.20	0.028	0.057	0.085	0.114	0.142
26	38.13	0.026	0.052	0.079	0.105	0.131
28	41.07	0.024	0.049	0.073	0.097	0.122
30	44.00	0.023	0.045	0.068	0.091	0.114
32	46.93	0.021	0.043	0.064	0.085	0.107
34	40.87	0.020	0.040	0.060	0.080	0.100
36	52.80	0.019	0.038	0.057	0.076	0.095
38	55.73	0.018	0.036	0.054	0.072	0.090
40	58.67	0.017	0.034	0.051	0.068	0.085
42	61.60	0.016	0.032	0.049	0.065	0.081
44	64.53	0.015	0.031	0.046	0.062	0.077
46	67.47	0.015	0.030	0.044	0.059	0.074
48	70.40	0.014	0.028	0.043	0.057	0.071
50	73.33	0.014	0.027	0.041	0.055	0.068

Figure F-1

## 8.9 DATA ACQUISITION SYSTEM

### 8.9.1 Signal Conditioning Equipment

A separate signal conditioning amplifier will be provided for each transducer, sensor or timing signal required. These signal conditioners are the Dynamics 7600 series and include selectable filtering, isolated input-output circuits and separate, individually controllable outputs for magnetic tape recorder, galvanometer (or strip chart recorder) and VCO's (Voltage Controlled Oscillator for multiplexing). The signal conditioner also provides a controllable excitation or operating voltage source (0-30 VDC) for each transducer as well as a convenient means of controlling set-up calibration, balance and output signal levels.

### 8.9.2 Multiplexing Equipment

A nine channel multiplex/demultiplex system consisting of IRIG constant bandwidth channels 1A through 9A manufactured by Metroplex Corp. will be used to multiplex and record up to nine channels of test data. The frequency response of the nine multiplexed channels is 1 KHz. An autotest calibration system is included to adjust bandcenter and check upper bandwidth of channel prior to recording or reproducing data. Pre and Post-test calibrations will be recorded on magnetic tape along with the data.



### 8.9.3 Magnetic Tape Recorders

- a. One Bell and Howell CPR4010 14 track tape recorder with 12 FM record/reproduce channels and 2 direct record/reproduce channels. The multiplexed data will be recorded on the FM tape channels. The frequency response of the FM tape channels is 10KHz at the 30 IPS tape speed which will be the recording speed.
- b. An Ampex FR 2000 tape recorder with reproduce channels compatible with the Bell and Howell 4010 will be used to reproduce the data for data reduction.

### 8.9.4 Strip Chart Recorders

- a. 100% back-up of all recorded data will be provided by strip chart recorders. The primary instrument of this type to be employed is the Bell and Howell Model 5-134 Oscillographic Recorder. This is an 18 channel system and will use fluid damped galvanometers capable of up to 5 KHz frequency response. These are light-beam type galvanometers and will be used with an ultra-violet developing type of light sensitive recording chart paper. No more than 12 channels of data, including IRIG-B timing will be recorded on the oscillograph. The additional data channels will be recorded in real time on an eight channel pen type strip chart recorder.

b. The strip chart/oscillographic recording of all data channels will provide an immediate, quick-look data read out for field inspection and instrumentation check-out/verification prior to final data reduction and analysis of the simultaneously recorded analog magnetic tape data.

#### 8.9.5 Time Code Generation

A time code generator and translator manufactured by Datum will be used to provide IRIG-B timing. This will be recorded on a selected tape channel during test to ensure correct time correlation of test data during data reduction. In addition to the IRIG-B time code format, slow codes at 1 PPS, 10 PPS and 1000 PPS and digital out-puts are provided for use during recording and data reduction.

9.0 PHOTOGRAPHY TECHNIQUES

## 19.0 PHOTOGRAPHY TECHNIQUES

- a. The Photo Instrumentation group will support the tests with a maximum of eleven motion picture cameras, one CCTV camera and a portable TV camera. This is in addition to the still coverage available.
- b. The eleven motion picture cameras are made up of the following:
  - 7 - 16mm Locams, variable from 24 to 500 FPS
  - 1 - 16mm Milliken, variable from 24 to 500 FPS
  - 1 - 16mm Milliken, capable of either 128 or 400 FPS
  - 1 - 16mm Arriflex, variable from 24 to 50 FPS
  - 1 - 16mm Arriflex, capable of 24 FPS
- c. The seven Locams will be used for prime coverage. The two Millikens will be used for backup.
- d. The exact location and number of cameras for each test will be determined as far in advance as possible. Due to the change of location of various test cars in the consist each camera station location will have to be determined precisely at the time of test. During the preliminary tests, it is expected that less than seven high speed cameras will be used. The later series will require the maximum high speed coverage. IRIG-B timing will be provided to all high speed camera stations.
- e. The photographic data will be recorded for each camera station and compiled in real time. This data will include items such as camera status, number, position, frame rate, focal length of lens, f stop, etc.

- f. Red and white square targets will be placed to enhance photography.
- g. Target distances and positions will be recorded.
- h. Best CCTV coverage will be determined for each test. The CCTV coverage will be utilized for quick look data.
- j. 16 mm Ektachrome EF daylight ASA 160 will be used as prime instrumentation film. 16mm Ektachrome MS ASA 64 will be used for documentation coverage. The motion picture film will be processed off-site.
- k. Camera stations will be numbered sequentially. Starting at the northern part of the test track and working south, the odd numbers will be on the west side of the track and the even numbers on the east side. To differentiate camera station, CC will indicate CCTV; D will indicate documentary coverage and instrumentation cameras will be numbered.

Example: Sta. 1 would be an instrumentation camera stationed on the northwest side of the track. Sta. CC 2 would be a CCTV stationed on the east side of the track. In addition, each camera station will be referenced to a master surveyed grid map. The coordinate data for each station will be compiled for each test and a map will be prepared indicating each camera station.

APPENDICES

- Appendix A List of Instrumentation
  - Appendix B Truck Spring Bolster Stiffness
  - Appendix C Coupler Vertical Spring Rate
  - Appendix D Car Into Car Impacts
  - Appendix E Manipulation of Data Channels
  - Appendix F Listing of Plot Example
  - Appendix G Drawings for Equipment
  - Appendix H Important Correspondence
- Index to Appendix H

LIST OF INSTRUMENTATION

<u>MEASUREMENT DEVICE</u>	<u>LOCATION</u>	<u>NUMBER</u>	<u>CALIBRATION</u>
Strain Gauge	Truck on impact end of hopper car (Fig. E-1)	2	100 Kips $\pm$ 10% on bolster
Strain Gauge	Sill on impact end of hopper car (Fig. E-2)	6	1 1/4 Kips $\pm$ 10%
Strain Gauge	Shank of coupler on hopper impact end, recessed (Fig. E-3)	4	1 1/4 Kips $\pm$ 10%
Accelerometer	Impact end of hopper car sill near strain gauges (Fig. E-2)	1	50 g's $\pm$ 10%
String Pot	Body to side frame on each corner of hopper (Fig. E-4)	8	-3" to +9" $\pm$ 1/10"
String Pot	Coupler longitudinal displacement on impact end of hopper	1	-2" to +4" $\pm$ 1/10"
Dynamometer Coupler	Impact end of hopper car pre-test only	1	- - -
Speed Gates	Track before and after impact location (Fig E-5)	2	0 -35 mph $\pm$ 1/10 mph
Dial Gauges	Car underframe to reference (Appendixes B and C)		- - -
Calibrated Cylinder	Truck bolster and coupler (Appendixes B and C)	1	400 Kips $\pm$ 1 Kip

Appendix A

CHANNEL NUMBER

DESCRIPTION

- 1. . . . . Bolster bending
- 2. . . . . Sum of strain measurements in sill
- 3. . . . . Difference of strain measurements in sill
- 4. . . . . Sill Accelerometer
- 5. . . . . Longitudinal coupler force
- 6. . . . . Coupler bending
- 7. . . . . Body to side frame deflection
- 8. . . . . Body to side frame deflection
- 9. . . . . Body to side frame deflection
- 10. . . . . Body to side frame deflection
- 11. . . . . Coupler longitudinal displacement
- 12. . . . . IRIG-B Time Code
- 13. . . . . Speed Gate Signal
- 14. . . . . Speed Gate Signal
- 15. . . . . Impact Indicator

When measurements are indicated as added or subtracted to form a channel, they may alternately be measured as separate channels and added in the data reduction. Channels are designated as C<sub>1</sub> through C<sub>20</sub>.



## Appendix B: Truck Spring and Bolster Stiffness

One truck from the hopper car and one from the tank car will be loaded by a load cell in tension as shown in Figure B-1. String pots will be used to measure the deflection between the truck bolster and reference bars that are clamped to the wheels. The reference bars will be stiff enough to have negligible deflection. The force will be incrementally increased and force and deflection and bolster strain gauge readings will be recorded until the springs bottom.

The load will then be removed and the springs replaced with blocks. The loading will then be resumed with dial indicators used to measure the bolster deflection with respect to the reference bar. The load will be incrementally increased to 50-100 kips beyond the load required to bottom the springs. Again, dial gauges and strain readings will be recorded.

The bolster and side frames tend to shift and roll under load, and the vertical displacement measurements must be taken with care so that the side frame shift or roll is not inadvertently measured as vertical deflection.

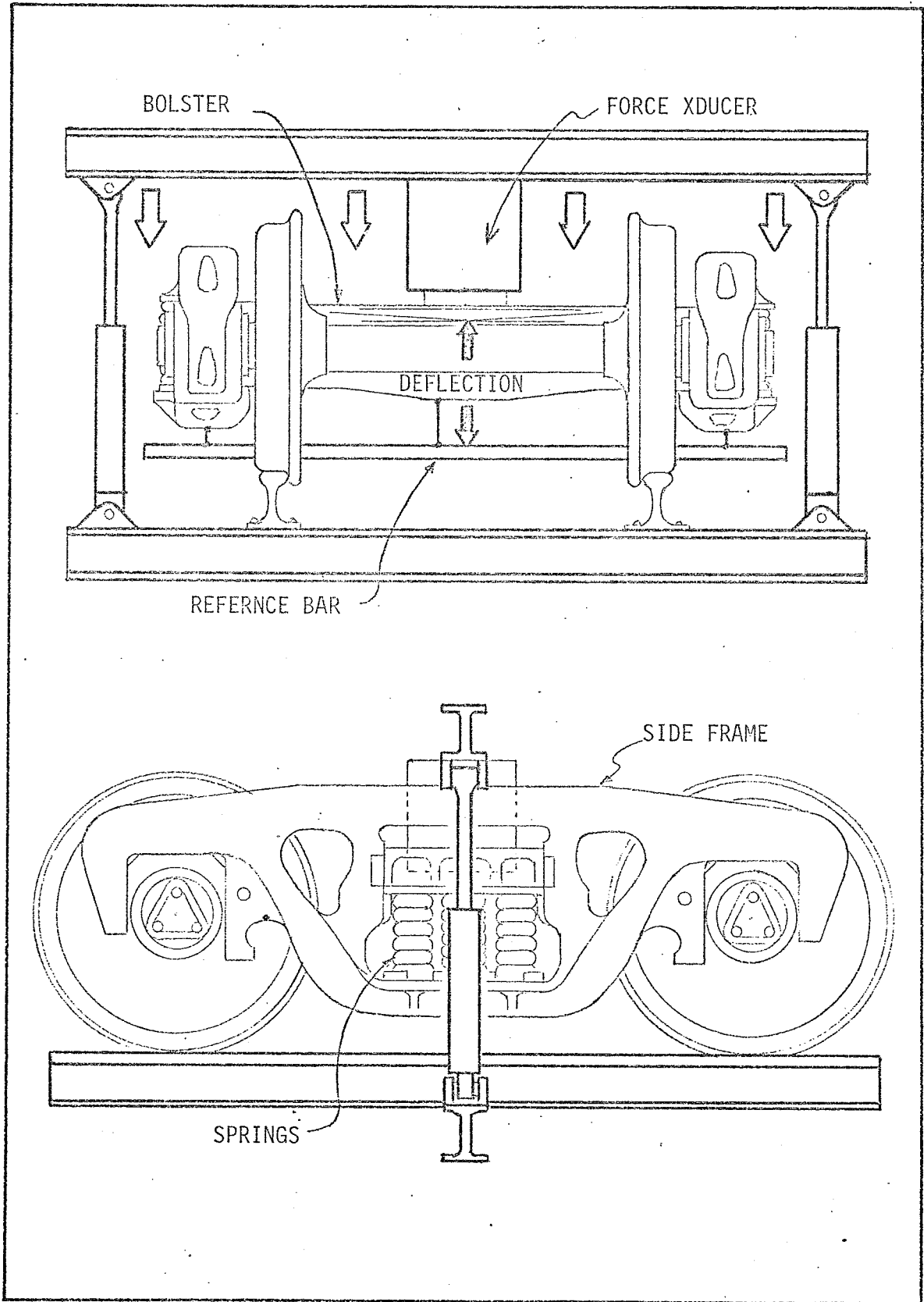
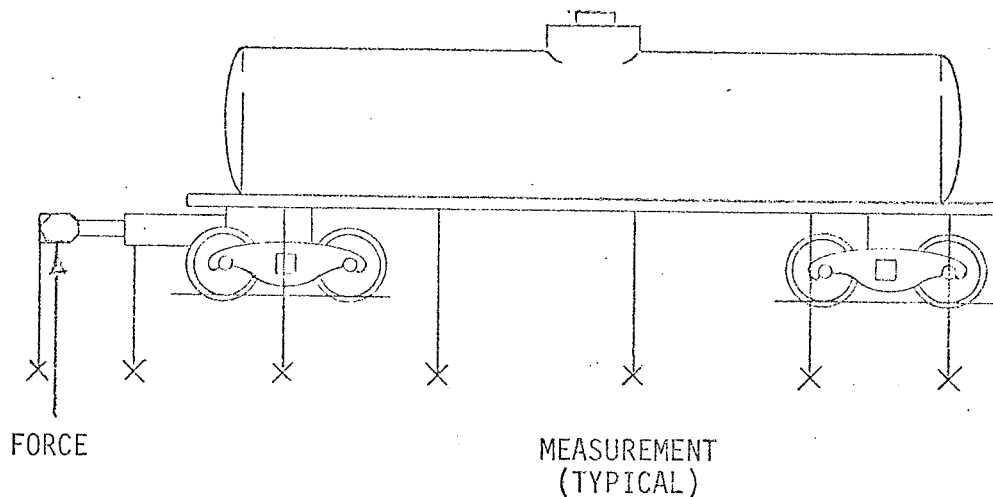


FIG. B-1

### Appendix C: Coupler Vertical Spring Rate

Apply an upward force on one car coupler in 5,000 pound increments until no load is applied on the nearest center plate (car off of bolster). Measure movement of car body at 6 points shown below using dial indicators with reference to striker face. Truck springs should be blocked to reduce car body movement on springs. Report spring rate of structure in bending and deflection curve



During application of loads, the strain gauge readings in the coupler and sill will be recorded for the hopper car.

Two series of tests are to be performed as follows:

Light car at 0 psi (no water load).

## Appendix D: Car Into Car Impacts

A standing car with no brakes applied will be impacted by an identical car moving at a specified impact speed. Draft gear will be blocked on both cars. For the hopper car into hopper car impacts, these speeds will be 5 mph and 10 mph. For the impacts between fully loaded tank cars, impact speeds will be 2 mph and 4 mph. In each test, one of the cars will be instrumented with a dynamometer coupler and longitudinal force measured. In addition, speed in and out for the impacting car and speed out for the impacted car will be recorded (Figure A-5). In the hopper car impacts, all standard hopper car instrumentation will be in operation and will be recorded. After the cars have separated (both couplers are open and cut bars tied up in this test), wayside brake trips will be used to stop the cars. Tank cars are to be pressurized to 100 psi and loaded to 62.7% water equivalent to GRL of 263,000#. 60° F temperature of H<sub>2</sub>O is not required for these tests.

## Appendix E: Manipulation of Data Channels

1. In the truck spring rate test, a calibration constant will be determined to convert channel 1 to truck force.

$$\text{Truck Force} = K_1 C_1$$

2. In the equal car impact tests, dynamometer coupler readings will be compared with channels 2, 3, and 4 to give relations between longitudinal force ( $f_L$ ) and strain on the sill. Similarly, the vertical coupler spring rate test will be used to determine the relationship between vertical force ( $f_V$ ) and channels 2, 3, and 6. Third, a compression test of the coupler will be used to determine the relationship between horizontal force and channel 5. These will yield coefficients  $A_{ij}$  and  $b_{ij}$  as shown below.

$$C_2 = A_{11}f_L + A_{12}f_V$$

$$C_3 = A_{21}f_L + A_{22}f_V$$

$$C_4 = g(f_L)$$

$$C_5 = b_{11}f_L + b_{12}f_V$$

$$C_6 = b_{21}f_L + b_{22}f_V$$

<u>Coefficient</u>	<u>Test in Which Determined</u>
$A_{11}$	hopper into hopper
$A_{12}$	vertical spring rate
$A_{21}$	hopper into hopper
$A_{22}$	vertical spring rate
$g(f_L)$	hopper into hopper
$b_{11}$	coupler compression test
$b_{12}$	vertical spring rate
$b_{21}$	=0 from theory
$b_{22}$	vertical spring rate of coupler

The equation can then be inverted to give:

$$\begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix}^{-1} = \begin{bmatrix} \bar{A}_{11} & \bar{A}_{12} \\ \bar{A}_{21} & \bar{A}_{22} \end{bmatrix}$$

$$\begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix}^{-1} = \begin{bmatrix} \bar{b}_{11} & \bar{b}_{12} \\ \bar{b}_{21} & \bar{b}_{22} \end{bmatrix}$$

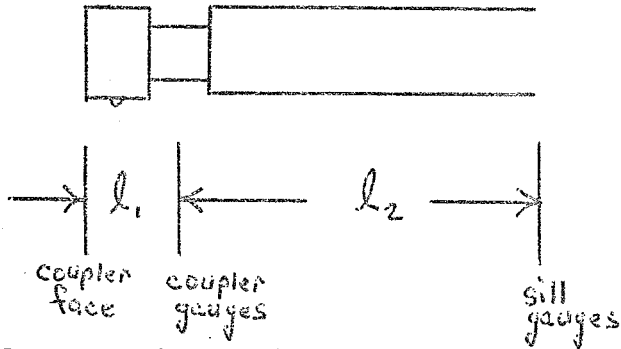
Thus, horizontal and vertical force can be calculated from the channels.

$$f_L = \bar{A}_{11} C_2 + \bar{A}_{12} C_3$$

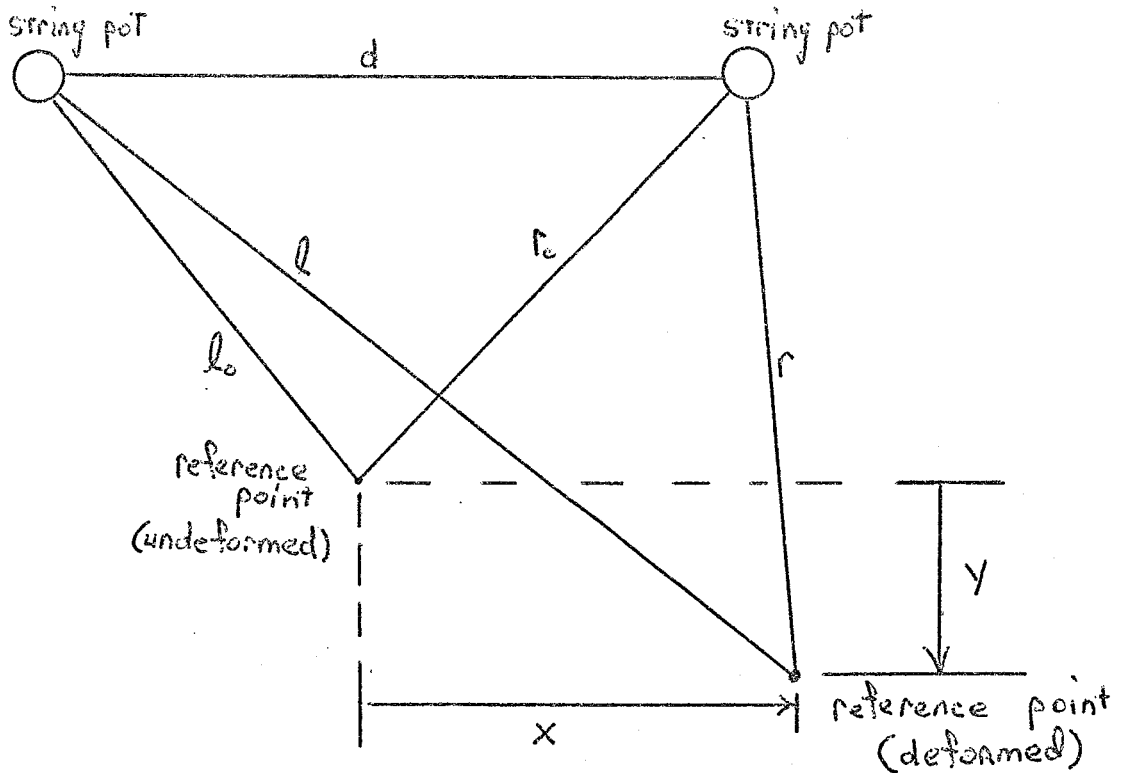
$$f_L = \bar{b}_{11} C_5 + \bar{b}_{12} C_6$$

$$f_L = g^{-1}(C_4)$$

$$f_v = \left(1 + \frac{l_1}{l_2}\right) (\bar{A}_{12} C_2 + \bar{A}_{22} C_3) - \frac{l_1}{l_2} (\bar{b}_{12} C_5 + \bar{b}_{22} C_6)$$



3. The final data manipulation will consist of converting string pot displacements to horizontal and vertical displacements. This can be done as shown below:

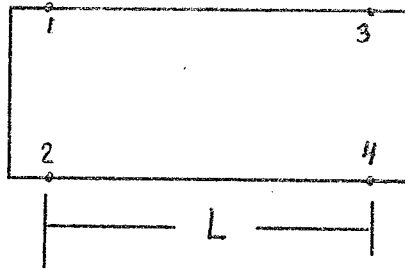


$$X = \frac{(l-r)(l+r)}{2d} - \frac{(l_c-r_c)(l_c+r_c)}{2d}$$

$$Y = \frac{\sqrt{(r+l-d)(r+l+d)(-r+l+d)(r-l+d)}}{2d}$$

$$- \frac{\sqrt{(r_c+l_c-d)(r_c+l_c+d)(-r_c+l_c+d)(r_c-l_c+d)}}{2d}$$

The total car lateral motion (X), heave motion (Y), and roll motion ( $\phi$ ) can then be determined from the x and y motions of each corner.



$$X = \frac{X_1 + X_2 + X_3 + X_4}{2}$$

$$Y = \frac{Y_1 + Y_2 + Y_3 + Y_4}{2}$$

$$\phi = \arcsin \left[ \frac{(Y_1 + Y_2) - (Y_3 + Y_4)}{L} \right]$$



APPENDIX F

LISTING AND PLOT EXAMPLE

RPI-ARR SWITCHYARD SAFETY PROGRAM (PHASE 15)  
 TEST 1 SERIES 1 RUN 1  
 07/18/75

TIME (SEC)	MEASUREMENT NUMBER							
	1	2	3	4	5	6	7	8
0.000	.70E 00	.27E 00	.31E 00	.42E 00	.69E 00	.35E 00	.91E 00	.35E 00
.001	.84E 00	.94E 00	.62E-01	.91E 00	.92E 00	.30E 00	.51E 00	.37E 00
.002	.67E 00	.67E 00	.10E 01	.97E 00	.84E 00	.31E 00	.29E 00	.96E 00
.003	.18E 00	.46E 00	.12E 00	.59E 00	.45E 00	.38E 00	.25E 00	.11E 00
.004	.38E 00	.31E 00	.42E 00	.77E 00	.74E 00	.51E 00	.41E 00	.82E 00
.005	.27E 00	.23E 00	.93E 00	.51E 00	.72E 00	.71E 00	.75E 00	.98E-01
.006	.85E 00	.21E 00	.61E 00	.82E 00	.39E 00	.97E 00	.28E 00	.94E 00
.007	.11E 00	.25E 00	.49E 00	.69E 00	.75E 00	.29E 00	.99E 00	.34E 00
.008	.63E-01	.35E 00	.55E 00	.12E 00	.80E 00	.68E 00	.90E 00	.30E 00
.009	.70E 00	.52E 00	.30E 00	.12E 00	.53E 00	.12E 00	.99E 00	.82E 00
.010	.28E-01	.75E 00	.23E 00	.67E 00	.95E 00	.63E 00	.27E 00	.91E 00
.011	.41E-01	.38E-01	.86E 00	.79E 00	.56E-01	.21E 00	.74E 00	.56E 00
.012	.74E 00	.39E 00	.87E 00	.47E 00	.85E 00	.84E 00	.39E 00	.78E 00
.013	.13E 00	.81E 00	.66E 00	.72E 00	.33E 00	.54E 00	.23E 00	.55E 00
.014	.21E 00	.29E 00	.85E 00	.52E 00	.50E 00	.30E 00	.26E 00	.69E 00
.015	.97E 00	.83E 00	.22E 00	.89E 00	.36E 00	.12E 00	.48E 00	.79E 00
.016	.42E 00	.43E 00	.72E 00	.83E 00	.91E 00	.54E-02	.38E 00	.25E 00
.017	.56E 00	.96E-01	.53E 00	.32E 00	.14E 00	.95E 00	.48E 00	.22E 00
.018	.39E 00	.82E 00	.47E 00	.38E 00	.58E-01	.96E 00	.25E 00	.87E 00
.019	.90E 00	.62E 00	.59E 00	.10E 01	.67E 00	.35E-01	.22E 00	.16E-01
.020	.10E 00	.47E 00	.90E 00	.18E 00	.96E 00	.17E 00	.39E 00	.73E 00
.021	.95E 00	.39E 00	.40E 00	.92E 00	.94E 00	.37E 00	.72E 00	.40E-02
.022	.57E 00	.36E 00	.84E-01	.23E 00	.61E 00	.63E 00	.25E 00	.84E 00
.023	.83E 00	.40E 00	.96E 00	.97E-01	.97E 00	.95E 00	.96E 00	.24E 00
.024	.78E 00	.51E 00	.17E-01	.53E 00	.15E-01	.33E 00	.87E 00	.21E 00
.025	.42E 00	.67E 00	.27E 00	.52E 00	.75E 00	.72E 00	.96E 00	.73E 00
.026	.75E 00	.90E 00	.70E 00	.79E-01	.17E 00	.29E 00	.24E 00	.82E 00
.027	.76E 00	.19E 00	.32E 00	.20E 00	.27E 00	.86E 00	.71E 00	.47E 00
.028	.46E 00	.55E 00	.13E 00	.88E 00	.70E-01	.50E 00	.36E 00	.62E 00
.029	.85E 00	.96E 00	.13E 00	.12E 00	.55E 00	.19E 00	.20E 00	.46E 00
.030	.93E 00	.44E 00	.32E 00	.93E 00	.72E 00	.95E 00	.23E 00	.80E 00
.031	.69E 00	.98E 00	.69E 00	.30E 00	.58E 00	.78E 00	.45E 00	.70E 00
.032	.14E 00	.53E 00	.25E 00	.23E 00	.12E 00	.66E 00	.85E 00	.16E 00
.033	.28E 00	.25E 00	.10E 01	.73E 00	.36E 00	.61E 00	.44E 00	.18E 00
.034	.11E 00	.98E 00	.94E 00	.78E 00	.28E 00	.62E 00	.22E 00	.77E 00
.035	.62E 00	.77E 00	.58E-01	.40E 00	.88E 00	.69E 00	.19E 00	.92E 00
.036	.82E 00	.63E 00	.37E 00	.58E 00	.18E 00	.83E 00	.34E 00	.63E 00
.037	.71E 00	.54E 00	.87E 00	.33E 00	.16E 00	.23E-01	.69E 00	.91E 00
.038	.29E 00	.52E 00	.55E 00	.63E 00	.83E 00	.28E 00	.22E 00	.75E 00
.039	.55E 00	.56E 00	.43E 00	.50E 00	.19E 00	.61E 00	.33E 00	.15E 00
.040	.50E 00	.66E 00	.49E 00	.93E 00	.23E 00	.99E 00	.34E 00	.11E 00
.041	.14E 00	.83E 00	.73E 00	.93E 00	.97E 00	.44E 00	.93E 00	.64E 00
.042	.47E 00	.59E-01	.17E 00	.49E 00	.39E 00	.95E 00	.21E 00	.72E 00
.043	.48E 00	.35E 00	.79E 00	.60E 00	.49E 00	.52E 00	.67E 00	.38E 00
.044	.18E 00	.70E 00	.60E 00	.29E 00	.29E 00	.15E 00	.33E 00	.59E 00
.045	.57E 00	.12E 00	.60E 00	.53E 00	.77E 00	.85E 00	.17E 00	.36E 00
.046	.64E 00	.60E 00	.79E 00	.34E 00	.94E 00	.61E 00	.20E 00	.70E 00
.047	.41E 00	.14E 00	.16E 00	.71E 00	.80E 00	.43E 00	.42E 00	.60E 00
.048	.86E 00	.74E 00	.72E 00	.64E 00	.34E 00	.32E 00	.82E 00	.65E-01
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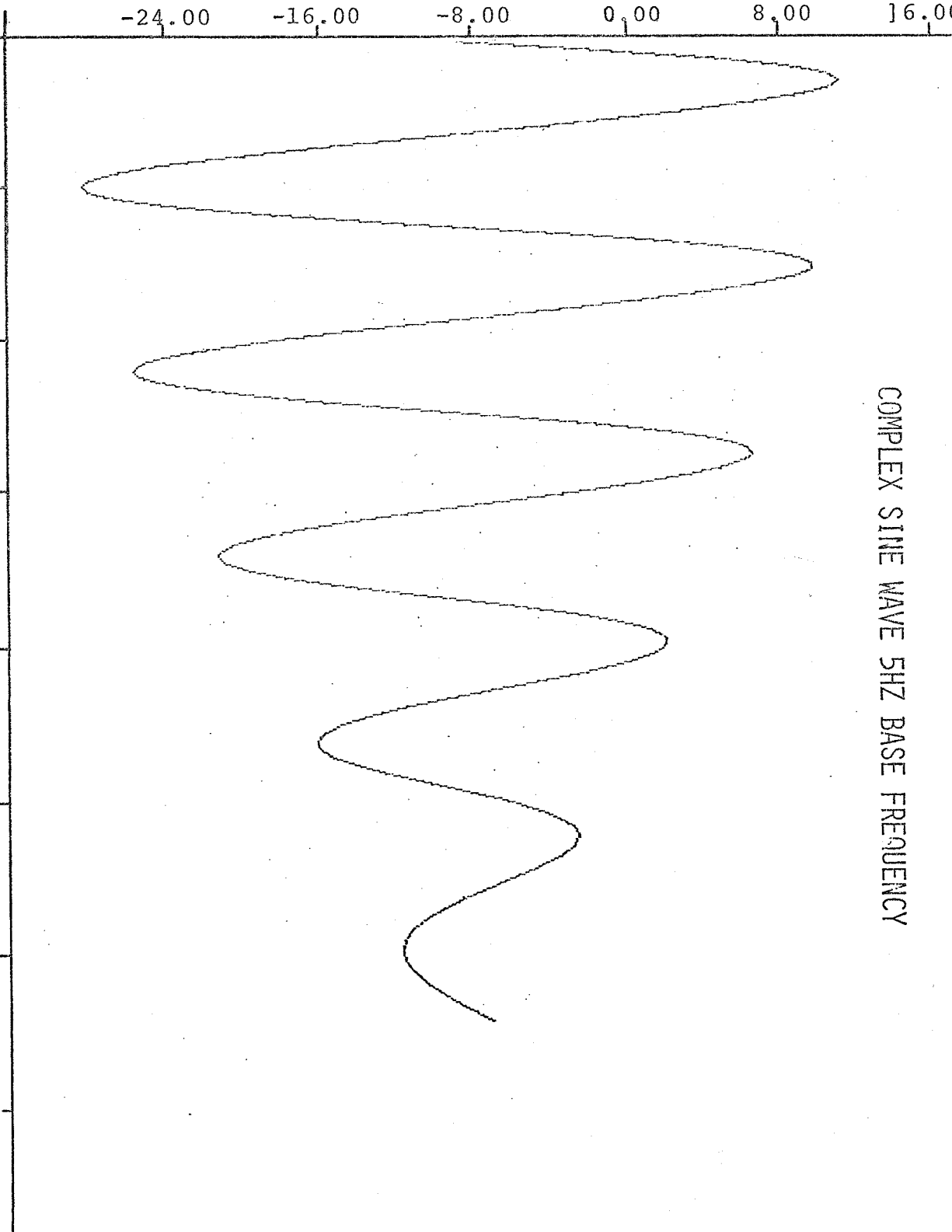
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COMPLEX SINE WAVE 5HZ BASE FREQUENCY

ARRAY

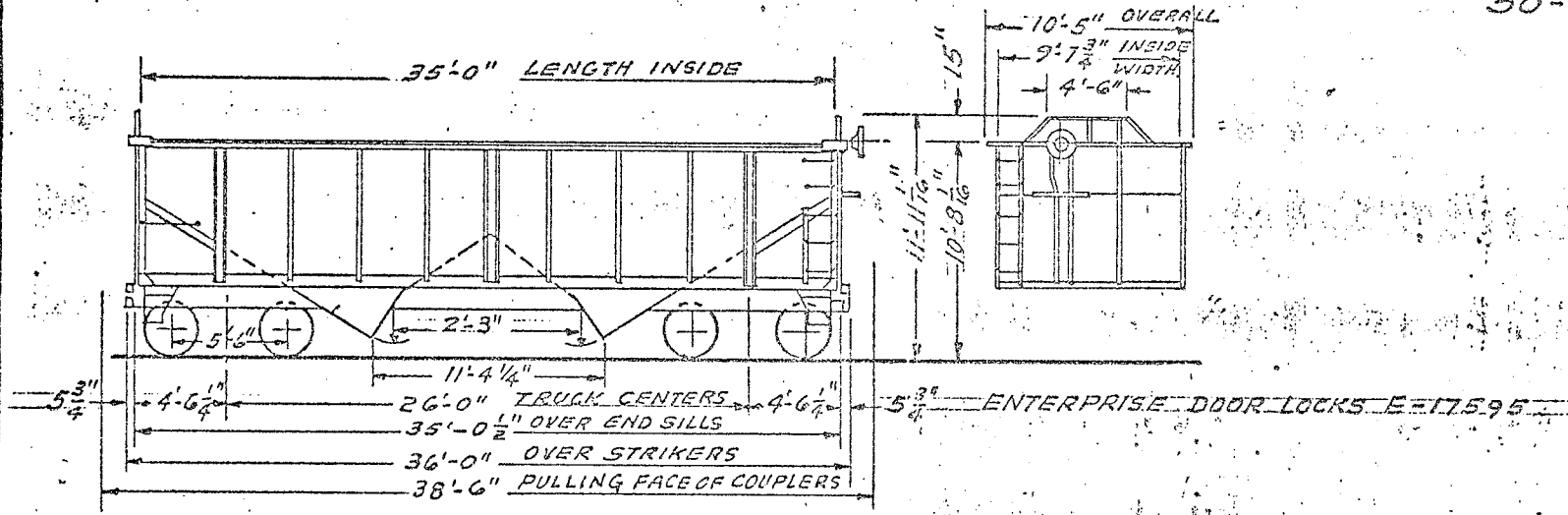
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APPENDIX G

DRAWINGS FOR EQUIPMENT

50-TON HOPPER CARS



GENERAL CAR DATA		50-TON TRUCK DATA		NO. CARS	CAR SERIES
Gen. Arrangement <i>F-17583</i>	Copy. Cu. Ft. <i>2046</i>	No. <i>99</i>	Type <i>S-2A</i>		
Brake Arrangement <i>F-17585</i>	With 10" Heap Cu. Ft. <i>2309</i>	Dwg. <i>E-17611</i>	Copy. <i>5 1/2" x 10"</i>	Journals <i>FRICITION BEARING</i>	
AAR Class <i>HM</i>	Total Copy. Cu. Ft.	Wt. <i>7600#</i>	Bowl Dia. <i>12"</i>	Ped. Adapter	
L&N Equip. Code <i>202</i>	Eq. End Hopper Cu. Ft.	Wheels <i>33" C-22940</i>	Side Frame <i>FS-4110, F-16656</i>	Axles <i>5 1/2" x 10" B-10553</i>	
Built By <i>P-S, Lot 8040</i>	Center Hopper Cu. Ft.	Side Frame <i>FS-4110, F-16656</i>	Bolster <i>F5-4158, E-17613</i>	Brake Beams <i>#18, B-16301</i>	
Built or Rebt. <i>APR, 1952, FEB, 1953</i>	Floor	Bolster <i>F5-4158, E-17613</i>	Bowl Wear Plate	Brake Shoes <i>AAR-1A</i>	
Taken From	Floor Copy.	Bowl Wear Ring	Bowl Wear Ring	Trk. Mounted Brakes	
Clearance Plate <i>B</i>	Lining Side or Interior	Live Lever <i>7" x 14" SH-36968</i>	Live Lever <i>7" x 14" SH-36968</i>		
Curve Negotiability-with 40'6" car	Lining End	Dead Lever <i>5" x 10" SH-37831</i>	Dead Lever <i>5" x 10" SH-37831</i>		
Average Lt. Wt. <i>43,800</i>	No. DF Belts	Bottom Rod (THRU) <i>SH-36178</i>	Bottom Rod (THRU) <i>SH-36178</i>		
Average Id. Lmt. <i>133,200</i>	No. Lading Anchors	TRUCK SPRINGS-PER TRUCK	MISCELLANEOUS		
Center of Gravity	Movable Bulkheads	Outer <i>10 SH-35480 (D-3)</i>			
Air Brakes <i>AB-1012</i>	No. Chain Tie Downs	Inner <i>4 SH-35481 (D-3)</i>			
Brake Regulator	Stake Pockets Per Side	Snubber			
Hand Brake <i>MINER, E-17591</i>	Gates or Doors <i>C-17632</i>	Shock Absorber			
Cushioning	Running Boards	RIDE CONTROL SPRGS. PER TRK.			
Coupler <i>B-E60B-HT</i>	Vibrator Attachment	Outer			
Yoke <i>C-9965</i>	Roof	Inner			
Draft Gear <i>C-13268, E-16558</i>	Removable Cover	Side <i>4 SH-36402</i>			
Striker <i>E-17593</i>	Drop Ends	Friction Casting <i>C-16138</i>			
Back Stop & C. Filler <i>E-17594</i>	Coiled Steel Cradles				

84200-85199

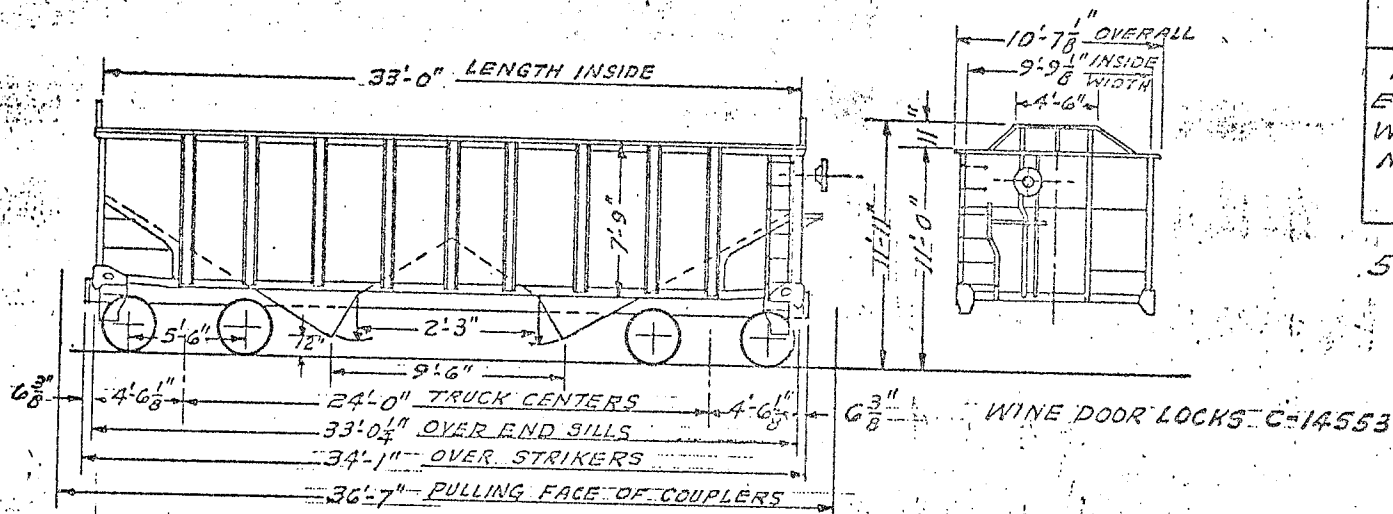
873

NO. CARS CAR SERIES

L & N R. R. CO.  
MECH. ENGINEERS OFFICE  
LOUISVILLE, KY.

REVISION SHEET NO.

H-12



SERIES	TRUCK.
115500-119999 EXCEPT 150 CARS WHICH HAVE TRUCK NO. 75-A.	71-B E-20098
	75-A E-20175

50-TON HOPPER CARS

GENERAL CAR DATA

50-TON

TRUCK DATA

Gen. Arrangement <i>F-24199</i>	Copy. Cu. Ft. <i>2020</i>	No. <i>71B</i> Type	Side Bearing <i>SEE TRK. DWG.</i>
Brake Arrangement <i>F-24203</i>	With 10" Heap Cu. Ft. <i>2280</i>	Dwg. <i>E-20098</i> Copy. <i>5 1/2" X 10"</i>	Journals <i>FRICTION BEARING</i>
AAR Class <i>HM</i>	Total Copy. Cu. Ft.	Wt. Bowl Dia. <i>12"</i>	Ped. Adapter
L&N Equip. Code <i>204</i>	Ea. End Hopper Cu. Ft.	Wheels <i>33" C-22940</i>	Axles <i>5 1/2" X 10" B-10553</i>
Built By Lot <i>JOB 450 234, 347</i>	Center Hopper Cu. Ft.	Side Frame <i>F5-3938, D-14495</i>	Brake Beams <i>#18, C-19397</i>
Built or Reblt. <i>L&amp;N. SO. LOU. 1960-61</i>	Floor	Bolster <i>F5-3939, D-14496</i>	Brake Shoes <i>AAR-1A</i>
Taken From <i>SEE NOTE 1.</i>	Floor Copy.	Bowl Wear Plate	Trk. Mounted Brakes
Clearance Plate <i>B</i>	Lining Side or Interior	Bowl Wear Ring	
Curve Negotiability-with 40'8" car	Lining End	Live Lever <i>8" X 16" SH-20684</i>	
Average Lt. Wt. <i>41,000#</i>	No. DF Belts	Dead Lever <i>8" X 16" SH-20684</i>	
Average Ld. Lmt. <i>136,000#</i>	No. Lading Anchors	Bottom Rod (UNDER) <i>SH-20685</i>	
Center of Gravity	Movable Bulkheads	TRUCK SPRINGS PER TRUCK	MISCELLANEOUS
Air Brakes <i>AB 10" X 12" OR CACO Q.R.V.</i>	No. Chain Tie Downs	Outer <i>SEE TRK. DWG.</i>	<i>1. 60000-68149, 72200-72397</i>
Brake Regulator	Stake Pockets Per Side	Inner " " "	<i>81950-82199, 88800-88994</i>
Hand Brake	Gates or Doors <i>E-23543</i>	Snubber " " "	
Cushioning	Running Boards	Shock Absorber	
Coupler <i>B-E60B-HT</i>	Vibrator Attachment	RIDE CONTROL SPRGS. PER TRK.	
Yoko	Roof	Outer <i>SEE TRK. DWG.</i>	
Draft Gear	Removable Cover	Inner " " "	
Striker <i>E-14480</i>	Drop Ends	Side " " "	
Back Stop & C. Filler <i>E-14481</i>	Coiled Steel Cradles	Friction Casting	

115500-119999

4268

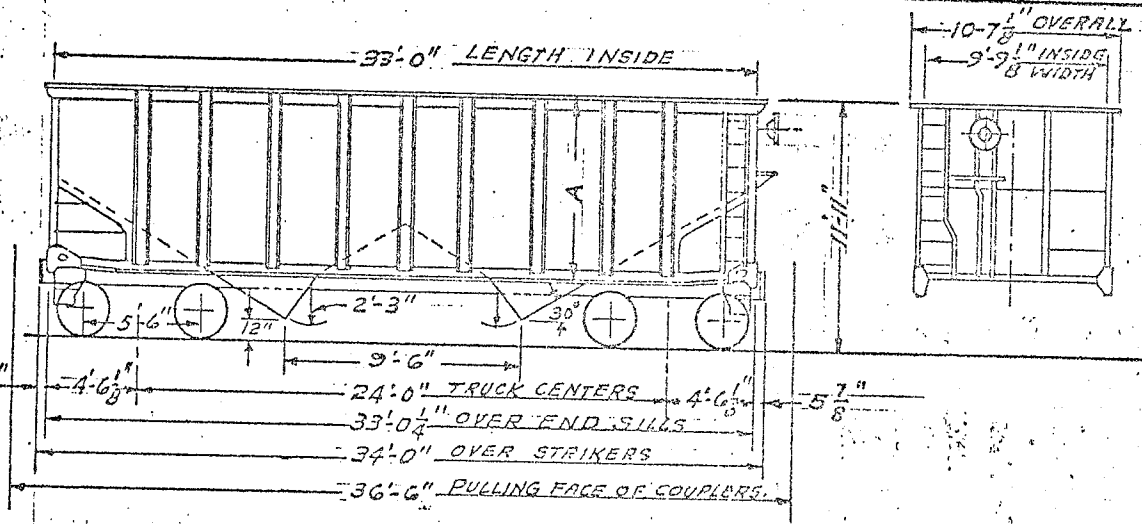
NO. CARS CAR SERIES

L & N R. R. CO.  
MECH. ENGINEERS OFFICE  
LOUISVILLE, KY.

REVISION SHEET NO.

H-15

111  
1118



SERIES	TRUCK No	SERIES	DOOR LOCKS
130000-131699 131900-132299	86 D-16238	132300-132499 131100-131299	E-16252 WINE ADJ.
130000-131699 132300-132499	87 E-16401	130000-131099 131300-132299	E-16402 ENTERPRISE
131700-131899	90 D-16600		

60-TON HOPPER CARS

GENERAL CAR DATA

60-TON TRUCK DATA

Gen. Arrangement	Capcy. Cu. Ft. 2450
Brake Arrangement	With 10" Heap Cu. Ft. 2718
AAR Class HM	Total Capcy. Cu. Ft.
L&N Equip. Code 210	Ea. End Hopper Cu. Ft.
Built By P-S. Lot 801, 808	Center Hopper Cu. Ft.
Built or Reblt. L&N 1964 S. LOU.	Floor
Taken From 32000-33999, 76150-81949	Floor Capcy.
Clearance Plate B	Lining Side or Interior
Curve Negotiability-with 40'6" car	Lining End
Average Lt. Wt. 40,900	No. DF Belts
Average Ld. Lmt. 136,100	No. Lading Anchors
Center of Gravity	Movable Bulkheads
Air Brakes AB-1012 (CACO)	No. Chain Tie Downs
Brake Regulator	Stake Pockets Per Side
Hand Brake E-16398, E-16472	Gates or Doors SEE NOTE 2
Cushioning	Running Boards
Coupler B-EGOB-HT	Vibrator Attachment
Yoke C-9965	Roof
Draft Gear	Removable Cover
Striker E-16096, E-16410	Drop Ends
Back Stop & C. Filler E-16468, E-16473	Coiled Steel Cradles

No. 86, 87, 90 Type S-2A, A-3	Side Bearing C-16140
Dwg. SEE TABLE Capcy. 5 1/2" x 10"	Journals FRICTION BEARING
Wt. SEE NOTE 1. Bowl Dia. 12"	Ped. Adapter
Wheels 33" C-22940	Axles 5 1/2" x 10" B-10553
Side Frame SEE TRK. DWG.	Brake Beams #18, B-16301
Bolster " " "	Brake Shoes AAR-1A
Bowl Wear Plate	Trk. Mounted Brakes
Bowl Wear Ring	
Live Lever SEE TRK. DWG.	
Dead Lever " " "	
Bottom Rod (THRU) " " "	
TRUCK SPRINGS PER TRUCK	
Outer SEE TRK. DWG.	MISCELLANEOUS
Inner " " "	1. #86 WT. - 7640#
Snubber " " 4	#87 WT. - 7250#
Shock Absorber	#90 WT. - 7840#
RIDE CONTROL SPRGS. PER TRK.	2. WINE E-23543
Outer SEE TRK. DWG.	ENTERPRISE E-23773
Inner " " "	
Side " " "	
Friction Casting	

130000-131699  
DIM. A = 8'-8"

131700-132499  
DIM. A = 8'-5 3/4"

2423

NO. CARS

CAR SERIES

L & N R. R. CO.  
MECH. ENGINEERS OFFICE  
LOUISVILLE, KY.

REVISION:

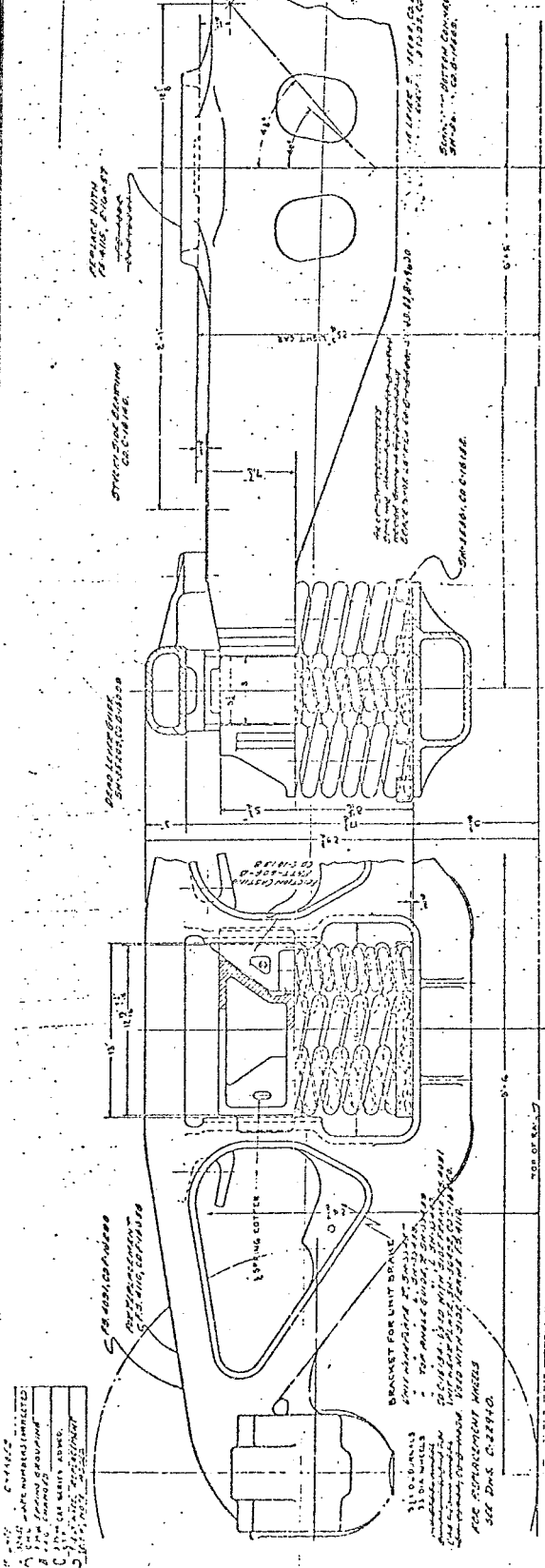
SHEET NO.  
11-17

LOUISVILLE & NASHVILLE R.R.  
 TRUCK NO. 89  
 L 16238

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NO. 1016	NO. 1017	NO. 1018	NO. 1019	NO. 1020	NO. 1021
NO. 1022	NO. 1023	NO. 1024	NO. 1025	NO. 1026	NO. 1027
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NO. 1094	NO. 1095	NO. 1096	NO. 1097	NO. 1098	NO. 1099
NO. 1100	NO. 1101	NO. 1102	NO. 1103	NO. 1104	NO. 1105



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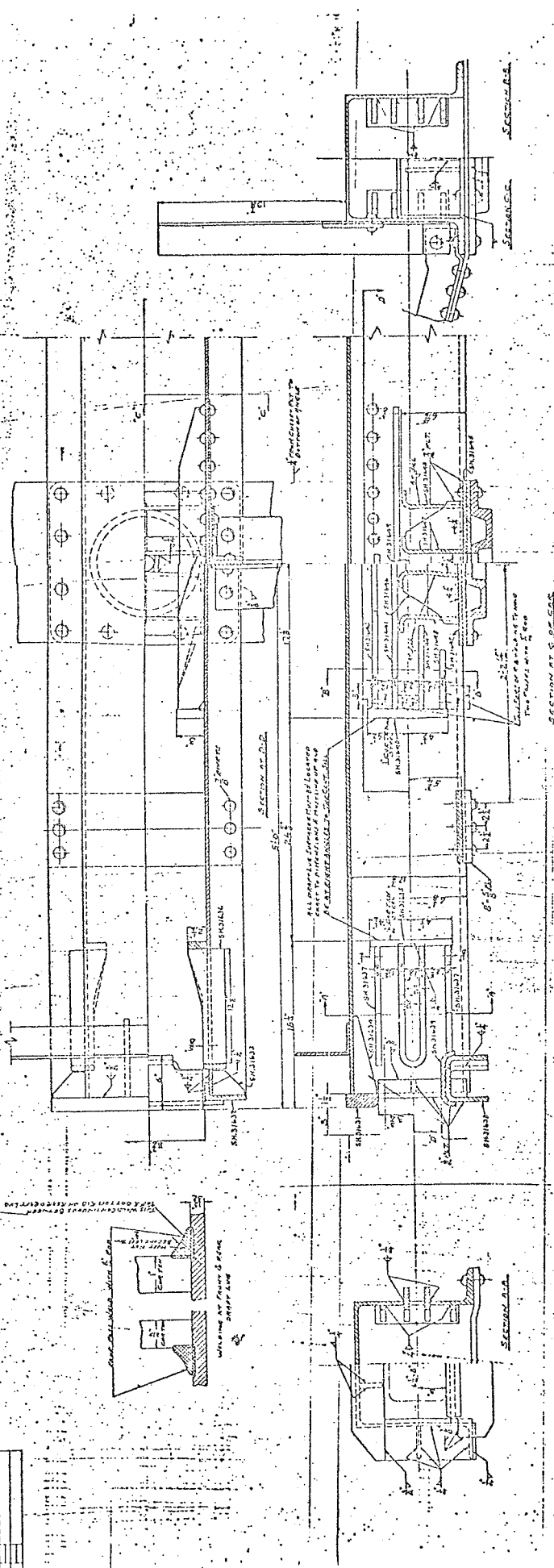
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 BRASS NAMEPLATE ON THE BACK OF THE  
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NO.	DESCRIPTION



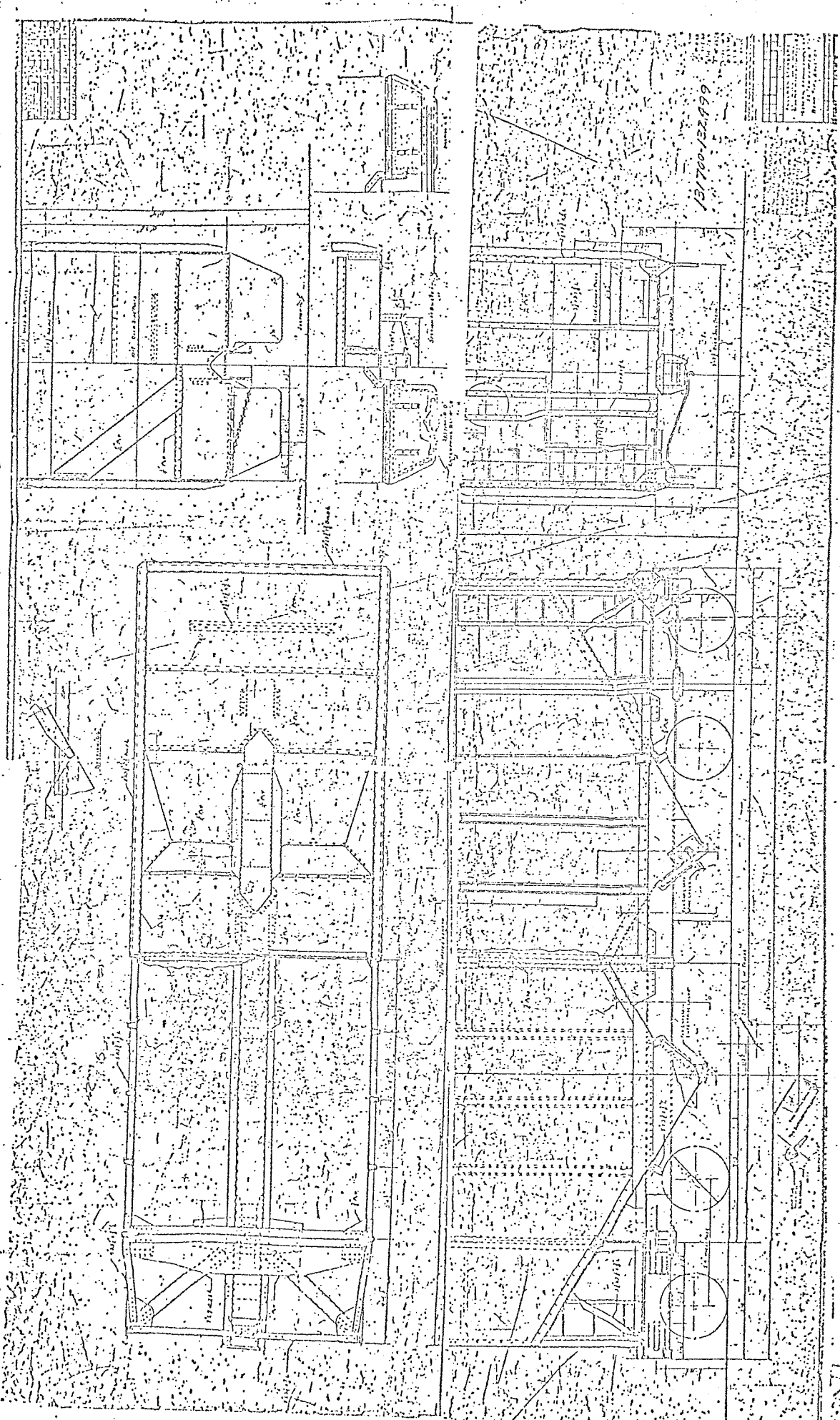
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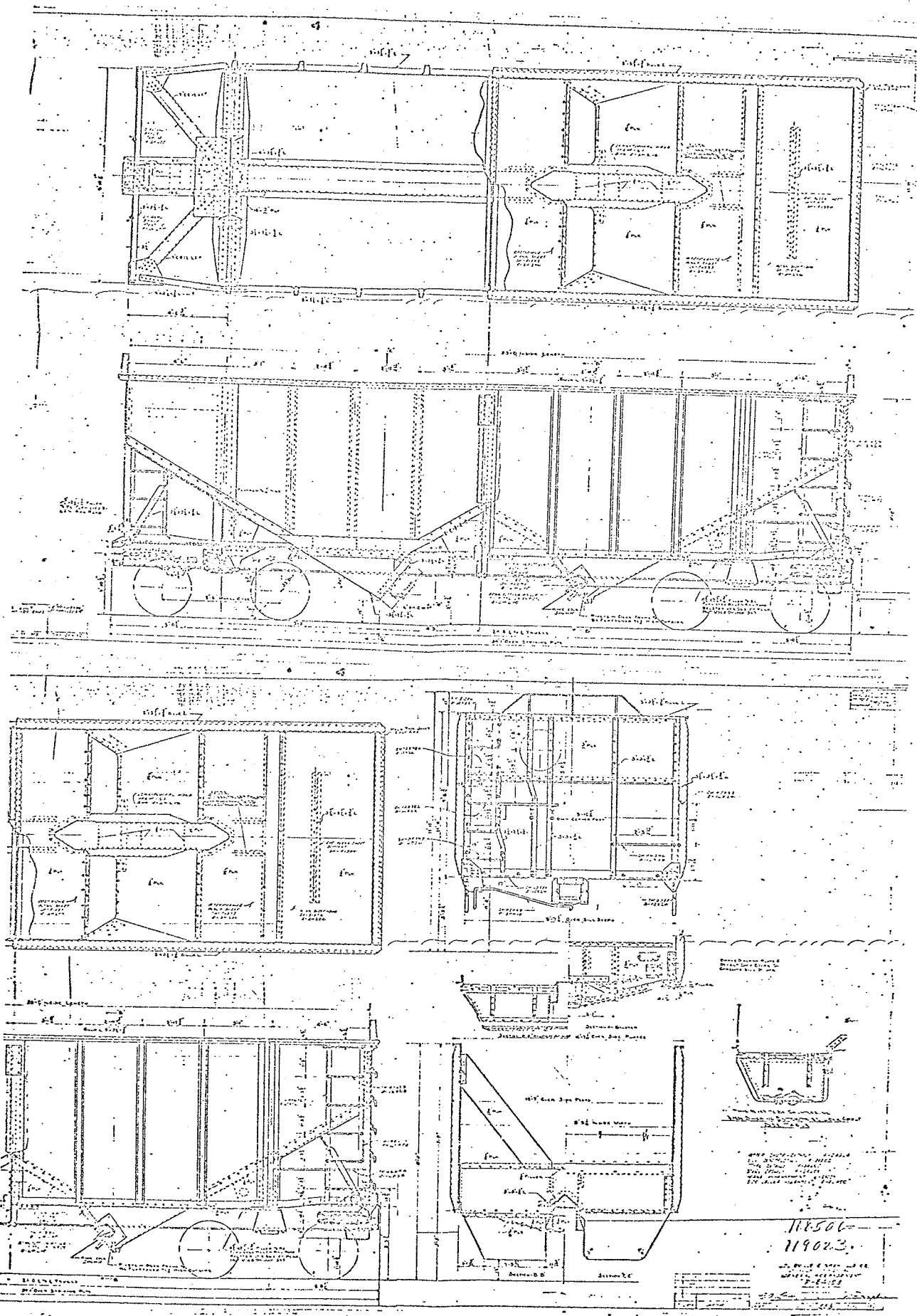
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LOUISVILLE & NASHVILLE R.R.  
DRAFT BILL  
F 1400A

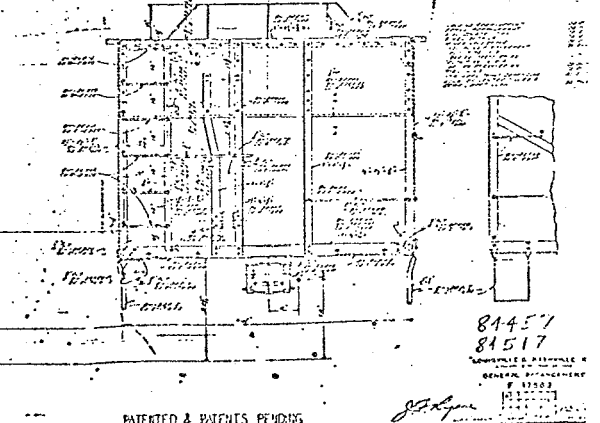
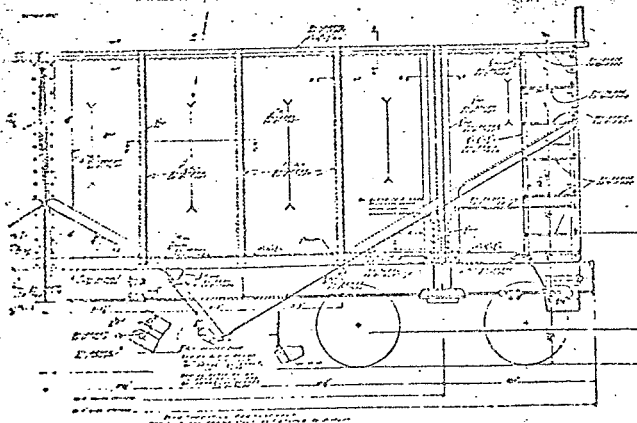
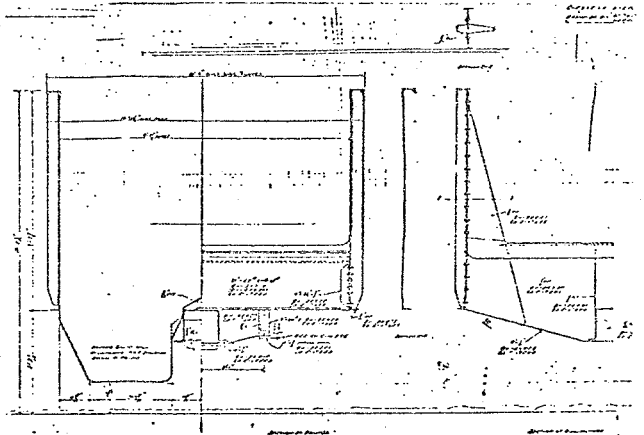
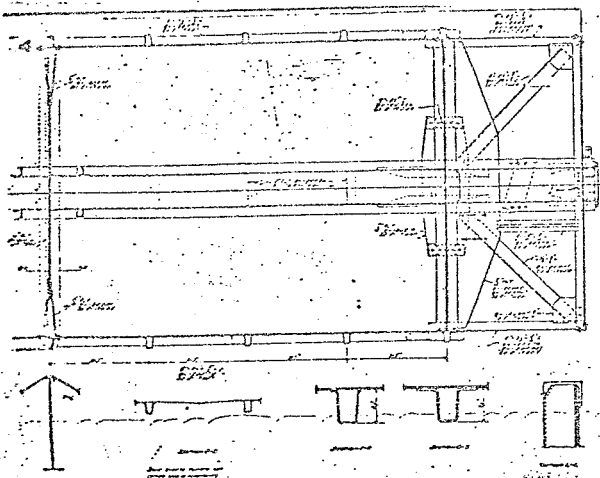
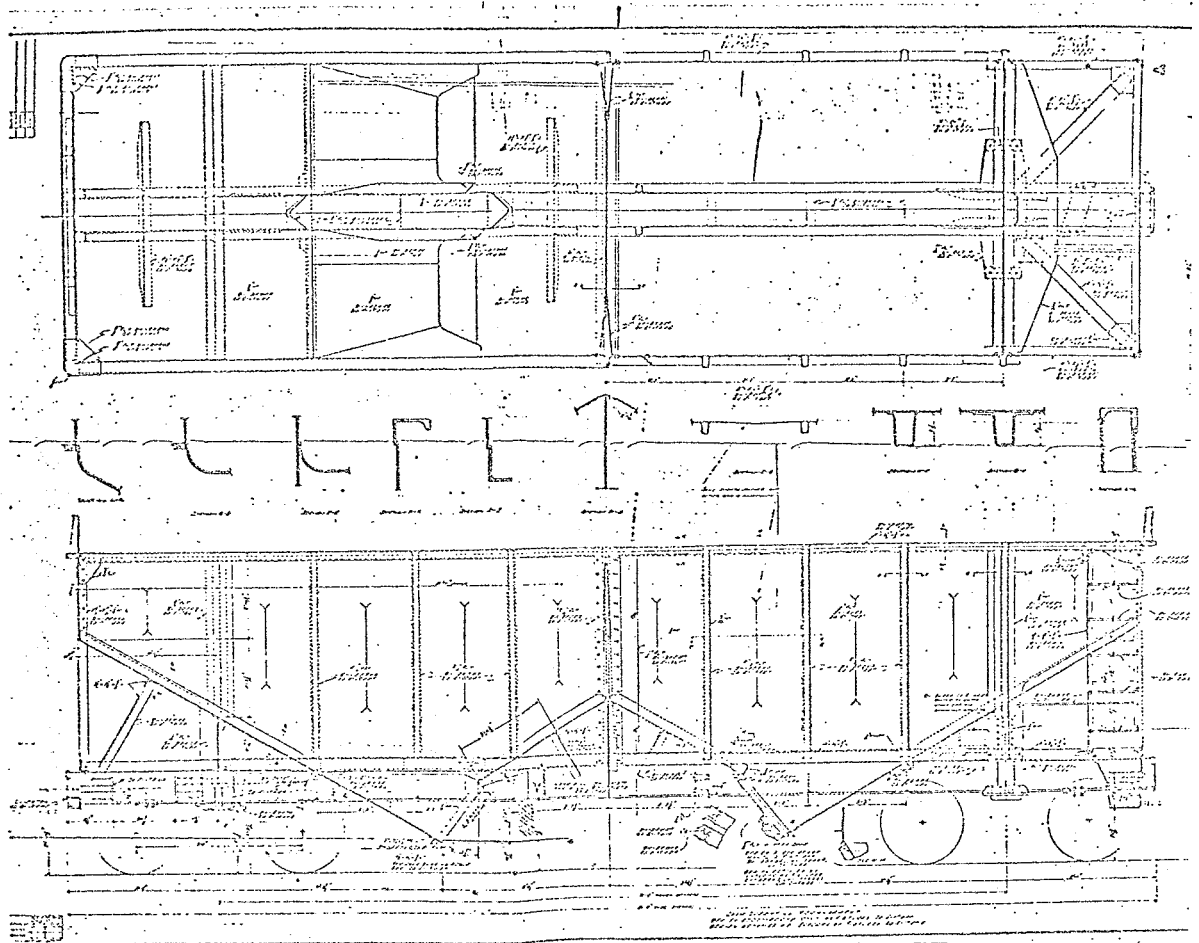
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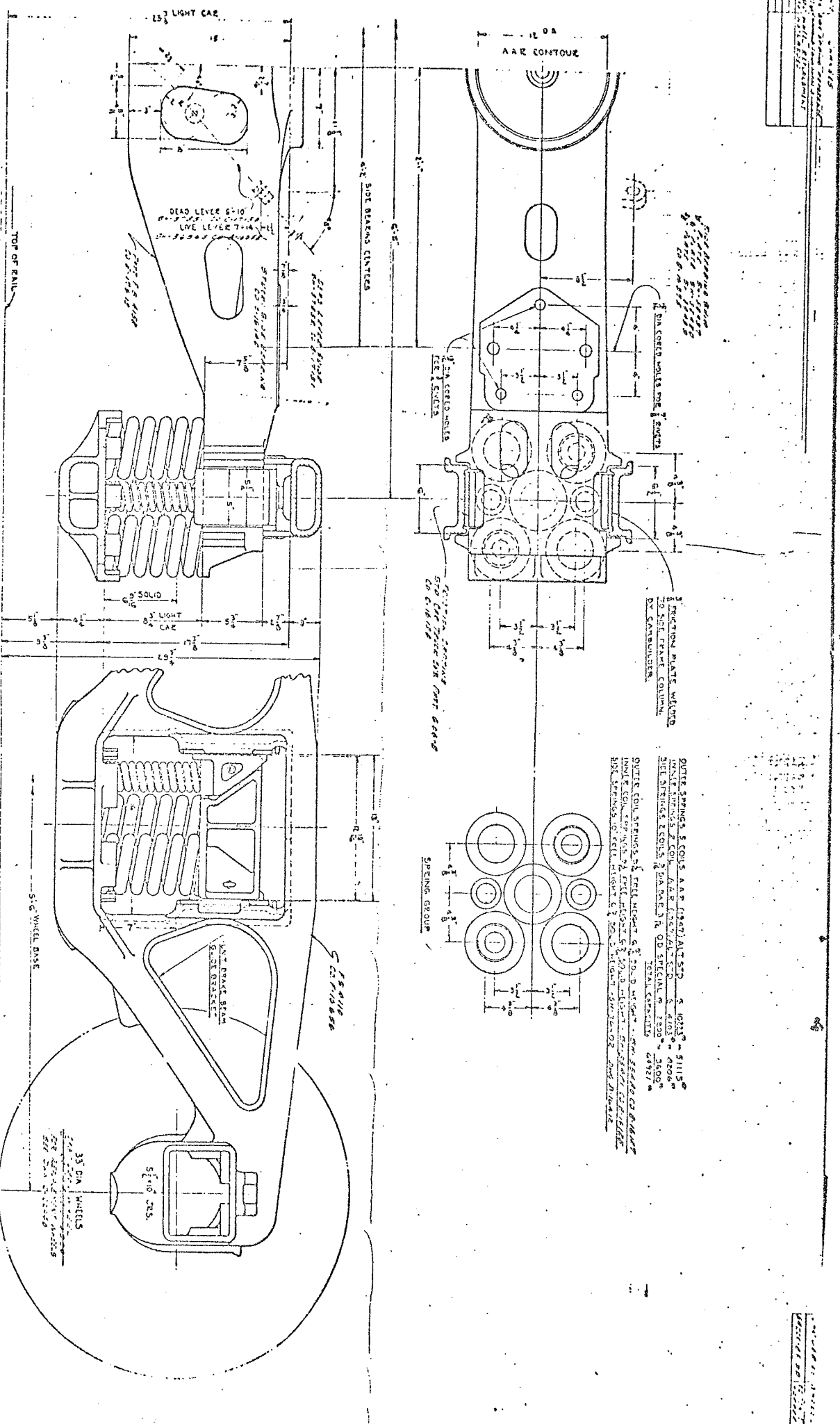
U.S. DEPARTMENT OF AGRICULTURE  
BUREAU OF PLANT INDUSTRY  
WASHINGTON, D. C.



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PATENTED & PATENTS PENDING

*J. H. ...*

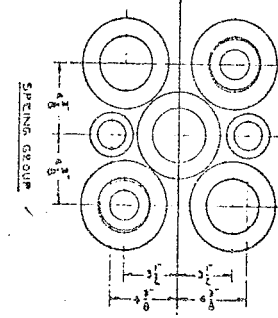


PERFORMANCE DATA  
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 2. 10000 LBS. GROSS WEIGHT  
 3. 10000 LBS. GROSS WEIGHT  
 4. 10000 LBS. GROSS WEIGHT

2 DIA. COILS W/OUT END BRGTS  
 3 SECTION PLATE WELDED TO SIDE FRAME COLUMN BY SAWBUCKER

7/8" DIA. COILS W/OUT END BRGTS  
 5/8" DIA. COILS W/OUT END BRGTS  
 5/8" DIA. COILS W/OUT END BRGTS

OUTER SPRINGS 5 COILS A.A.R. (1937) A.T. STD. 2 10113 - 51115  
 INNER SPRINGS 2 COILS A.A.R. (SPECIAL) STD. 2 4103 - 4204  
 SHELL SPRINGS 2 COILS 2 DIA. (N.E.) R. OD SPECIAL 2 7202 - 7302  
 TOTAL CAPACITY 23927  
 OUTER COIL SPRINGS 2 1/2" PITCH 5 1/2" DIA. W/OUT END BRGTS  
 INNER COIL SPRINGS 2 1/2" PITCH 5 1/2" DIA. W/OUT END BRGTS  
 SHELL SPRINGS 2 1/2" PITCH 5 1/2" DIA. W/OUT END BRGTS



TOP OF RAIL

5" WHEEL BASE

35 DIA. WHEELS  
 5" DIA. AXLES  
 5" DIA. AXLES  
 5" DIA. AXLES

SHOCK S-14 SHOCKERS  
 3" DIA. SHOCKERS

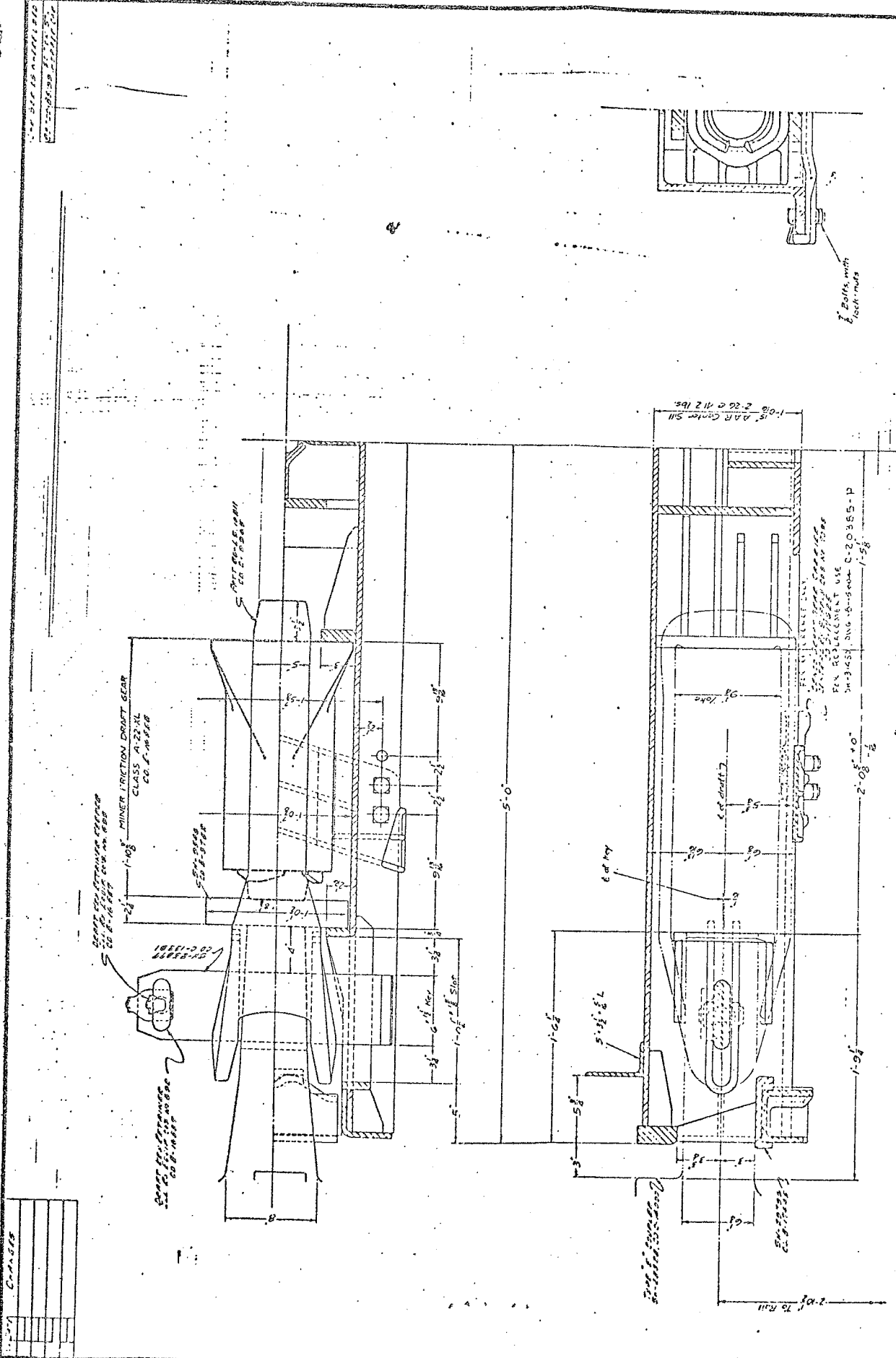
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 2. 10000 LBS. GROSS WEIGHT  
 3. 10000 LBS. GROSS WEIGHT  
 4. 10000 LBS. GROSS WEIGHT

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 11.1  
 11.1  
 11.1

LOUISVILLE & NASHVILLE R.R.  
 TRUCK NO 99  
 E 17814

*[Handwritten signature]*





LOUISVILLE & NASHVILLE RR.  
 DRAFT GEAR  
 E 17592

DATE  
 DRAWN BY  
 CHECKED BY  
 APPROVED BY

REVISIONS

LOUISVILLE & NASHVILLE RR.  
 DRAFT GEAR  
 E 17592

REVISIONS

DATE  
 DRAWN BY  
 CHECKED BY  
 APPROVED BY

LOUISVILLE & NASHVILLE RR.  
 DRAFT GEAR  
 E 17592



APPENDIX H

IMPORTANT CORRESPONDENCE

INDEX TO APPENDIX H

1. Letter and attachments, dated August 26, 1975, to L. J. Schlink from J. E. Everett, GATX Corporation, regarding spring capacities, specifications and drawings on tank cars.
2. Letter and attachments, dated October 8, 1975, to Ross Gill from C. E. Reedy, RPI-AAR, regarding procedure for pressurization of tank cars to 100 psi. Letter dated October 7, 1975 attached hereto.
3. Letter from L. J. Schlink to R. T. Gill, dated October 6, 1975, regarding followup details of meeting held at Washington University on October 1 and 2, 1975.
4. Letter from L. J. Schlink to Ross Gill, dated October 17, 1975, relative to outages and coupler information.
5. Letter from L. J. Schlink to R. T. Gill, dated October 31, 1975, relative to specifications and drawings for GATX 57688 and GATX 92571 .

R. G. 9/15/75  
SEP 15 1975  
REC'D

# RAILROAD TANK CAR SAFETY RESEARCH AND TEST PROJECT AN RPI-AAR COOPERATIVE PROGRAM

August 26, 1975

**PROJECT REVIEW COMMITTEE**

**CHAIRMAN**

R. E. Oppenheimer, Executive Vice  
President, Operations  
North American Car Corporation

**VICE CHAIRMAN**

W. J. Harris, Jr., Vice President  
Research and Test Department  
Association of American Railroads

A. L. Gery, President  
Pullman Transport Leasing Company  
Pullman Incorporated

J. S. Carlson, Vice President  
ACF Industries and  
General Manager  
Shippers Car Line Division

C. E. Coyt, Vice President  
General American Transportation  
Corporation

C. A. Love, Chief Mechanical Officer  
Equipment, Operating Department  
Louisville and Nashville Railroad

R. D. McEvers, Vice President  
Trans Union Corporation

R. E. Taylor, Assistant Vice President  
Mechanical Department  
Burlington Northern Lines, Inc.

File: G.S. 39.336  
PH 15

**PROJECT DIRECTOR**  
Earl Phillips

**DEPUTY PROJECT DIRECTOR**  
Lee Olson

Mr. L. J. Schlink  
Union Tank Car Company  
151st Street & Railroad Avenue  
East Chicago, Indiana 46312

SUBJECT: ASSIGNMENTS FROM PUEBLO MEETING OF AUGUST 5, 1975

Dear Sir:

1. GATX 92561 is scheduled to ship from our Argentine Shop week of 8-25-75.
2. I have looked into the springing situation for this car. The car as shipped had this spring group for a rail load of 263,000 lbs.

7 outer D3 @ 10223	=	71,561
4 inner D3 @ 4103	=	16,412
2 side coils @ 4499	=	8,998
Total Group Capacity	=	96,971#
	(Solid)	
Total Truck Capacity	=	193,942
Total Car Capacity	=	387,884

Working capacity is 263/388 - 67% of actual capacity. At rail load, the car is 62% full (of water) by volume. At 75% full (of water) the car weighs 292,000 lbs. This is 29,000 lbs. overweight, therefore, this springing capacity must be added to the car or 29,000/4 = 7250 lbs. per truck. I would, therefore, recommend adding two (2) D3 inner springs per group.

SP, L, N, E  
4/20/75

7 outer D3 @ 10223	=	71,561	added
6 inner D3 @ 4103	=	24,618	8206
2 side coils @ 4499	=	8,998	
Total Group Capacity	=	105,177	8206
	(Solid)		
Total Truck Capacity	=	210,354	16412
Total Car Capacity	=	420,708	32824

Working capacity is 292/421 = 69% of actual.

(con't)

Reply to J. E. Everett  
GATX Corporation  
P.O. Box 532  
Sharon, Pennsylvania 16146

August 26, 1975

TO: L. J. Schlink

File: G.S. 39.336  
PH 15

For the 92% capacity (by volume) the rail load would be 338,300 lbs. or an increase of 75,000 lbs. over the 62% full car. This is 18,750 lbs. per spring group. We can only add one more D3 inner spring and two (2) inner side coils which results in the following:

7 outer D3 @ 10223	=	71,561	added
7 inner D3 @ 4103	=	28,721	12309
2 outer side coils			
@ 4499	=	8,998	
2 inner side coils			
@ 1738	=	3,475	3475
Total Group Capacity	=	112,756	15784
(Solid)			
Total Truck Capacity		225,512	31568
Total Car Capacity		451,024	63135

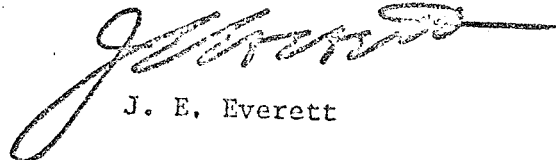
Working capacity is  $338/451 = 74\%$  of actual

This results in springing that is 12,000 lbs. under the required amount based on the criteria we are using. This 12,000 lbs. is only 3% of the total load on the car, therefore, not too bad. The only way we can add more capacity is to either purchase special springs or go to D-2 springs which, in my opinion will result in too much of a change in the springing rate. In view of this, it appears the arrangement shown for the 92% outage can be used.

3. As you requested, I am enclosing 15 sets of prints for the orange book which include the test car general arrangement and manway arrangement drawings.
4. Enclosed is our outage table 6895 which covers the test cars GATX 91833 and 92561.
5. Also enclosed are some specification sheets on these cars. The center of gravity above the center plate is marked on these and is 63.7 inches.

Would you please distribute any or all the above to the appropriate people.

Very truly yours,



J. E. Everett

JEE:rm

Enclosures

E. A. Phillips  
AS 148.2  
PH 15

ENGINEERING SPECIFICATIONS

CLASS OF CAR: TCC-112A310-W  
 TANK CAPACITY: 33,500 Gallon  
 TYPE OF UNDERFRAME: 08  
 TYPE OF TRUCKS: 100 Ton S-2-A Truck Mounted Cylinders  
 TYPE OF AIR BRAKE: "AP" Freight Equipment  
 INSULATION: None INT. LINING: None  
 LINE CAR  , SALE CAR  , PROTOTYPE   
 CUSTOMER OR LESSEE: Diloma Gas Products Company  
 COMMODITY: Anhydrous Ammonia  
 GENERAL ARRANGEMENT DRAWING: 1058-1048

ORDER NO. P.O.-8202  
 ENGINEERED BY: AVV/JSP  
 DATE: 2-8-68

91883

CG ABOVE CENTER PLATE 63.7"

ENGINEERING SPECIFICATIONS/PART 2

(SHOP INSTRUCTIONS)  
SHEET 2

ORDER NO. BO 8202  
ENGINEERED BY: AVV/JSF  
DATE: 2-8-68

NOTATION: THE INSTRUCTIONS LISTED ON THIS SHEET SHALL PERTAIN TO AND BE CONSIDERED PART OF THE ORDER NUMBER ABOVE. SUBSEQUENT ADDITIONAL SHEETS MAY BE ISSUED TO ADD TO, OR SUPERCEDE PREVIOUS INSTRUCTIONS.

- 1) TRUCKS: Arrgt. Dwg.: 1000-120-A Capacity: 100 ton  
 Bearings: "AP" roller GATX Stock No. 4-9999-2  
 Brake Beams: Truck Mounted Assembly GATX Stock No. 7-1109  
 Truck Bolster: Barber Stabilized S-2-A GATX Stock No. 26-9999-12  
 Truck Side Frame: Barber Stabilized S-2-A GATX Stock No. 20-9999-17  
 Side Bearings: Single - Stucki #656  
 Center Pin: One Piece  
 Wheels: 36" Dia. 1-W, R.S. or C.S. rim treated
  
- 2) UNDERFRAME: Arrgt. Dwg.: 1210-43 Type: 98  
 Truck Centers: 52'-4-1/2" Length Over Strikers: 63'-3-1/2"  
 Draft Sill Assy. Dwg.: 306-335  
 Draft Gear: Arrgt. Dwg.: 1025-37-C  
 Coupler: B-E60A-HT
  
- 3) TANK Arrgt. Dwg.: 1184-10-1  
 ID 119" I.B.H. 59'-11-1/2"  
 No. of Rings in Shell: Six (6) Shell Thickness: 5/8"  
 Heads: 2:1 ellip. Thickness: 11/16"  
 Shell & Head Mat'l: AAR M-128 Gr. "B" F.Q.S.  
 Location of Tank Attach. Dwg.: 1184-10-1

(SHOP INSTRUCTIONS)

SHEET 3ORDER NO. BO 8202ENGINEERED BY: AVV/JEPDATE: 2-8-63

NOTE: THE INSTRUCTIONS LISTED ON THIS SHEET SHALL PERTAIN TO AND BE CONSIDERED PART OF THE ORDER NUMBER SHOWN ABOVE. SUBSEQUENT ADDITIONAL SHEETS MAY BE ISSUED TO ADD TO, OR SUPERCEDE PREVIOUS INSTRUCTIONS.

- 4) FITTINGS: Arrgt. Dwg.: 1049-538  
 Manway Dwg.: 1078-146 I.D.: 18"  
 Safety Valve Dwg.: 1049-538 Release Pressure: 280.5#  
 Air Connection Dwg.: 1049-538  
 Bottom Outlet Dwg.: N/A  
 Stuffing Box Dwg.: N/A  
 Washout Dwg.: N/A Valve Rod: N/A  
 Top Unloading Dwg.: 1049-538 Consisting of: (2) 3" angle valves  
 W/3 x 2 reducer and plugs  
 Education pipe arrgt. dwg. 1132-282  
 Manway bonnet arrangement dwg. 1194-25-B
- 5) SAFETY APPLIANCES: Ladder Arrgt. Dwg.: 1023-155  
 End Arrgt. Dwg.: 1181-80  
 Platform Arrgt. Dwg.: 1051-930 Type: Walkway Grating Type: BK-P16  
 Safety Railing Arrgt. Dwg.: N/A  
 Mudguard arrangement dwg.: 1107-143
- 6) AIRBRAKE: Arrgt. Dwg.: 1052-243  
 Description: Reconditioned brake equipment  
 Airbrake Equipment Support Location Dwg.: 1181-78-1  
 Train Line and Cylinder Line Arrangement Dwg.: 1052-240-A  
 Brake Shoes: Composition
- 7) HANDBRAKE: Arrgt. Dwg.: 1055-90-F  
 Description: Vertical Type W//66 bell crank.

GATX ENGINEERING SPECIFICATIONS/PART I

CLASS OF CAR: ICC-112A340W  
TANK CAPACITY: 33,500 Gallons  
TYPE OF UNDERFRAME: 98 U/F  
TYPE OF TRUCKS: 100 Ton S-2-A Truck Mounted Cylinders  
TYPE OF AIR BRAKE: "AB" Freight Equipment  
REGULATION: None INT. LINING None  
LEASE CAR  , SALE CAR  , PROTOTYPE   
CUSTOMER OR LESSEE: GATX - Shell Oil Co.  
COMMODITY: Liquified Petroleum Gas  
GENERAL ARRANGEMENT DRAWING: 1058-1068-A

ORDER NO. BO 8418  
ENGINEERED BY: AVV/RF  
DATE: 9-12-68

92561

CC ABOVE CENTER R 63.7"



ENGINEERING SPECIFICATIONS/PART

12/0

(SHOP INSTRUCTIONS)  
SHEET #2

ORDER NO. BO 8418  
ENGINEERED BY: AVV/RF  
DATE: 9-12-68

NOTICE: THE INSTRUCTIONS LISTED ON THIS SHEET SHALL PERTAIN TO AND BE CONSIDERED PART OF THE ORDER NUMBER SHOWN ABOVE. SUBSEQUENT ADDITIONAL SHEETS MAY BE ISSUED TO ADD TO, OR SUPERCEDE PREVIOUS INSTRUCTIONS.

- 1) TRUCKS: Arrgt. Dwg.: 1000-120-B  
 Bearings: "AP" Roller  
 Brake Beams: Truck Mounted Assembly  
 Truck Bolster: Barber Stabilized S-2-A  
 Truck Side Frame: Barber Stabilized S-2-A  
 Side Bearings: Single, Stucki #656  
 Center Pin: One Piece  
 Wheels: 36" Dia. 1-W, R.S. or C.S. Rim Treated  
 Capacity: 100 Ton  
 GATX Stock No. 4-9999-2  
 GATX Stock No. 7-1109  
 GATX Stock No. 26-9999-138  
 GATX Stock No. 20-9999-178
  
- 2) UNDERFRAME: Arrgt. Dwg.: 1210-65-A  
 Truck Centers: 52" - 4-1/2"  
 Draft Sill Assy. Dwg.: 306-361  
 Draft Gear: Arrg't Dwg. 1025-37-C  
 Coupler: B-E60A-HT  
 Type: #98  
 Length Over Strikers: 63'-3-1/2"
  
- 3) TANK  
 ID 119"  
 No. of Rings in Shell: Six (6)  
 Heads: 2:1 Ellips.  
 Shell & Head Mat'l: AAR M-128, Gr. "B" - F.Q.S.  
 Location of Tank Attach. Dwg.: 1184-10-1-A  
 Arrgt. Dwg.: 1184-10-1-A  
 I.B.H. 59' - 11'-1/2"  
 Shell Thickness: 5/8"  
 Thickness: 11/16"

## ENGINEERING SPECIFICATIONS/PART 2

12/68

(SHOP INSTRUCTIONS)  
SHEET #3ORDER NO. BO 8418  
ENGINEERED BY: AVV/RF  
DATE: 9-12-68

NOTE: THE INSTRUCTIONS LISTED ON THIS SHEET SHALL PERTAIN TO AND BE CONSIDERED PART OF THE ORDER NUMBER SHOWN ABOVE. SUBSEQUENT ADDITIONAL SHEETS MAY BE ISSUED TO ADD TO, OR SUPERCEDE PREVIOUS INSTRUCTIONS.

4) FITTINGS:

Manway Dwg.: 1078-146-A  
Safety Valve or Vent Dwg.: 1049-538-B  
Air Connection Dwg.: 1049-538-B  
Bottom Outlet Dwg.: N/A  
Stuffing Box Dwg.: N/A  
Washout Dwg.: N/A  
Top Unloading Dwg.: 1049-538-B  
Education Pipe Arrg't Dwg. 1132-240-A  
Manway Bonnet Arrg't Dwg. 1194-25-D

Arrgt. Dwg.: 1049-538-B

I.D.: 18"

Release Pressure: 280.5#

Valve Rod: N/A

Consisting of: (3) - 3" Angle Valves  
with 3" x 2" Reducer & Plugs.  
(2) - 3" Discharge Pipes.

5) SAFETY APPLIANCES:

End Arrgt. Dwg.: 1181-80  
Platform Arrgt. Dwg.: 1051-930-A  
Safety Railing Arrgt. Dwg.: N/A  
Mudguard Arrg't Dwg.: 1107-143

Ladder Arrgt. Dwg.: 1023-155

Type:

Grating Type: BK-P-16

6) AIRBRAKE:

Description: Reconditioned Brake Equipment

Arrgt. Dwg.: 1052-243

Airbrake Equipment Support Location Dwg.: 1181-78-1

Train Line and Cylinder Line Arrangement Dwg.: 1052-240-A

Brake Shoes: Composition

7) HANDBRAKE:

Description: Vertical Type with #66 Bell Crank

Arrgt. Dwg.: 1055-90-H

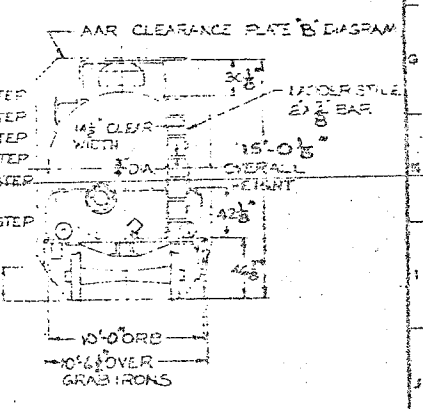
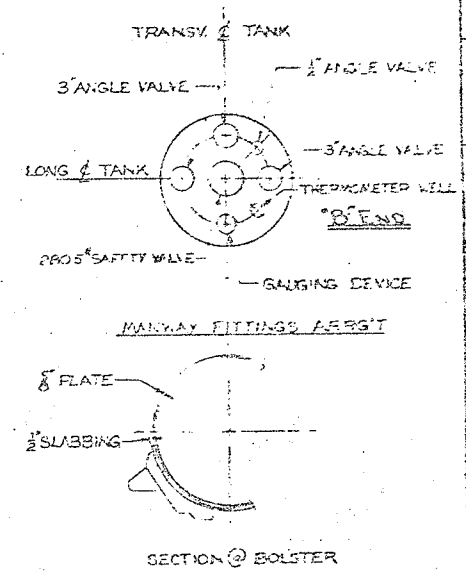
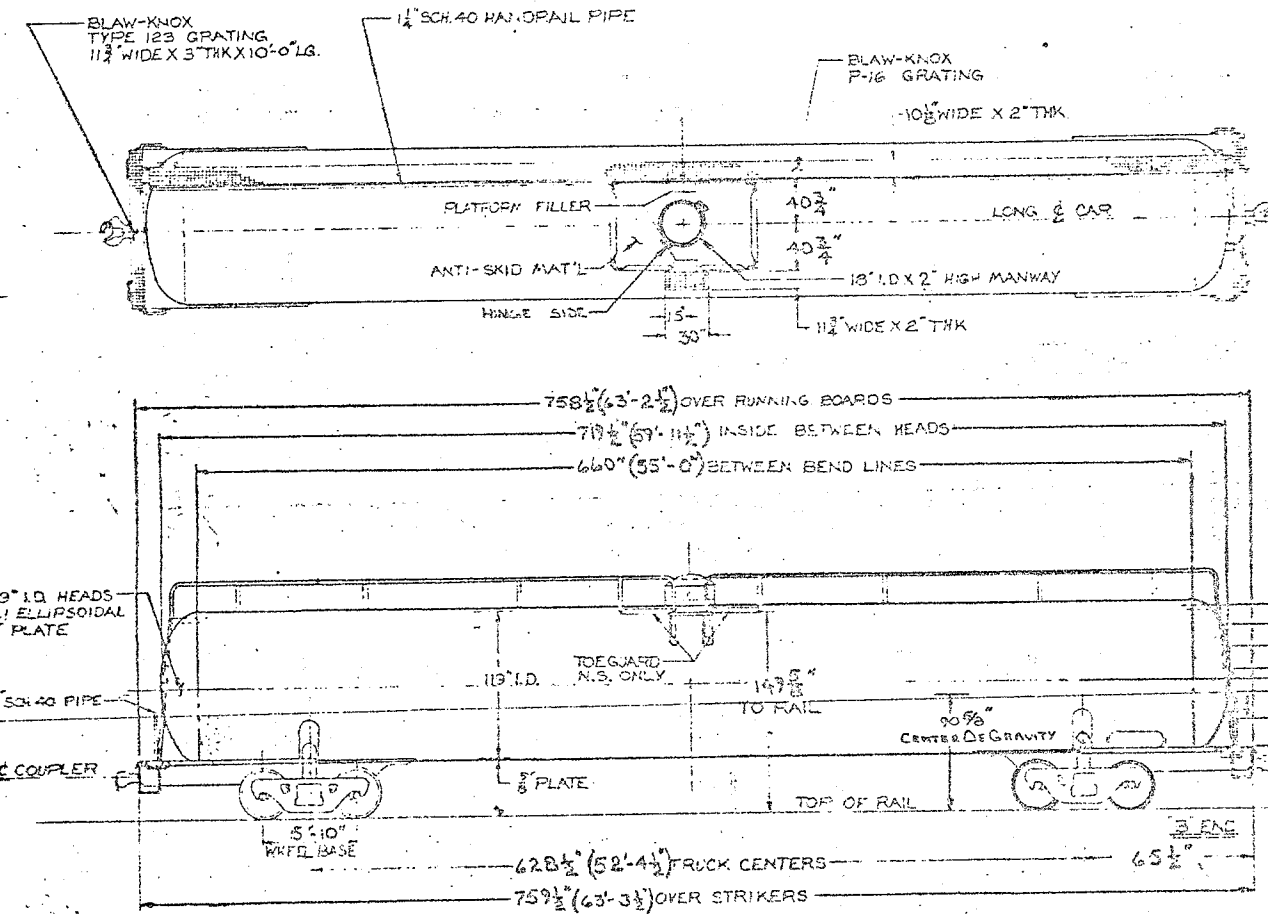
GALLONS PER INCH IN MANWAY 1.10

INS	GALS	INS	GALS	INS	GALS	INS	GALS	INS	GALS	INS	GALS
0	3	10	1320	20	3666	30	6585	40	9873	50	13380
1/4	8		1369		3733		6663		9959		13478
1/2	18		1419		3800		6742		10045		13568
3/4	30		1470		3868		6820		10131		13658
1	45	11	1521	21	3936	31	6900	41	10217	51	13740
1/4	61		1572		4005		6979		10303		13830
1/2	80		1624		4073		7058		10389		13920
3/4	100		1677		4142		7138		10476		14010
2	121	12	1730	22	4212	32	7218	42	10562	52	14100
1/4	144		1783		4281		7298		10649		14190
1/2	169		1837		4352		7378		10736		14280
3/4	194		1892		4422		7459		10823		14370
3	221	13	1947	23	4492	33	7540	43	10910	53	14460
1/4	248		2002		4563		7621		10997		14550
1/2	277		2058		4635		7702		11084		14650
3/4	307		2115		4706		7783		11172		14740
4	338	14	2172	24	4778	34	7865	44	11259	54	14830
1/4	370		2229		4850		7946		11347		14912
1/2	403		2287		4923		8028		11435	55	15193
3/4	436		2346		4995		8110		11523		15374
5	471	15	2404	25	5069	35	8193	45	11610	56	15556
1/4	506		2464		5142		8275		11699		15737
1/2	543		2523		5215		8358		11787	57	15919
3/4	580		2583		5289		8440		11875		16100
6	618	16	2644	26	5363	36	8523	46	11963	58	16282
1/4	656		2705		5438		8607		12052		16464
1/2	696		2766		5512		8690		12140	59	16646
3/4	736		2828		5587		8773		12229		16828
7	777	17	2890	27	5663	37	8857	47	12318	60	17010
1/4	819		2953		5738		8941		12406		17191
1/2	861		3016		5814		9025		12495	61	17373
3/4	904		3079		5890		9109		12584		17555
8	948	18	3143	28	5966	38	9193	48	12673	62	17737
1/4	992		3207		6043		9278		12762		17919
1/2	1037		3271		6119		9362		12852	63	18100
3/4	1083		3336		6196		9447		12941		18281
9	1129	19	3401	29	6273	39	9532	49	13030	64	18463
1/4	1176		3467		6351		9617		13120	110**	33653
1/2	1223		3533		6429		9703		13209	EMPTY	
3/4	1272		3599		6506		9788		13299		

ZERO INCHES REPRESENTS MANWAY NOZZLE CAPACITY  
 \*\* REPRESENTS SHELL CAP. PLUS MANWAY CAPACITY

GATX 92930  
 91833  
 92561

A  
B  
C  
D  
E  
F  
G  
H  
I  
J  
K  
L  
M



**SPECIFICATIONS:**

NOMINAL CAPACITY.....	33,500 GALLONS
EST. LT. WT.....	83,300 LBS.
RAIL LOAD.....	24,500 LBS.
TRUCKS.....	100 TON BARBER S2A STABILIZED WITH AAR STANDARD ROLLER BEARINGS WITH ALUMITE FITTINGS
WHEELS.....	36" DIA. ONE (1) WEAR ROLLED STEEL OR 60S (1) WEAR CAST STEEL RIM TREATED
AIR BRAKES.....	8" INCH I.A. TRUCK MOUNTED CYLINDERS WITH COMPOSITION SHOES
HANDBRAKE.....	VERTICAL WHEEL TYPE
DRAFT GEAR.....	AAR HIGH CAPACITY
COUPLER.....	AAR B-EGOA-MT
TYRE.....	AAR B-T40 (24-5/8" GEAR POCKET)

HANDRAILS.....	1-1/2" SCH 40 PIPE
TANK SHELL.....	11/8" I.D. 5/8" PLATE TRA. AAR M-128 GRADE B FLOOR QUALITY STEEL
TANK HEAD.....	11/16" NOMINAL THK. 2:1 ELLIPSOIDAL AAR M-128 GRADE 7/8" FLANGE QUALITY STEEL
GRATING.....	MANWAY-BLAW FNOX P-16 END PUNCHING BOARD: BLAW KNOX #123
END LADDERS.....	TWO (2)
MINIMUM HORIZONTAL CURVE NEGOTIABILITY	
1. TWO LIKE CARS COUPLED TOGETHER.....	24W
2. TANK CAR ON CURVE - STANDARD CAR ON TANGENT.....	24S

DESIGNED FOR WFLD  
JOINT EFFICIENCY  
OF 1.0

**RELOCATED HINGE ON MANWAY**  
BONNET 503320 RF 1-30-65

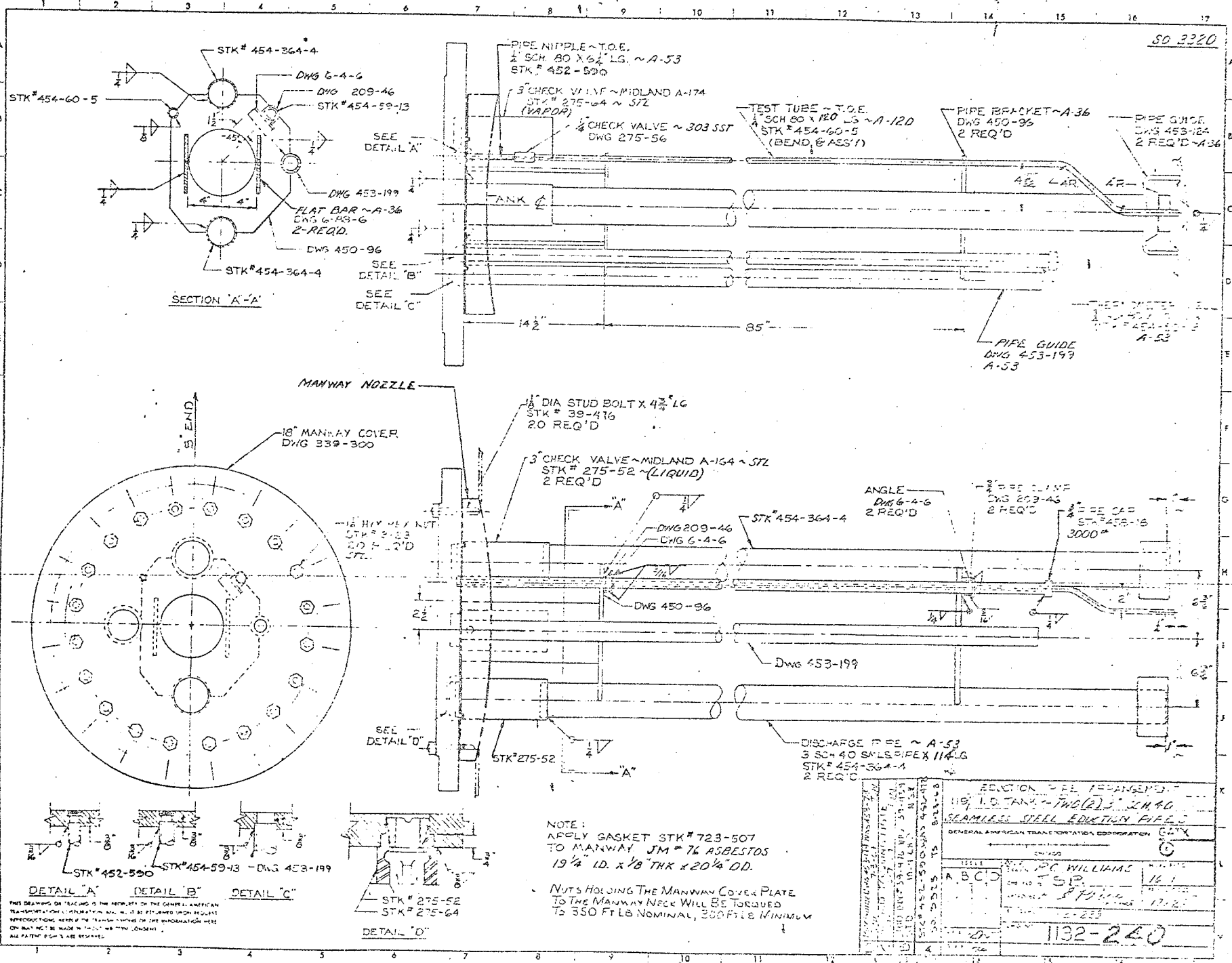
GENERAL ASSIGNMENT  
33,500 GALLONS CAR - 98 LIF  
100 H.C. 40 - W. 10' 10" TANK 100 - T.C.

SPECIAL AMERICAN TRANSPORTATION CORPORATION  
GATX

1339E  
DRAWN: J.S.O.  
CHECK: T.S.  
APPROVED: *John R. ...*  
REV. SERVICE: 375 1051  
LOG NO: 1058-1048

THE BUILDING OF TRACKS IS THE PROPERTY OF THE GENERAL AMERICAN TRANSPORTATION CORPORATION AND MUST BE RETURNED WITHIN 1000 FT. OF THE TRACKS. REPAIRS SHOULD BE MADE WITHIN 24 HOURS OF THE INFORMATION HEREON. THIS MAY NOT BE MADE WITHOUT WRITTEN CONSENT. ALL DIMENSIONS ARE IN FEET.

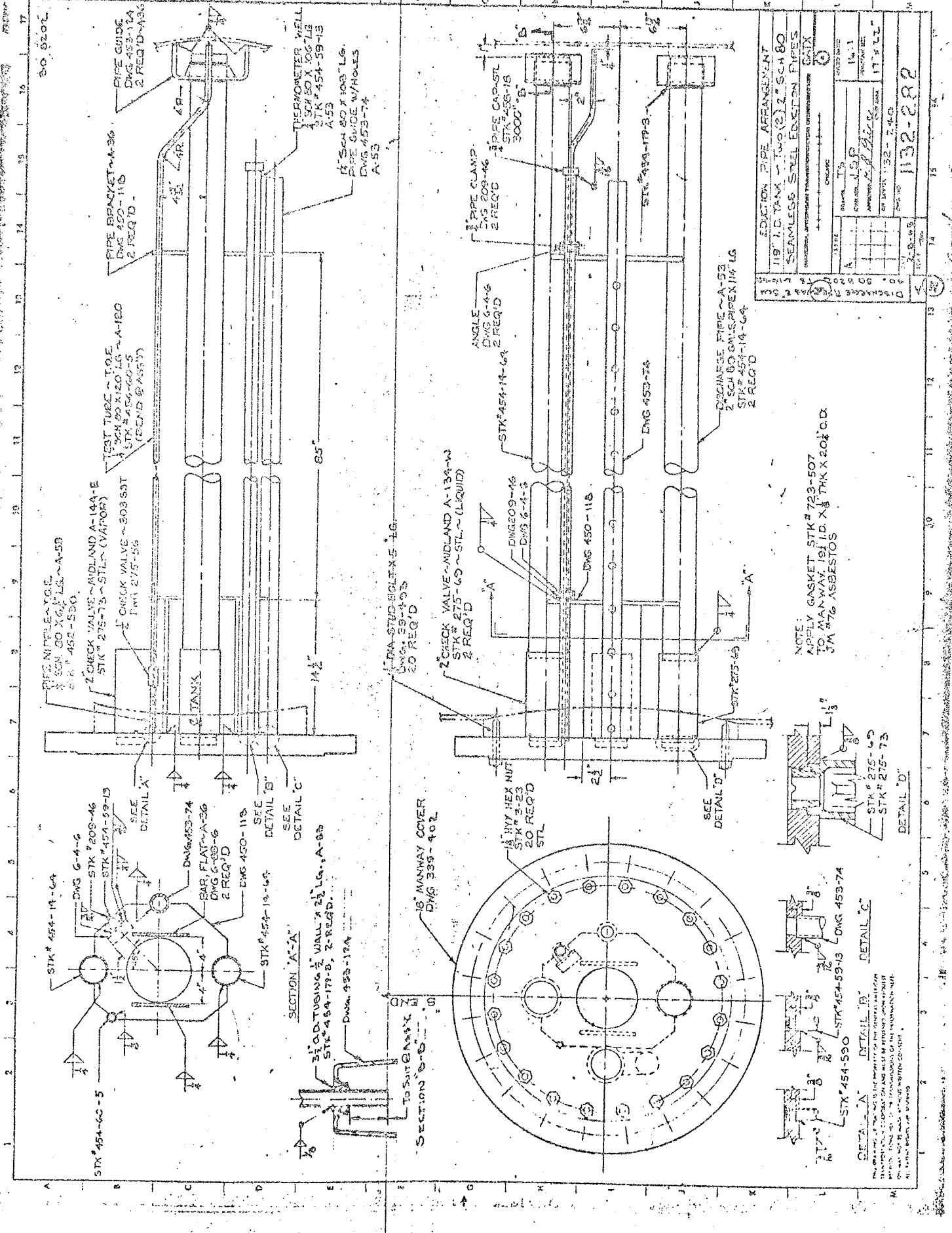
SO 3320



SECTION 'A-A' ARRANGEMENT	
18" I.D. TANK - TWO (2) 1 1/2" SCH 40	
SEAMLESS STEEL EJECTION PIPE	
GENERAL AMERICAN TRANSPORTATION CORPORATION	
CH 150	
SCALE	1/4" = 1"
DESIGNED BY	J. C. WILLIAMS
CHECKED BY	S.P.
DATE	11/21
PROJECT	1132-240
NO.	1

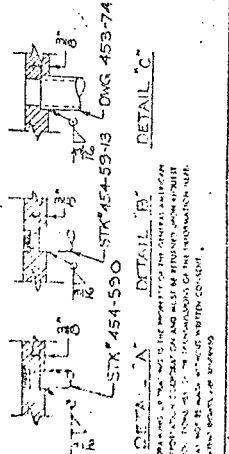
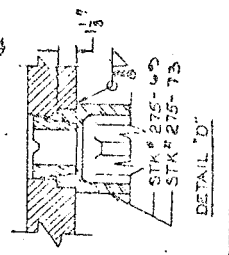
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EDUCATION PIPE ARRANGEMENT			
119" I.C. TANK - TWO (2) 2" SCH 80			
SEAMLESS STEEL EDUCATION PIPES			
CONSTRUCTION INFORMATION: CONTRACTOR NAME	DATE	SCALE	NO.
CONTRACTOR			
DATE			
SCALE			
NO.			
1132-282			

NOTE: APPLY GASKET STK # 723-507 TO MANWAY 19" I.D. X 1/2" THK X 20" O.D. JM #76 ASBESTOS



10-07-75

# RAILROAD TANK CAR SAFETY RESEARCH AND TEST PROJECT AN RPI-AAR COOPERATIVE PROGRAM

PROJECT REVIEW COMMITTEE

CHAIRMAN

J. R. Krutzenga, President  
Union Tank Car Company

VICE CHAIRMAN

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Research and Test Department  
Association of American Railroads

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C. A. Love, Assistant Vice President  
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Louisville and Nashville Railroad

R. B. Oppenheimer, Executive Vice  
President, Operations  
North American Car Corporation

R. E. Taylor, Assistant Vice President  
Mechanical Department  
Burlington Northern, Inc.

PROJECT DIRECTOR  
Earl Phillips

DEPUTY PROJECT DIRECTOR  
Lee Olson

October 7, 1975

Mr. Ross Gill, Project Manager  
Rail Operations Control  
U. S. Department Transportation Test Center  
Pueblo, CO 81001

Dear Mr. Gill:

Subject: Phase 15 - Orange Book

Enclosed are two copies of addition (17) to the Orange Book.

Larry Schlink asked me to send you advance copies as you are ready to use this section in the present Switchyard Impact Test Program.

Sincerely,

*C. E. Reedy*

C. E. Reedy

CER/jb

cc Mr. Larry Schlink - attachments

Reply to: Project Director — Tank Car Research  
Association of American Railroads, Technical Center  
3140 South Federal Street, Chicago, Illinois 60616  
312-225-9600 ext 863



(17)

RPI-AAR TANK CAR SAFETY PROJECT  
PHASE 15, SWITCHYARD IMPACT TEST PROGRAM

Procedure for Pressurizing Tank Cars  
of DOT 112A Specification

I. Safety Precautions

1. Place caution sign on track a safe distance in front of and to the rear of tank car to indicate workman on car.
2. Set handbrake on car and/or
3. Place wood wedge blocks on track in front and rear of one set of wheels.

II. Preparation of Tank Pressure Test

1. Refer to Sketch 17-1, and open Manway Housing Cover (7).
2. Make up a hose line (1), air line shut-off valve (2), pressure indicating gage (3), and suitable pipeline (4) to connect to the tank car vapor valve (5).
3. Confirm that tank was filled with water to desired level before connecting pressure pipe (4) to car vapor valve (5).

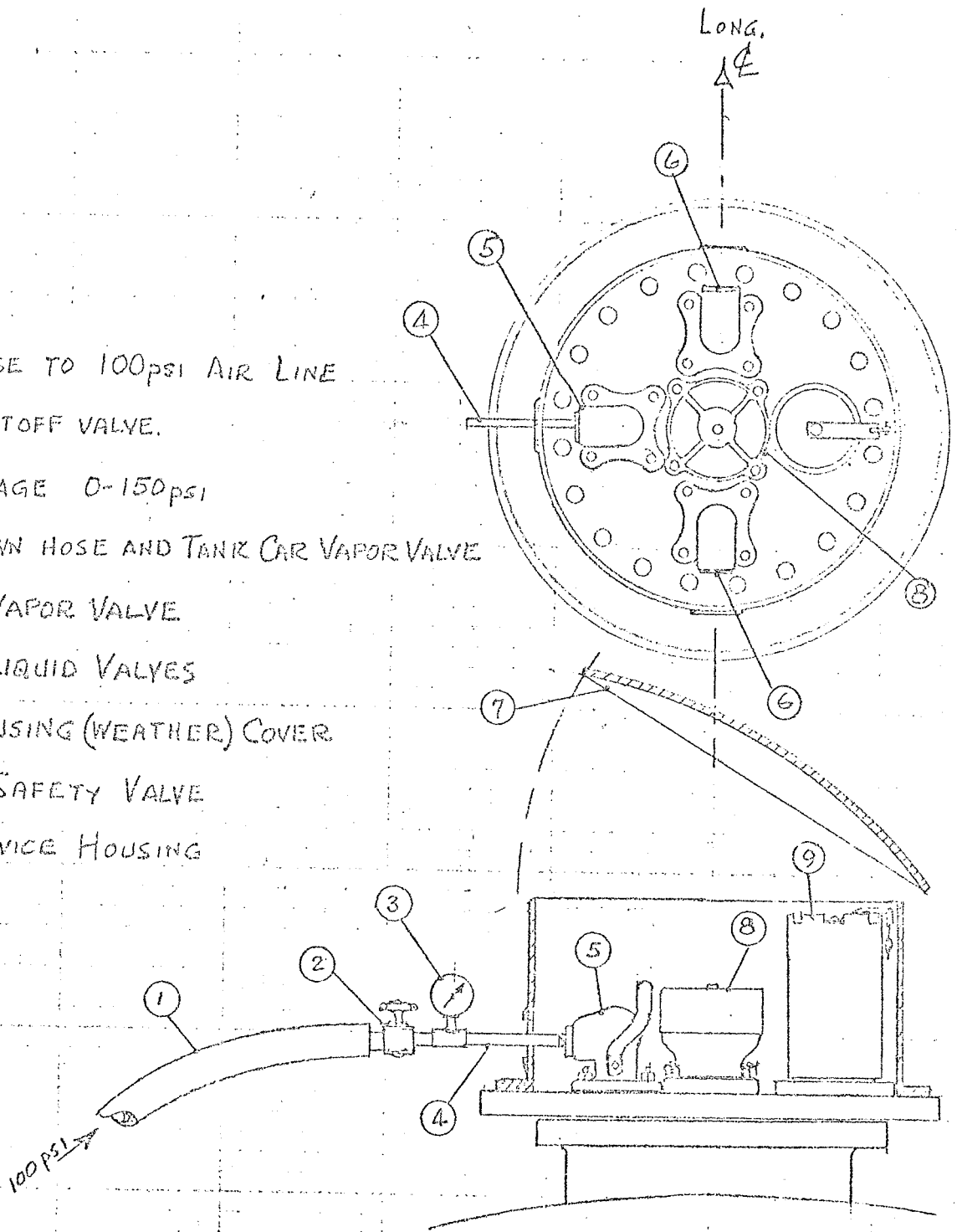
III. Pressurizing Tank Car

1. Connect pipe line (4) to tank car vapor valve (5). Open vapor valve (5).
2. Open air line valve (2) to pressurize tank car.
3. Close air line valve (2) to determine correct pressure (3) in tank.
4. When tank pressure gage (3) reads 100 psi, close tank vapor valve (5).
5. Disconnect air line pipe (4) from vapor valve (5).
6. Remove caution signs from track and release hand brake and/or remove wheel wedge blocks.

IV. De-pressurizing Tank Car

1. After impact test is completed, open tank car vapor valve (5) to release 100 psi air from tank.

- ① - AIR LINE HOSE TO 100psi AIR LINE
- ② - AIR LINE SHUTOFF VALVE.
- ③ - PRESSURE GAGE 0-150psi
- ④ - PIPE LINE BTWN HOSE AND TANK CAR VAPOR VALVE
- ⑤ - TANK CAR VAPOR VALVE
- ⑥ - TANK CAR LIQUID VALVES
- ⑦ - MANWAY HOUSING (WEATHER) COVER
- ⑧ - TANK CAR SAFETY VALVE
- ⑨ - GAUGING DEVICE HOUSING



AN RPI-AAR COOPERATIVE PROGRAM

MADE BY CER	FOR PROCEDURE FOR PRESSURIZING TANK CARS	LOT NO.
CHECKED BY	SUBJECT PHASE 15 - SWITCHYARD IMPACT TESTS	EST. NO.
APP'D. BY		DATE 10-6-75
REV.	REFERENCES	SKETCH 17-1

(17)

RPI-AAR TANK CAR SAFETY PROJECT  
PHASE 15, SWITCHYARD IMPACT TEST PROGRAM

Procedure for Pressurizing Tank Cars  
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I. Safety Precautions

1. Place caution sign on track a safe distance in front of and to the rear of tank car to indicate workman on car.
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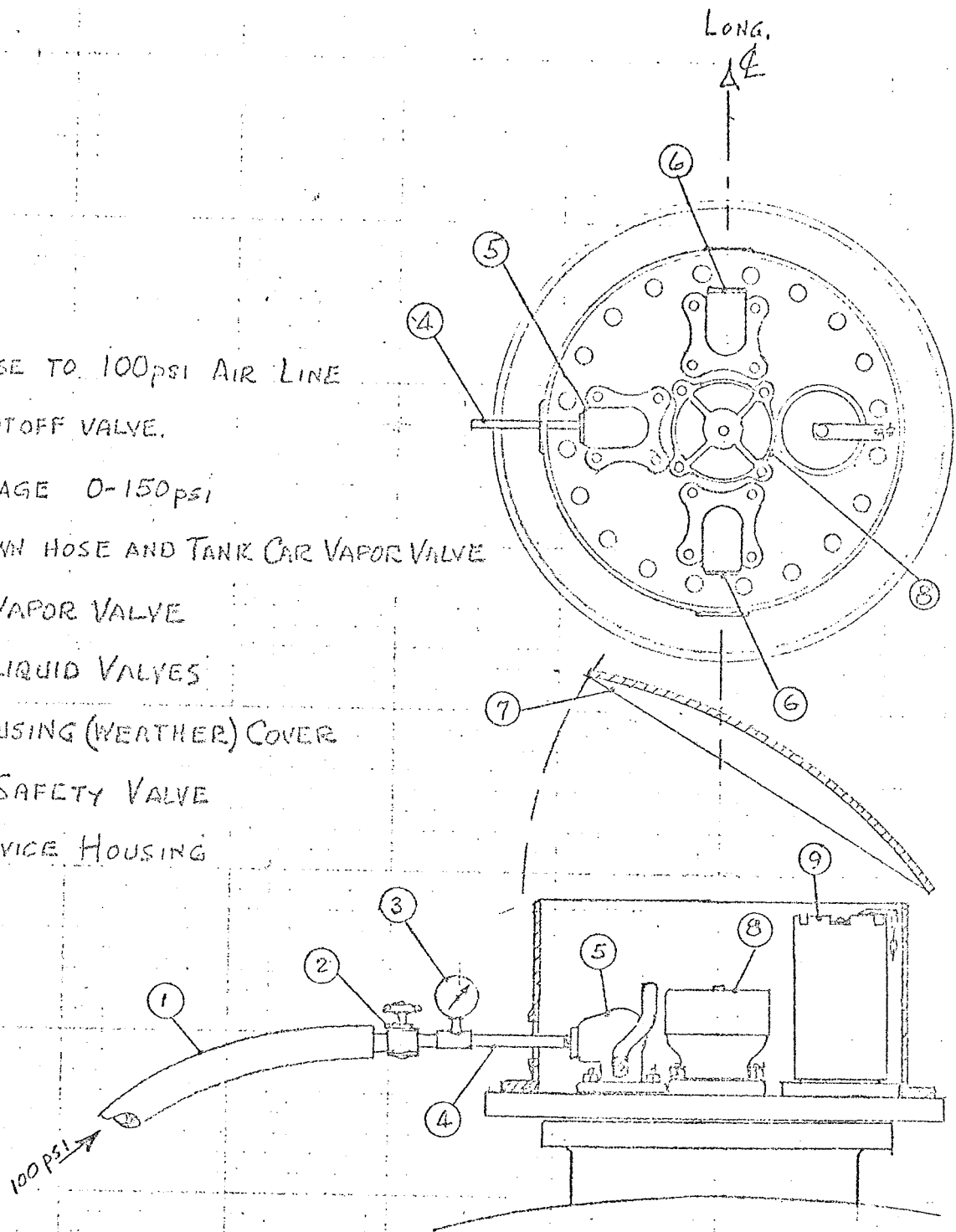
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3. Close air line valve (2) to determine correct pressure (3) in tank.
4. When tank pressure gage (3) reads 100 psi, close tank vapor valve (5).
5. Disconnect air line pipe (4) from vapor valve (5).
6. Remove caution signs from track and release hand brake and/or remove wheel wedge blocks.

IV. De-pressurizing Tank Car

1. After impact test is completed, open tank car vapor valve (5) to release 100 psi air from tank.

- ① - AIR LINE HOSE TO 100psi AIR LINE
- ② - AIR LINE SHUTOFF VALVE.
- ③ - PRESSURE GAGE 0-150psi
- ④ - PIPE LINE BTWN HOSE AND TANK CAR VAPOR VALVE
- ⑤ - TANK CAR VAPOR VALVE
- ⑥ - TANK CAR LIQUID VALVES
- ⑦ - MANWAY HOUSING (WEATHER) COVER
- ⑧ - TANK CAR SAFETY VALVE
- ⑨ - GAUGING DEVICE HOUSING



AN RPI-AAR COOPERATIVE PROGRAM

MADE BY CER	FOR PROCEDURE FOR PRESSURIZING TANK CARS	LOT NO.
CHECKED BY	SUBJECT PHASE 15 - SWITCHYARD IMPACT TESTS	EST. NO.
APP'D. BY		DATE 10-6-75
REV.	REFERENCES	SKETCH 17-1

RAILROAD TANK CAR SAFETY RESEARCH  
AND TEST PROJECT AN RPI-AAR COOPERATIVE PROGRAM

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The American Car Corporation

PROJECT DIRECTOR  
Earl Phillips

DEPUTY PROJECT DIRECTOR  
Lee Olson

October 6, 1975

Mr. R. T. Gill  
Rail Operations Controller  
U. S. Department of Transportation  
Transportation Test Center  
Pueblo, Colorado 81004

SUBJECT: Switchyard Impact Tests - RPI-AAR Phase 15

Dear Mr. Gill:

1. As requested at the October 1 - October 2, 1975 meeting, the following wording is suggested to describe the responsibilities of the RPI-AAR Phase leader (or his alternates):

L. J. Schlink will be the RPI-AAR Phase leader for the Phase 15 switchyard impacts. It will be his responsibility to insure that:

- 1.4.2
- a. The RPI-AAR commitments to this program are fulfilled in an orderly manner,
  - b. Test data suitable to the RPI-AAR is obtained,
  - c. Any conflict regarding the conduction of the test and changes in the test program are resolved to the mutual satisfaction of the RPI-AAR and the DOT.

J. E. Everett, E. L. Kunz, and/or L. L. Olson will serve as alternates.

(cont'd...)

Reply to: Project Director — Tank Car Research  
Association of American Railroads, Technical Center  
3140 South Federal Street, Chicago, Illinois 60616  
312-225-9600 ext 863

Mr. R. T. Gill  
October 6, 1975  
Page 2...

2. For test consistency, Test Series 10 of the test matrix should precede Test Series 9. That is, the column titled "Head Shields" should read 'no' for Test Series 9 and 'yes' for Test Series 10.
3. Enclosed for your information are three tabulations that were developed using the impact test schedule, Figure B-1, and by assuming impact velocities for each test series. Accordingly, cars will be scheduled for arrival at TTC as per Table 3. Note that the number of 112A cars has increased from 26 to 28 due to expansion of test matrix to include Test 10.
4. As also requested at the Oct. 1 - Oct 2 meeting, I have discussed the question of grid lines on the RPI-AAR movies with Earl Phillips. We have no objection to grids on our movies.
5. In the "Test Specifications" under Par.2.2e, the AAR reference for restoring the butt end of the coupler is "Manual of Standards and Recommended Practices" Specification M-204A-68 Figure 8.

Very truly yours,



L. J. Schlink

mr.

cc: D. M. Dancer  
J. E. Everett  
E. L. Kunz  
L. L. Olson  
E. A. Phillips

SERIES	START	VELOCITY (MPH)		REMARKS
		INCREMENT	FINAL	
Preliminary	4	2	8	No damage
①	4	2	Destruction	Repeat non-destructive impacts
②	Uncoupling	2	Destruction	
③	Final from ②	2	Destruction	
④	Final from ②	--	---	One test only
⑤	Final from ②	--	---	One test only
⑥	Final from ②	--	---	One test only
⑦	4 mph less than final from ②	2	Destruction	
⑧	Final from ②	2	Destruction	
⑨	4	2	Destruction	
⑩	Final from ⑨	2	Destruction	
⑪	4	2	8	No damage

- Note: 1) It is assumed that Test ⑪ will be scheduled prior to final test series so that Test ⑪ car(s) can be used in destructive tests.
- 2) All tests that do not start at 4 mph are to be preceded by 4 mph impact for instrumentation check.

TABLE 2

CAR REQUIREMENTS

TEST	ASSUMED VELOCITIES	TANK CARS	HOPPER CARS
1	4 - 10	1	2
	12	1	1
	14	1	1
	16	1	1
2	8 - 10	1	2
	12	1	1
	14	1	1
	16	1	1
3	16	1	1
	18	1	1
4	16	1	1
5	16	1	1
6	16	1	1
7	14	1	1
	16	1	1
	18	1	1
8	16	1	1
	18	1	1
	20	1	1
	22	1	1
9	4 - 10	1	2
	12	1	1
	14	1	1
	16	1	1
	18	1	1
10	18	1	1
	20	1	1
	22	1	1
TOTAL		28	31

Note: 1) Tank cars assumed unusable after 10 mph impact  
2) Hopper cars assumed unusable after 8 mph impact  
Uncoupling velocity assumed to be 8 mph



TABLE 3

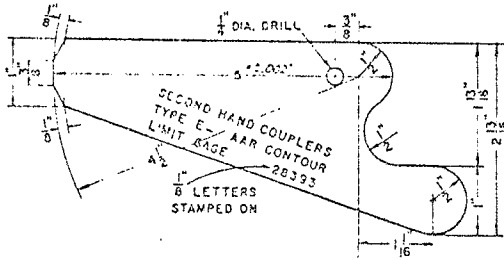
## CAR REQUIREMENTS

TEST SERIES	TANK CARS		NUMBER REQUIRED		DATE REQUIRED AT TTC
	COUPLERS	HEAD SHIELDS	HOPPER	TANK	
1	E (Std)	No	5	4	10 Nov 75
2	E (Std)	No	5	4	8 Dec 75
3	E (Std)	Yes	2	2	12 Jan 76
4	F (Std)	No	1	1	9 Feb 76
5	E (SheIf)	No	1	1	8 Mar 76
6	F (SheIf)	No	1	1	5 Apr 76
7	E (Std)	Yes	3	3	3 May 76
8	E (SheIf)	Yes	4	4	1 Jun 76
9	E (Std)	No	6	5	28 Jun 76
10	E (Std)	Yes	3	3	26 Jul 76

31 28

2 additional impacting cars (not 112A or 114A) are required at TTC on June 28, 1976

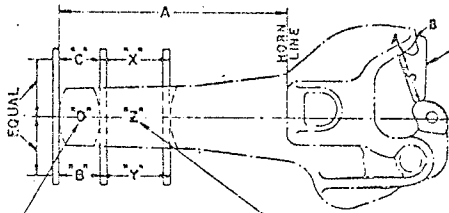
PLATE I.



**USE OF GAGE:**  
THIS COUPLER CONTOUR IS CONDEMNED WHEN THE GAGE CAN BE PASSED VERTICALLY THROUGH THE CONTOUR IN POSITION SHOWN AND WITH POINTS 'A' AND 'B' CONTACTING GUARD ARM.

1/8 STEEL PLATE - HARDEN & FINISH CONTACT POINTS.  
CONTOUR LIMIT GAGE NO. 28393

FIG. 1



THIS DIMENSION, 'D', TO BE 3 7/8 MIN. 4 3/2 MAX. AND IS DETERMINED BY TAKING 1/2 THE SUM OF MEASUREMENTS 'B' AND 'C'.

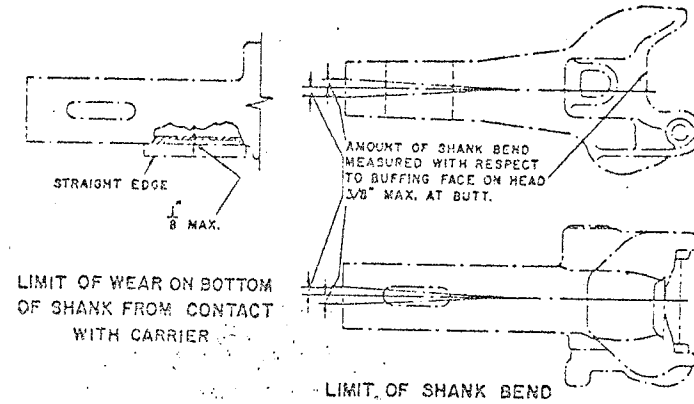
THIS DIMENSION TO BE DETERMINED BY TAKING 1/2 THE SUM OF MEASUREMENTS 'X' AND 'Y' AND SHALL BE GREATER THAN 'Z' MIN. IN TABLE.

CATALOG NO.	DIM. 'A'		DIM. 'Z'
	MIN.	MAX.	
E60	21"	21 3/8"	6 1/2"
E63, B-E63-HT B-E63A-HT	21"	21 3/4"	5"
B-E60A-HT	21"	21 5/8"	6 3/4"
B-E67-HT	24 1/2"	25 1/8"	8 1/2"

SHANK LENGTH AND KEYSLOT LIMIT  
RIGID SHANK COUPLERS.

FIG. 2

PLATE III.

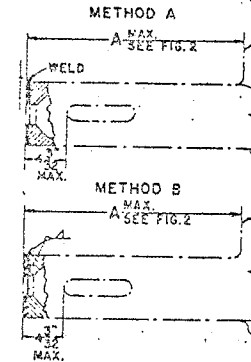


LIMIT OF WEAR ON BOTTOM  
OF SHANK FROM CONTACT  
WITH CARRIER

LIMIT OF SHANK BEND

FIG. 6

FIG. 7



WORN COUPLER BUTT MAY BE RESTORED AS SHOWN BY ELECTRIC WELDING. WELDED SURFACE SHOULD BE REASONABLY SMOOTH AND IN A PLANE PERPENDICULAR TO THE CENTER LINE OF THE SHANK.

WORN COUPLER BUTT MAY BE RESTORED BY WELDING ON A STEEL PLATE AS SHOWN. THE BUTT MUST FIRST BE MACHINED PERPENDICULAR TO THE CENTER LINE OF THE SHANK. THE PLATE MUST BE SMALLER THAN THE BUTT SURFACE TO PROVIDE SPACE FOR WELDING EQUAL IN WIDTH TO THE PLATE THICKNESS UP TO 1/4

METHODS OF RESTORING RIGID SHANK LENGTH

FIG. 8

CC-11-11628 OCT 21 1975 REC'D

# RAILROAD TANK CAR SAFETY RESEARCH AND TEST PROJECT AN RPI-AAR COOPERATIVE PROGRAM

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Association of American Railroads

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President, Operations  
North American Car Corporation

PROJECT DIRECTOR  
Earl Phillips

DEPUTY PROJECT DIRECTOR  
Lee Olson

October 17, 1975

Mr. Ross Gill  
Rail Operations Controller  
U. S. Department of Transportation  
Transportation Test Center  
Pueblo, Colorado 81004

SUBJECT: Switchyard Impact Tests - RPI-AAR Phase 15

Dear Mr. Gill:

1. Enclosed is the procedure for filling the tank cars with water to the rail load limit. This procedure was prepared by J. E. Everett as requested at the October 1, 1975 meeting.
2. For your information, GATX has also calculated heat loss on a 33,500 gallon tank and find that if loaded with 21,500 gallons of water at 60°F and allowed to stand in a 0°F environment, the water will drop to 32°F in 29 hours with no wind and 20 hours with a 10 mph wind.
3. We have contacted Mr. N. Morella, as requested, and he advises that raising the cut lever after the coupler knuckle is open will be the best assurance that the knuckle thrower is clear of the knuckle lock.

(cont'd...

Reply to: Project Director — Tank Car Research  
Association of American Railroads, Technical Center  
3140 South Federal Street, Chicago, Illinois 60616  
312-225-9600 ext 863

Mr. Ross Gill  
October 17, 1975  
Page 2...

4. GATX 57688 and GATX 92571 are now at General American's Argentine, Kansas repair shop being conditioned for test purposes. This completes the estimated package of 4 tank cars required for Series 1 testing. It is anticipated these cars will be at TTC by November 10, 1975.

Very truly yours,



L. J. Schlink

mr  
Enclosure

cc: D. M. Dancer  
J. E. Everett  
E. L. Kunz  
L. L. Olson  
E. A. Phillips  
C. E. Reedy

TANK FILL PROCEDURE

## A. PRELIMINARY CALCULATIONS TO DETERMINE TANK OUTAGE REQUIRED.

1. Determine weight of water to be put in car to bring car to 263,000 pounds. Subtract light weight of car (stenciled on side of car) from 263,000 pounds. Convert this weight to gallons by dividing by 8.33.
2. Determine outage (vapor space above liquid) in gallons by subtracting the volume, in gallons, to be put in the tank from the total capacity of tank, in gallons. The total gallon capacity is stenciled on the head of the tank.
3. Determine outage in inches for the above outage requirements in gallons by referring to the proper outage table for the car in question.

EXAMPLE:

Tank car lightweight 85,300 pounds (assumed)  
Find weight of water to put in tank  
 $263,000 - 85,300 = 177,000$  pounds  
Find volume in gallons  
 $177,000 \div 8.33 = 21,248$  gallons  
Find outage in gallons  
From head of tank, capacity is 33,653 gallons  
 $33,653 - 21,248 = 12,405$  gallons outage req'd.  
Find outage in inches from outage table  
Looking at table, 12,405 gallons = 47-1/4 inches

## B. PROCEDURE FOR FILLING TANK

1. Set liquid level outage gage to 47-1/4 inches, open valve on top of gage.
2. Connect water fill hose to one of the two (2) tank eduction angle valves. These are the large valves on the longitudinal center line of the car. The other valve to be closed.
3. Open the eduction angle valve to which the water hose is connected and turn on water and begin to fill tank.
4. When water starts into tank, crack the induction angle valve. This is the large valve off of the longitudinal center line. Regulate this valve so that some air bleeds out of the tank but maintains a slight pressure (3 to 5 PSI) in the tank so that air also bleeds out of the liquid level tube. This pressure is not critical. Its only purpose is to insure that when the level of water reaches the bottom of the liquid level outage gage tube some water squirts out of the top of the tube to indicate the tank is at the level set on the tube. The pressure should not be so high as to oppose the flow of water into the tank.

5. When water squirts out of the liquid level tube the water is to be shut off. Open the induction valve wide to relieve any pressure in the tank and disconnect water line. Push the liquid level tube down and lock it and close its valve. Close the induction and eduction valves. The tank is now at 263,000 pounds.

C. PROCEDURE FOR EMPTYING TANK

1. Open induction valve (this is the valve off of the longitudinal center line) to relieve any pressure in the tank.
2. Connect an air line to the induction valve.
3. Connect a nipple approximately 12" long to either eduction valve so water will discharge outside housing. (eduction valve is either one on longitudinal center line).
4. Open eduction and induction valve and turn on air to tank. (max. pressure 100 PSI, 20 PSI should be adequate.
5. When tank is empty, shut off air supply and disconnect hose. Open induction valve to relieve pressure in the tank. When pressure is relieved, close all valves.

CAPACITY FOR 1 1/2" MANWAY 1.10

INS	GALS	INS	GALS	INS	GALS	INS	GALS	INS	GALS
0	2	10	1320	20	2664	30	4008	40	5352
1/4	3		1375		2733		4077		5427
1/2	10		1419		2800		4142		5490
3/4	20		1470		2878		4218		5568
1	30	11	1521	21	2936	31	4270	41	5646
1/4	61		1572		3001		4349		5724
1/2	80		1624		3073		4428		5802
3/4	100		1677		3143		4508		5880
2	121	12	1729	22	3202	32	4588	42	5958
1/4	144		1783		3281		4668		6036
1/2	169		1837		3352		4749		6114
3/4	194		1892		3423		4830		6192
3	221	13	1947	23	3493	33	4910	43	6270
1/4	248		2002		3564		4991		6348
1/2	277		2058		3635		5072		6426
3/4	307		2115		3706		5153		6504
4	338	14	2172	24	3778	34	5234	44	6582
1/4	370		2229		3850		5315		6660
1/2	403		2287		3923		5396		6738
3/4	436		2346		3995		5477		6816
5	471	15	2404	25	4069	35	5558	45	6894
1/4	506		2464		4142		5639		6972
1/2	543		2523		4215		5720		7050
3/4	580		2583		4289		5801		7128
6	618	16	2644	26	4363	36	5882	46	7206
1/4	656		2705		4438		5963		7284
1/2	696		2766		4512		6044		7362
3/4	736		2828		4587		6125		7440
7	777	17	2890	27	4663	37	6206	47	7518
1/4	819		2953		4738		6287		7596
1/2	861		3016		4814		6368		7674
3/4	904		3079		4890		6449		7752
8	948	18	3143	28	4966	38	6530	48	7830
1/4	992		3207		5043		6611		7908
1/2	1037		3271		5119		6692		7986
3/4	1083		3336		5196		6773		8064
9	1129	19	3401	29	5273	39	6854	49	8142
1/4	1176		3467		5351		6935		8220
1/2	1223		3532		5429		7016		8298
3/4	1271		3599		5507		7097		8376

7000 INCHES REPRESENTS MANWAY NOZZLE CAPACITY  
 88 REPRESENTS SHELL CAP. PLUS MANWAY CAPACITY

GATX 92930  
 91833  
 92561

# RAILROAD TANK CAR SAFETY RESEARCH AND TEST PROJECT AN RPI-AAR COOPERATIVE PROGRAM

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North American Car Corporation

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Earl Phillips

DEPUTY PROJECT DIRECTOR  
Lee Olson

October 31, 1975

Mr. R. T. Gill  
Rail Operations Controller  
U. S. Department of Transportation  
Transportation Test Center  
Pueblo, Colorado 81004

SUBJECT: Phase 15 Switchyard Impact Tests

Dear Mr. Gill:

GATX 57688 and GATX 92571 are currently being prepared for shipment to TTC and are expected to be at North Avondale by November 10, 1975. These cars complete the package of four tank cars expected to be used in Series 1 testing. General American outage table No. 6895 (you have a copy) applies to these cars also.

UTLX 38482, UTLX 38493, UTLX 38498 and UTLX 38547 will be furnished for Series 2 tests. Enclosed are drawings (71075, 70883 and 70884), specifications and outage tables for these cars. (U.S. Table 1197 applies to UTLX 38482, 38547, and 38493. U.S. Table 1193 is for UTLX 38498.)

Very truly yours,



/mr

cc: D. M. Dancer  
J. E. Everett  
E. L. Kunz  
L. L. Olson  
D. A. Peters  
E. A. Phillips  
C. E. Reedy

L. J. Schlink

Reply to: Project Director — Tank Car Research  
Association of American Railroads, Technical Center  
3140 South Federal Street, Chicago, Illinois 60616  
312-225-9600 ext 863



Table with columns for Inches and Gals. for nozzle capacity (1 Gallons Shell Capacity). It lists various nozzle sizes (e.g., 1/4, 1/2, 3/4) and their corresponding gallon capacities across multiple rows.

TABLE 1198

Table with columns for Inches and Gals. for nozzle capacity (1 Gallons Shell Capacity). This table continues the list of nozzle sizes and gallon capacities, providing a comprehensive reference for various nozzle specifications.

Table with 12 columns and 12 rows of nozzle and shell capacity data. Each row represents a nozzle size (e.g., 1/4 inch) and lists nozzle capacities in gallons for various shell diameters (e.g., 14, 15, 16 inches).

Table with 12 columns and 12 rows of nozzle and shell capacity data, continuing from Table 1193. It follows the same structure of nozzle size vs. shell diameter and capacity in gallons.



# UNION TANK CAR COMPANY

111 W. JACKSON BLVD., CHICAGO, ILL. 60604, TELEPHONE 431-3111, (AREA CODE 312)

MODEL NUMBER ISSUED

TANK CAR SPECIFICATIONS FOR QUOTATION NUMBER B.D. 67-100-34 (0969) DATE September 24, 1969

CUSTOMER U.T.C. Fleet COMMODITY LPG-AA WEIGHT PER GAL. 4.89#

DOT 112A340W COMPTS 1 GALLONS NOMINAL CAPACITY 33,800 ALLOWABLE WEIGHT PER GALLON 5.1#

GENERAL DATA: SHELL CAPACITY 33,800 GALS. INCLUDES 0 % OUTAGE MAXIMUM WT. ON RAILS 263,000#  
LIGHTWEIGHT OF CAR 38,600# LENGTH OVER STRIKERS 64'-10" LENGTH OVER TRUCK CENTERS 54'-6"  
HEIGHT 15'-0 $\frac{1}{2}$ " WIDTH 10'-5 $\frac{1}{2}$ " RADIUS OF CURVATURE CAR CAN NEGOTIATE 238 Ft.

TANK: PLATE SPECIFICATION T.C. 128-B OUTSIDE DIAMETER: SHELL 119.3" HEADS 119.3"  
PLATE THICKNESS - SHELL 5/8" HEADS 11/16" LENGTH OVER SEAMS 56'-2 $\frac{1}{2}$ "  
TANK TESTED TO 340 P.S.I. TANK INTERIOR PREPARATION Sweep Clean

HEATER PIPES: DESIGN None INLETS - OUTLETS - NO. OF RUNS -  
SIZE - MATERIAL -

BODY: DESIGN HD (No Underframe) RUNNING BOARDS Top of Tank - AAR Approved  
END PLATFORM AAR Approved SAFETY PLATFORM 2 Board - 4 Way  
BRAKES WABCO PAC HAND BRAKE Vertical Handwheel

TRUCKS: DESIGN Barber CAPACITY 100-Ton JOURNAL BEARINGS Roller  
WHEELS 36" One Wear MUDGUARDS None

INSULATION: None JACKET None

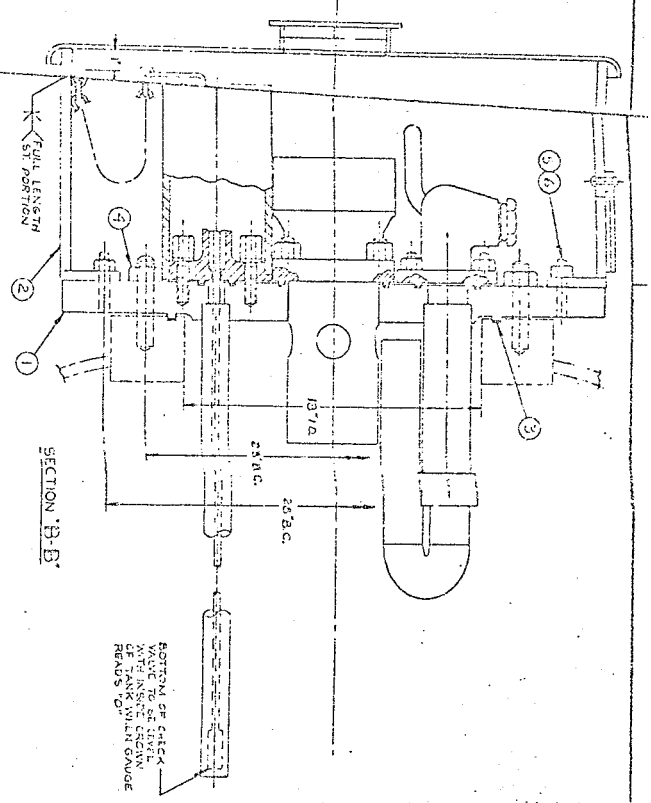
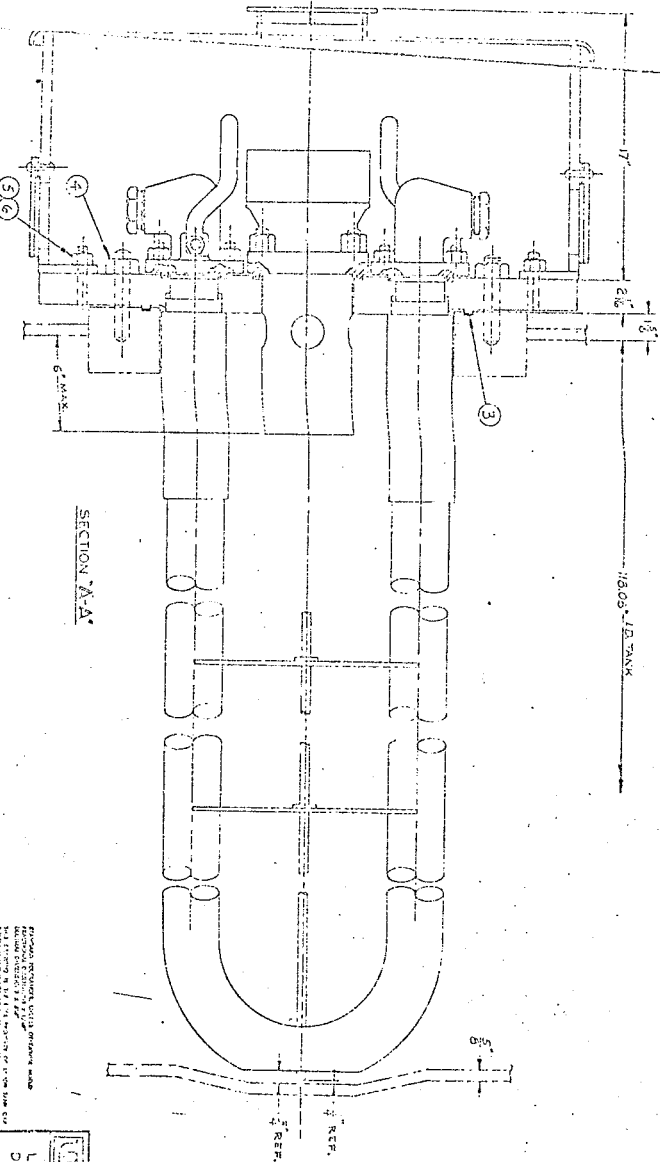
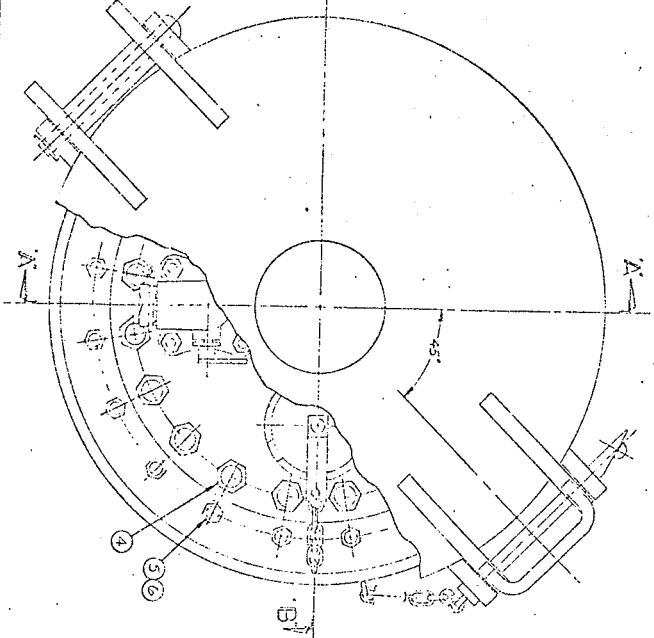
FITTINGS: BOTTOM UNLOADING None VALVE SIZE AND TYPE - CONNECTION -  
OVERHEAD UNLOADING 2-2" VALVE SIZE AND TYPE Ball Type, Angle, Flanged PIPE SIZE 2-3" Steel  
AIR VALVE 1-2" SIZE AND TYPE Ball Type, Angle, Flanged, Steel Body-SS Ball  
WASHOUT NOZZLE None VACUUM RELIEF VALVE None  
SAFETY RELIEF Valve 280.5psi MANWAY COVER 18" Pressure Type TELL TALE None  
THERMOMETER WELL 3/4" Steel SAMPLING LINE 1/2" Steel (S.S. Valve)  
GAUGING DEVICE Slip Tube GASKET MATERIAL Chemical Asbestos

PAINT: FINISH Black and White Alkyd STENCILLING AAR-DOT  
ADVERTISING None

LINING: None RUBBER SADDLE None

SPECIAL DESIGN FEATURES: 1.0 Joint Efficiency  
125-Ton Body Bolsters  
Car Equipped with Excess Flow Valves





REVISIONS

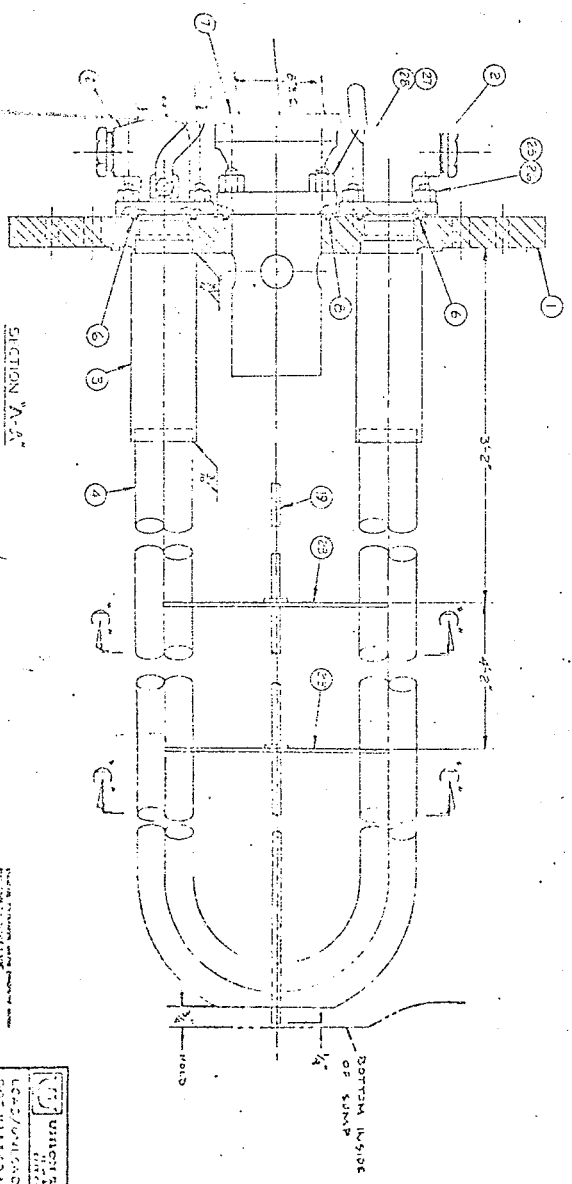
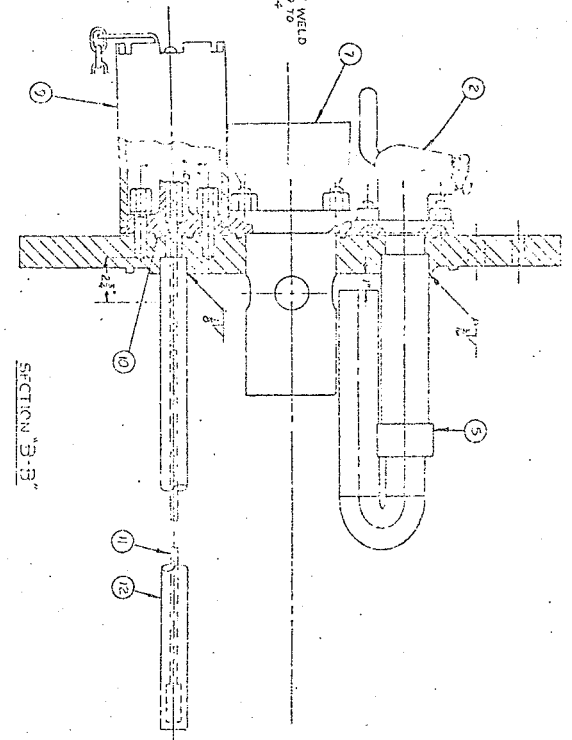
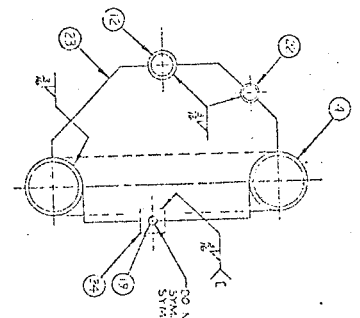
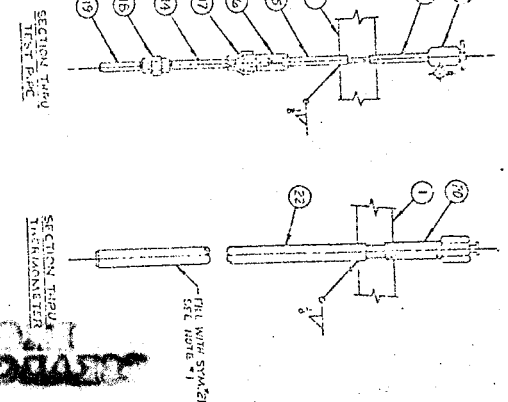
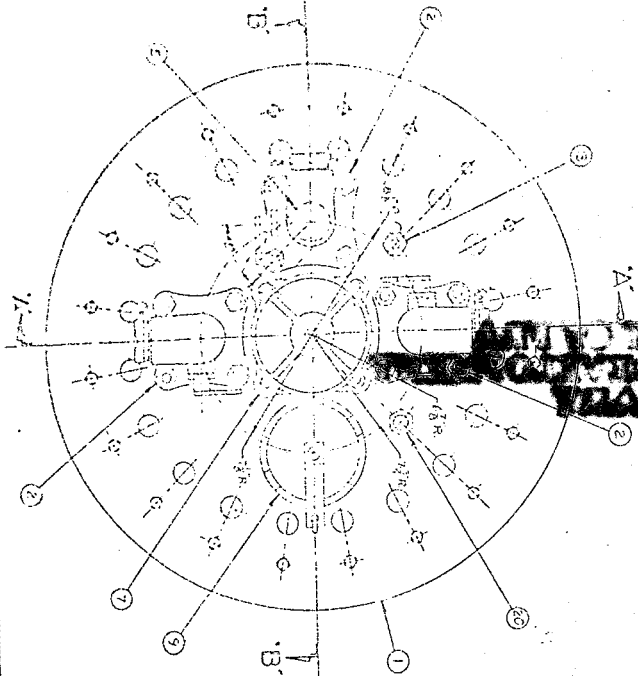
NO.	DATE	DESCRIPTION	BY	CHKD.
1	10/12/50	ISSUED FOR FABRICATION	W. J. HARRIS	J. W. HARRIS
2	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
3	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
4	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
5	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
6	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
7	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
8	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
9	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS
10	10/12/50	REVISION	W. J. HARRIS	J. W. HARRIS

70824

UNITED STATES GUN CO.  
DOT 12.5/300M TANK CAR

70824

70824



NOTES:  
 1. ANTI-FREEZE TO BE 20-50 MIXTURE OF ETHYLENE GLYCOL AND WATER.  
 2. VALVE HANDLES SHOWN IN OPEN POSITION.

NO.	DESCRIPTION	QTY	UNIT	REMARKS
1	VALVE BODY	1	EA	
2	VALVE PLATE	1	EA	
3	VALVE PLATE GASKET	1	EA	
4	VALVE PLATE NUT	1	EA	
5	VALVE PLATE WASHER	1	EA	
6	VALVE PLATE LOCKWASHER	1	EA	
7	VALVE PLATE SCREW	1	EA	
8	VALVE PLATE GASKET	1	EA	
9	VALVE PLATE NUT	1	EA	
10	VALVE PLATE WASHER	1	EA	
11	VALVE PLATE LOCKWASHER	1	EA	
12	VALVE PLATE SCREW	1	EA	
13	VALVE PLATE GASKET	1	EA	
14	VALVE PLATE NUT	1	EA	
15	VALVE PLATE WASHER	1	EA	
16	VALVE PLATE LOCKWASHER	1	EA	
17	VALVE PLATE SCREW	1	EA	
18	VALVE PLATE GASKET	1	EA	
19	VALVE PLATE NUT	1	EA	
20	VALVE PLATE WASHER	1	EA	
21	VALVE PLATE LOCKWASHER	1	EA	
22	VALVE PLATE SCREW	1	EA	
23	VALVE PLATE GASKET	1	EA	
24	VALVE PLATE NUT	1	EA	
25	VALVE PLATE WASHER	1	EA	

UNION PACIFIC  
 LCA-2/VALVING S/A  
 DOT 104333W VALVING CAR

70243