

Administration

X2000 U.S. Demonstration Vehicle Dynamics Trials, Preliminary Test Report

Office of Research and Development Washington, D.C. 20590

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PREFACE

Many advanced intercity high-speed train technologies have become an operating reality in recent years. Though mostly of foreign origin, these new trains offer the potential for immediate application in the United States to lessen trip times and improve ridership. Each high-speed train has been developed to meet the particular operating environment appropriate to the parent country's transportation policy, and must be evaluated with regards to applicability to U.S. practices and expectations to ensure that the safety levels are maintained in the U.S. environment. This responsibility rests with the Federal Railroad Administration (FRA), U.S. Department of Transportation (U.S. DOT), which is charged with ensuring the safety of rail systems in the United States under the Federal Railroad Safety Act of 1970, as amended.

The Swedish X2000 tilting train, manufactured by ASEA-Brown Boveri (ABB), offers opportunity for application over the existing rail infrastructure. For evaluation purposes, a representative X2000 trainset was provided to Amtrak by the Swedish State Railways (SJ) for test and revenue service demonstration in the U.S. Northeast Corridor. A cooperative test effort was conducted under the direction of Amtrak and supported by the FRA Office of Research and Development, with test instrumentation supplied and operated by SJ, data analysis support provided by ABB, and test monitoring maintained by the FRA Office of Safety. Based on the results of the performance testing, the trainset was entered into a revenue service demonstration.

This report describes the procedures and results of the vehicle dynamics tests carried out with the X2000 trainset in the Northeast Corridor and on the Philadelphia - Harrisburg line, in a time period between October, 1992, and January, 1993. Instrumented wheelsets, installed on both the power car and cab car ends of the trainset, provided direct and immediate measurement of the wheel/rail forces experienced during high speed and high cant deficiency operation. In order to attain maximum speeds in tangent and curved track, the tests were conducted incrementally, with analysis of forces and accelerations evaluated against safety criteria during and at the conclusion of each test run before proceeding to the next stage.

This test report, prepared for the U.S. DOT, FRA Office of Research and Development, is preliminary in nature. Its purpose was to provide the FRA Office of Safety Enforcement with timely technical data and test results on which to base decisions in establishing operating limits for the ensuing revenue service demonstration of the X2000 trainset in the Northeast Corridor. The final report describing the complete test program and results will be forthcoming in a separate document.

The authors wish to thank Arne Bang and Thomas Schultz of the FRA Office of Research and Development, for their direction and support in realizing the test and demonstration, and Ken Koehler who managed the program for Amtrak. Valuable information during the test program and in the preparation of this document was provided by Amtrak, under the test direction of Ed Lombardi, by Al Shaw, Michael Trosino and Conrad Ruppert.

The authors also wish to thank Al MacDowell and William O'Sullivan of the FRA Office of Safety, and Herbert Weinstock of the Volpe National Transportation Systems Center for their careful monitoring and judgement in the progression of all tests.

In the conduct of tests, the personnel of ABB Traction, lead by Jan-Olof Häggblad and Roger Nilsson, and the personnel of SJ, lead by Lennart Kloow and Martin Bäfverfeldt are gratefully acknowledged for their careful preparation, proficient data collection and presentation.

Finally, the authors wish to thank Thomas Edwards of ABB Traction for his thorough, informed analysis and interpretation of the test data and valuable discussions throughout the program.

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X2000 U.S. DEMONSTRATION VEHICLE DYNAMICS TRIALS

TABLE OF CONTENTS

<u>Secti</u>	<u>on</u>		Page
1.	BACK	GROUND/INTRODUCTION	1
	1.1 1.2 1.3	Summary	2
2.	SAFE	TY REQUIREMENTS	4
	2.1	Safety Criteria	4
3.	TEST	PROCEDURE	7
	3.1 3.2 3.3 3.4 3.5 3.6	Train Configuration	8 11 12 15
4.	RESU	LTS	18
	4.1 4.2 4.3 4.4 4.5 4.6 4.7 4.8 4.9	Maximum Unbalance Recorded	25 27 27 27
5.	DISC	JSSION OF RESULTS	45
	5.1 5.2 5.3 5.4	Test Highlights and Significant Events	45

TABLE OF CONTENTS (con't)

Sectio	<u>n</u>		<u>Page</u>
	5.5 5.6	Effect of Side-wind on Attainable Cant Deficiency Effect of Track Geometry Variance on Attainable Cant	46
		Deficiency	47
	5.7	Effect of Speed Variance on Attainable Cant Deficiency	
	5.8	Effect of Vehicle Condition on Attainable Cant Deficiency	47
	5.9	Summary of Effects on Sustainable Operational Cant Deficiency	48
6.	PRELI	MINARY RECOMMENDATIONS AND CONCLUSIONS	49
	6.1	Recommendation for Operation at 9" of Cant Deficiency	49
	6.2	Recommended Conditions for 9" Cant Deficiency Operation	50
	6.3	Recommendations for Operation at 10" of Cant Deficiency in Selected Curves	51
	6.4	Recommendation for 135 mph Maximum Operation Speed	52
APPEN	IDIX A	Test Event Log, X2000 U.S. Demonstration	
ΔPPFN	IDIX B	Track Curve Information	

LIST OF TABLES

	<u>Page</u>
Transducers and Signal Names for X2000 Test Runs	9
Strip Chart Recorder Channel Designations	11
X2000 Test Runs in Chronological Order	16
Peak Values Measured From All Test Zones, Harrisburg and	
NEC Lines	19-20
Peak Values, Simulated Revenue Run, NEC,	
Washington - New York	30-33
•	
	37-44
	Strip Chart Recorder Channel Designations

LIST OF FIGURES

<u>Fig</u>	<u>ure</u>	<u>Page</u>
3.1	Transducer Configuration, X2000 Tests	. 10
4.1 4.3 4.4 4.5 4.6 4.7 4.8 4.1 4.1 4.1 4.1 4.1	Minimum Vertical Wheel Force, Measured in Curve 671, Westbound Peak Net Axle Lateral Forces, Locomotive (Composite of Test Runs) Peak Net Axle Lateral Forces, Cab Car (Composite of Test Runs) Peak Net Axle Lateral Force, Axle 24, In Curve 672, Track 4 Peak Maximum Wheel L/V Ratios (Composite, All Wheels, Test Runs) Peak Maximum Wheel L/V Ratios, Left Wheel, Axle 1, Curve 663 Peak Maximum Truck Side L/V Ratios (Composite of Test Runs) Peak Maximum Truck Side L/V Ratios, Truck 12 (Cab) in Curve 672 Minimum Vertical Wheel Forces, Simulated Revenue Service Run Peak Net Axle Lateral Forces, Simulated Revenue Service Run Maximum Wheel L/V Ratios, Simulated Revenue Service Run Minimum Vertical Wheel Forces, Simulated Revenue Service Run Minimum Vertical Wheel Forces, Simulated Revenue Run + 5 mph Peak Net Axle Lateral Forces, Simulated Revenue Run + 5 mph Maximum Wheel L/V Ratios, Simulated Revenue Run + 5 mph Maximum Wheel L/V Ratios, Simulated Revenue Run + 5 mph	21 22 23 23 24 25 26 26 28 29 34 35
5.1	Effect of 5 mph Overspeed on Cant Deficiency	48

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1. INTRODUCTION/BACKGROUND

1.1 SUMMARY

The evaluation program for the X2000 trainset involved a series of different technical tests followed by two simulated or demonstration revenue service operations. Each test in sequence was dependent upon successful completion and analysis of performance from previous tests.

The overall test sequence was as follows:

- 1) Commissioning confirmed operational readiness.
- 2) Cant Deficiency established safe curving limits.
- 3) High Speed Stability established maximum safe speed.
- 4) Pre Revenue Test Runs demonstrated the safety of the intended revenue service operation.

The purpose of this preliminary test report is to document the procedures, events and results from the overall test program, to support Amtrak's request for FRA approval for operation in revenue service.

Current plans for revenue service type operations include approximately four months of revenue service between Washington, DC and New Haven (or New York City).

1.1.1 Commissioning Tests in Northeast Corridor

The purpose of the commissioning tests was to confirm operational readiness, up to 125 mph, with particular interest in: 1) propulsion systems, 2) safety appliances (i.e.-lights, horns, etc.), 3) brake systems, and 4) cab signals.

A stop test using only air brakes was performed from 125 mph.

Operational checkout was also performed for:

- tight switch/curve negotiation,
- clearances,
- ride quality of a coach and locomotive,
- basic vehicle stability,
- stop distance,
- EMI (including during regeneration braking),
- pantograph uplift forces, and
- acceleration/current draw and transformer in-rush current.

(NOTE: interior and wayside sound level, stop distances, and wheel and disc temperatures were assessed using data provided by ABB).

1.1.2 Cant Deficiency Tests

5" to 12" cant deficiency runs were conducted over a test zone between Harrisburg and Philadelphia (curves between MP 44 to MP 68 were identified as suitable test candidates.

7" to 12" cant deficiency tests were run between New Brunswick and Metro Park.

1.1.3 High Speed Stability Tests

Tests of high speed stability were conducted east of Trenton between MP34 and MP54 on the Northeast Corridor (NEC) Mainline. Tests were scheduled to a maximum speed of 150 mph.

Stop tests, using air brakes only, were performed during a run at which 135 mph was achieved and a run at which 151 mph was achieved.

1.1.4 Pre-Revenue Test Run - Round Trip Washington to New York City

A recommended revenue speed profile run between Washington and New York City was submitted by Amtrak and approved by the FRA. Following the above tests, two round trips were made between Washington and New York City, one at the proposed revenue service cant deficiency/speed profile and the second at a speed profile 5 mph faster where the 125 mph maximum speed would not be exceeded.

1.1.5 New York to Boston Demonstration

Following the successful completion of the above tests and approval by the FRA, the X2000 was operated on several demonstration runs at a maximum of seven inches of cant deficiency on Metro North and eight inches of cant deficiency elsewhere. This consist was powered by two RTL turbo locomotives, between New Haven and Boston.

1.1.6 Revenue Service Operation

Following successful completion of the above and approval by the FRA, the X2000 will be placed in service in the Northeast Corridor from New Haven and New York City to Washington and from New York City to Boston for approximately two (2) months.

1.2 INTRODUCTION AND AIMS

The objective of this test was to determine the suitability of the X2000 trainset for operation at elevated cant deficiencies and speeds in Amtrak's Northeast Corridor under existing track conditions. The results of the technical tests will be used as a basis for the FRA to assess and evaluate Amtrak's request to run the X2000 at higher cant deficiencies and speeds in a revenue service demonstration.

1.3 REPORT ORGANIZATION

The purpose of this preliminary test report is to document the procedures, events and results from the overall test program as a reference for the FRA to assess Amtrak's request for demonstration in revenue service.

The safety criteria against which the performance of the X2000 test train was examined during the tests are reviewed in Section 2. The train configuration, instrumentation, procedures, and test locations are discussed in Section 3. Preliminary results of testing on the Philadelphia - Harrisburg and NEC mainlines are presented in Section 4. In Section 5, the significance of the results are discussed, and in Section 6, preliminary conclusions and recommendations are drawn from the results.

2. SAFETY REQUIREMENTS

The fundamental basis for safe operation at higher cant deficiencies and speeds is the satisfactory control of forces acting at and across the wheel/rail interface. Safety criteria are concerned with assessing the risk of vehicle derailment through vehicle overturning, wheel climb, track gage widening (rail rollover, lateral deflection), lateral panel shift, and truck hunting.

2.1 SAFETY CRITERIA

Instrumented wheelsets were installed on the locomotive and on the driving trailer (cab car) of the X2000 trainset (a total of 4) to directly measure wheel/rail forces during these tests. The safety criteria against which the measured wheel forces are assessed were established prior to testing and are given below. These parameters and limits were used to monitor all test operations:

1) Track Panel Shift: Net Axle Lateral Force (NAL) < 0.5 x Static Axle Load

for the X2000 locomotive,

NAL < 90 kN

for the X2000 cab car,

NAL < 78 kN

- 2) Wheel Climb Derailment: L/V Ratio (Nadal), Single Wheel < 0.8
 - conditions considered safe if each wheel L/V is less than 0.8; if any wheel exceeds 0.8, then:

Axle Sum L/V Ratio (Weinstock) < 1.0

- examine axle sum if single wheel L/V exceeds 0.8; conditions are considered safe if sum is less than 1.0
- 3) Rail Rollover: Truck Side L/V Ratio (T-L/V) < 0.5
- 4) Vehicle Overturn: Minimum Vertical Wheel Force (Vmin) > -10% of Static Wheel Load

for the X2000 locomotive,

Vmin > 9.0 kN

for the X2000 cab car,

Vmin > 7.8 kN

- 5) Truck Hunting: | Truck Frame Acceleration | < 0.8 g
 - no sustained oscillations

Measurements of safety parameters 1) - 4) were low-pass filtered at 25 Hz; measurements of 5), truck frame acceleration, were band-pass filtered, 2 - 8 Hz.

During any test run, these safety criteria were monitored to ensure that none of the above limits were exceeded. Data projections had been used to minimize the likelihood that any safety limit would be exceeded. Prior to each run above five inches of cant deficiency, the track was visually inspected by Amtrak.

If any stop test criterion was met or exceeded during the test period, that condition was used to define the limiting speed for that particular curve.

Vertical and lateral accelerations were recorded at various locations on the car body. For future test considerations, it may be desirable to correlate carbody accelerations versus instrumented wheelset measurements.

Review of Test Safety Assurance

Prior to test initiation, ABB provided test results from previous X2000 trials carried out in Germany. It was demonstrated that, during these tests, no safety criteria limits were reached and that a substantial margin of safety was evident for all cant deficiencies. Issues of note included:

- o top speed was 251 km/h; maximum cant deficiency was 12 inches.
- o track in Germany is of better Class than in U.S.; measured lateral forces on U.S. track were expected to be somewhat higher, but the load limits are higher also.
- o radial steering made a significant contribution to the reduction of wheel/rail forces in curves of 500 m radius and greater; for curve radii less than 500 m, partial radial steering was purported to reduce wear and wheel/rail noise.

Comparisons of simulation predictions and measurements taken from tests in Sweden were also provided; agreement was good (given the limitations of the simulation) and a good margin of safety was both predicted and observed.

For comparison purposes, measurements taken from previous tests-on the NEC of a somewhat similar vehicle, the "banking Amcoach", at cant deficiencies up to 12 inches were reviewed. Again, a good margin of safety was observed.

A test zone of the Harrisburg Line, including 4 principal curves, was referenced for the presentation of simulation predictions. ABB provided model projections of the anticipated forces and L/V ratios using, as input, track data (specifically Track 4) from this test zone provided by Amtrak. Items noted include:

- a 2-point wheel-rail contact condition could occur in most curves of the Harrisburg Line, given the worn track profile; projections for both single and 2-point contact conditions were reviewed.
- significant track alignment deviations measured by Amtrak at the beginning and end of curve transition spirals were included in the simulation.

 the critical speed (hunting), even at an equivalent conicity of 0.4, is predicted to be well above 150 mph (~165 - 175 mph).

Extensive vehicle dynamic simulations were carried out for the X2000 configuration, the details of which are given in (proprietary) ABB Reports TRP 9224 and TRP 9226. The data used in these simulations are representative of the X2000 vehicle types that went to make up the actual X2000 trainset under test in the United States.

The relevant pages of TRP 9226 give an explanation of the main parameters used in the simulations mentioned above. Thereafter follow several tables giving the values of parameters for the different vehicles in the X2000 of the mathematical model.

3. TEST PROCEDURE

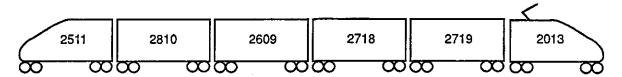
3.1 TRAIN CONFIGURATION

The X2000 trainset used during the trials was comprised of a 6 car consist as indicated below.

CAR TYPE	CAR CLASS	CAR NUMBER
Locomotive	X2	2013
Coaches	UA2	2719
	UA2	2718
	UA2	2810
First-Class Buffet	UAR2	2609
Driving Trailer (Cab C	ar) UA2X	2511

$$UA2X + UA2 + URA + UA2 + UA2 + X2$$

Driving trailer + 1st Class Car + Bistro Car + 1st Class Car + 1st Class Car + Power Unit



Two RTL turbo power cars were coupled to the X2000 trainset for motive power in the non-electrified territory between New Haven and Boston only.

Wheel Profile

The X2000 demonstrated in the US was equipped throughout with S1002 wheel profiles with a thin 30mm flange. This profile had been chosen to approximate the AAR 1B, and to provide:

- adequate conicity and thus steering of wheelsets in curves,
- o stable running at speed even on sections of tight gauge (no less than 1428mm), and
- a stable wheel profile shape which should not change too much with wear.

The X2000 wheel profile was checked by superimposing it on the Amtrak standard wheel profile per drawing 246. The Amtrak wheel profile is identical to the AAR wheel profile, the only exception being the tread taper modified from 1:20 to 1:40. The comparison showed the X2000 and Amtrak profiles to be very similar, and the X2000 profile was approved for use on the Amtrak system.

The suitability of this profile to conditions on the North East Corridor (NEC) has been investigated by ABB for the 140 RE rail profile both as new and for actual worn rail profiles measured in curves 662 and 663 (track #4) at Gap and Eby's on the Harrisburg Line, and from worn rail head profiles for tangent track of the section of the NEC where 150 mph running was performed. An analysis of the profiles indicates that rail heads are worn slightly flatter than new 140RE rail which leads ABB to expect that equivalent conicities exceeding 0.4 are possible (continuous rail head profiles would be needed to enable a check of the entire route). Significant deviation of maximum likely equivalent conicity from the above values was not likely and did not occur as far as known.

For more detailed description and analyses of the probable wheel-rail combinations met during trails on the Harrisburg Line and for nominal conditions in the United States of America, see ABB Report TRP 9224, Section 3.3.

3.2 INSTRUMENTATION

A description of the measurement transducers and their locations on the vehicle is given in Table 3.1, and depicted in Figure 3.1.

The nomenclature used to define each signal name was as follows:

V = Vertical wheel/rail force

L = Lateral wheel/rail force

y = Lateral acceleration

z = Vertical acceleration

I = left side

r = right side

a = axle, on axle bearing

b = bogie (truck), on bogie

cb = car body, on car floor over bogie (truck) center

TABLE 3.1 TRANSDUCERS AND SIGNAL NAMES FOR X2000 TEST RUNS

Signal #	Transducer Type	Signal Name	Description
1	Instrumented Wheelset	L1I	W/R Lateral Force, Axie 1, left wheel (Locomotive)
2	Instrumented Wheelset	L1r	W/R Lateral Force, Axle 1, right wheel (Locomotive)
3	Instrumented Wheelset	V1I	W/R Vertical Force, Axle 1, left wheel (Locomotive)
4	Instrumented Wheelset	V1r	W/R Vertical Force, Axle 1, right wheel (Locomotive)
5	Instrumented Wheelset	L2I	W/R Lateral Force, Axle 2, left wheel (Locomotive)
6	Instrumented Wheelset	L2r	W/R Lateral Force, Axle 2, right wheel (Locomotive)
7	Instrumented Wheelset		W/R Vertical Force, Axle 2, left wheel (Locomotive)
8	Instrumented Wheelset	V2r	W/R Vertical Force, Axle 2, right wheel (Locomotive)
9	Instrumented Wheelset	L23I	W/R Lateral Force, Axie 23, left wheel (Cab Car)
10	Instrumented Wheelset	L23r	W/R Lateral Force, Axle 23, right wheel (Cab Car)
11	Instrumented Wheelset	V23i	W/R Vertical Force, Axle 23, left wheel (Cab Car)
12	Instrumented Wheelset	V23r	W/R Vertical Force, Axle 23, right wheel (Cab Car)
13	Instrumented Wheelset	L241	W/R Lateral Force, Axie 24, left wheel (Cab Car)
14	Instrumented Wheelset	L24r	W/R Lateral Force, Axle 24, right wheel (Cab Car)
15	Instrumented Wheelset	V24I	W/R Vertical Force, Axle 24, left wheel (Cab Car)
16	Instrumented Wheelset	V24r	W/R Vertical Force, Axle 24, right wheel (Cab Car)
17	Servo Accelerometer	ycb1	Lateral Acceleration in car over Bogie 1 (Locomotive)
18	Servo Accelerometer	zcb1	Vertical Acceleration in car over Bogie 1 (Locomotive)
19	Servo Accelerometer	yb1	Lateral Acceleration, Bogie 1 (Locomotive)
20	Variable Capacitance Accelerometer	ya2	Lateral Acceleration, Axle 2 (Locomotive); used to measure unbalance or cant deficiency
21	Servo Accelerometer	ycb5	Lateral Acceleration in car over Bogie 5 (Coach)
22	Servo Accelerometer	zcb5	Vertical Acceleration in car over Bogie 5 (Coach)
23	Servo Accelerometer	yb5	Lateral Acceleration, Bogie 5 (Coach)
24	Servo Accelerometer	ycb12	Lateral Acceleration in car over Bogie 12 (Cab Car)
25	Servo Accelerometer	zcb12	Vertical Acceleration in car over Bogie 12 (Cab Car)
26	Servo Accelerometer	yb12	Lateral Acceleration, Bogie 12 (Cab Car)
27	Servo Accelerometer	ycbRTL	Lateral Acceleration in car over front Bogie of leading RTL unit (Boston - New Haven tests only)
28	Speed Pickup	٧	Trainset forward speed

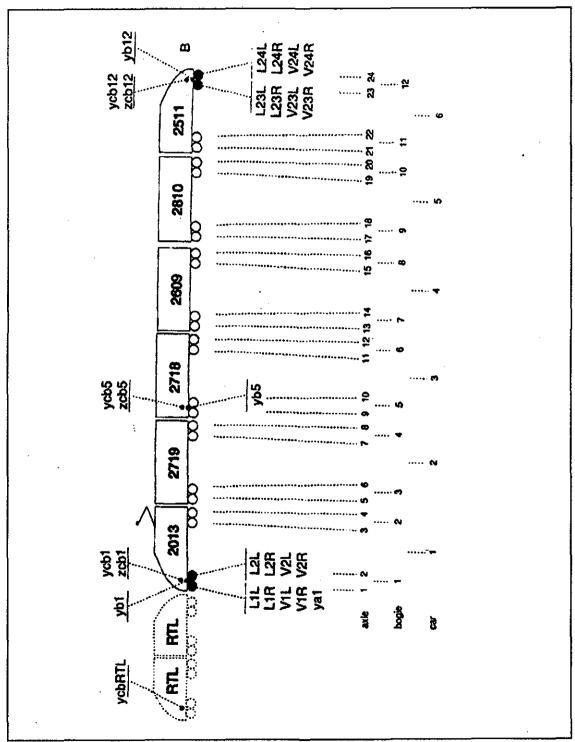


Figure 3.1: Transducer Configuration, X2000 Tests USA

3.3 CHANNEL DESIGNATION

Safety criteria parameters were displayed in real time during the test runs using five 6-channel strip chart recorders. The channel allocations and descriptions are given in **Table 3.2.**

TABLE 3.2 STRIP CHART RECORDER CHANNEL DESIGNATIONS

Stripchart Channel #	Signal Name	Description
1.1	NA1L	Net Axle Lateral Force, Axle 1 (Locomotive) [kN] {0 to ±100 kN}
1.2	V1I	Vertical Wheel Force, Axle 1, left wheel (Locomotive) [kN] {O to 200 kN}
1.3	V1r	Vertical Wheel Force, Axle 1, right wheel (Locomotive) [kN] [0 to 200 kN]
1.4	NA2L	Net Axle Lateral Force, Axle 2 (Locomotive) [kN] {0 to ±100 kN}
1.5	V2I	Vertical Wheel Force, Axie 2, left wheel (Locomotive) [kN] {0 to 200 kN}
1.6	V2r	Vertical Wheel Force, Axle 2, right wheel (Locomotive) [kN] {0 to 200 kN}
2.1	L/V1!	Wheel L/V Ratio, Axle 1, left wheel (Locomotive) {-0.1 to 0.9}
2.2	L/V1r	Wheel L/V Ratio, Axle 1, right wheel (Locomotive) {-0.1 to 0.9}
2.3	L/V2!	Wheel L/V Ratio, Axle 2, left wheel (Locomotive) {-0.1 to 9.9}
2.4	L/V2r	Wheel L/V Ratio, Axle 2, right wheel (Locomotive) {-0.1 to 0.9}
2.5	T1-L/VI	Truck Side L/V Ratio, Truck 1, left side (Locomotive) {-0.1 to 0.9}
2.6	T1-L/Vr	Truck Side L/V Ratio, Truck 1, right side (Locomotive) {-0.1 to 0.9}
3.1	NA23L	Net Axle Lateral Force, Axle 23 (Cab Car) [kN] {0 to ±100 kN}
3.2	V23I	Vertical Wheel Force, Axle 23, left wheel (Cab Car) [kN] {0 to 200 kN}
3.3	V23r	Vertical Wheel Force, Axle 23, right wheel (Cab Car) [kN] {0 to 200 kN}
3.4	NA24L	Net Axle Lateral Force, Axle 24 (Cab Car) [kN] {0 to ±100 kN}
3.5	V24I	Vertical Wheel Force, Axle 24, left wheel (Cab Car) [kN] {0 to 200 kN}
3.6	V24r	Vertical Wheel Force, Axie 24, right wheel (Cab Car) [kN] {0 to 200 kN}
4.1	L/V23I	Wheel L/V Ratio, Axle 23, left wheel (Cab Car) {-0.1 to 0.9}
4.2	L/V23r	Wheel L/V Ratio, Axle 23, right wheel (Cab Car) {-0.1 to 0.9}
4.3	L/V24I	Wheel L/V Ratio, Axle 24, left wheel (Cab Car) {-0.1 to 0.9}
4.4	L/V24r	Wheel L/V Ratio, Axle 24, right wheel (Cab Car) {-0.1 to 0.9}
4.5	T12-L/VI	Truck Side L/V Ratio, Truck 12, left side (Cab Car) {-0.1 to 0.9}
4.6	T12-L/Vr	Truck Side L/V Ratio, Truck 12, right side (Cab Car) {-0.1 to 0.9}
5.1	ya2	Lateral Acceleration, Axle 2 (Locomotive) [m/s²] {0 to ± 2.5 m/s²}
5.2	ycb5	Lateral Acceleration, car over Truck 5 (Coach) [m/s²] {0 to ± 2.5 m/s²}
5.3	ycb12	Lateral Acceleration, car over Truck 12 (Cab) [m/s²] {0 to ± 2.5 m/s²}
5.4	yb12	Lateral Acceleration, Truck 12 (Cab Car) [m/s²] {0 to ± 10 m/s²}
5.5	v	Vehicle forward speed [mph] {0 to 150 mph}
5.6		Tractive effort

3.4 TEST ZONES

The trials run to date have been divided up into four main test zones:

- 100 Series Philadelphia Harrisburg Line between Parkesburg and Lancaster; Cant Deficiency Tests up to 110 mph
- 200 Series Northeast Corridor (NEC) Mainline (Philadelphia New York) between New Brunswick and Metro Park; Cant Deficiency Tests up to 125 mph
- 300 Series NEC Mainline (Philadelphia New York) between Trenton and New Brunswick; High Speed Stability Tests up to 150 mph
- 400 Series NEC Mainline between Washington, DC and New York Penn Station; Simulated Revenue Earning Service Long Distance Runs up to 125 mph

3.4.1 100 Series Test Runs, Philadelphia - Harrisburg Line, MP 44 - 68

The test zone between Parkesburg (MP 44) and Lancaster (MP 68) comprised 24 miles (39 km) of electrified double track on wooden ties with tie-plates and cut spike rail fasteners. The majority of rail was CWR or long welded rail with a 140 RE profile. Some sections of jointed (bolted) rail exist with 39 foot rail lengths and staggered joints. 155 RE rail profiles also occur on this test zone. At approximate intervals of two miles, a 30 foot cut section (insulated joint) was welded into the track for signalling (cab signal) purposes. The track was well bedded in stone ballast. Although the wooden ties fully meet the FRA safety standards for the speeds run, there were a number of isolated locations where ties were allowing little gauge widening restraint.

There are 23 curves encountered within this test zone on each track as described in Appendix B. Four particular test curves were selected for more detailed computer analyses in two groups of reversed pairs for each track. Travelling west in the direction of Lancaster on Track #4, these particular test curves are encountered as follows:

Curve Number	Curve Name	Location MP		vature/ adius]	Super elevation	Posted Speed	12" UB Speed	Direction
662 (A&B)	Gap	51	4° 10′	[419 m]	5 1/2"	55 mph	77 mph	Left
663	Eby's	52 - 53	4° 12′	[416 m]	6"	55 mph	78 mph	Right
671	Ronks	60 - 61	2° 4′	[845 m]	6"	75 mph	112 mph	Right
672	Bird-in-Hand	61 - 62	2° 2′	[859 m]	6"	75 mph	112 mph	Left

Travelling East in the direction of Parkesburg on Track #1, the detailed test curves are encountered as follows:

Curve Number	Curve Name	Location MP	Curvature/ [Radius]	Super elevation	Posted Speed	12" UB Speed	Direction
672	Bird-in-Hand	62 - 61	2° 4′ [845 m]	5 3/4"	75 mph	111 mph	Right
671	Ronks	61 - 60	2° 1′ [866 m]	5 3/4"	75 mph	112 mph	Left
663	Eby's	53 - 52	4° 6′ [426 m]	5 1/2"	50 mph	78 mph	Left
662 (A&B)	Gap	51	4° 16′ [409 m]	5 1/2"	50 mph	77 mph	Right

3.4.2 200 Series Test Runs, New Brunswick to Metro Park, MP 31 - 21

The test zone, roughly between New Brunswick (MP 31) and Metro Park (MP 21) comprised 10 miles (16 km) of electrified quadruple track. The two center high speed tracks consisted of concrete mono-block ties with Pandrol rail fasteners. The majority of rail was CWR with a 140 RE profile. The interlockings (cross-overs) were on wooden ties with tieplates and cut spike rail fasteners. At approximate intervals of two miles, a 30 foot cut section (insulated joint) was welded into the track for signalling (cab signal) purposes. The track was well bedded in stone ballast. The maximum line speed in the zone was 125 mph.

There are 12 curves encountered within this test zone on each track as described in Appendix B. Three particular test curves were selected for more detailed computer analyses in two groups comprising one reversed pair and a singlet for each of the high speed Tracks # 2 and 3. Travelling East in the direction of Metro Park on Track #2, the particular test curves are encountered as follows:

Curve Number	Curve Name	Location MP	Curvature/ [Radius]	Super elevation	Posted Speed	12" UB Speed	Direction
268	1st Curve west of Lincoln	27 - 26	1° 52′ [934 m]	6*	80 mph	117 mph	Left
266	Curve west of MP 24	25 - 24	1° 33′ [1127 m]	5 3/4"	90 mph	128 mph	Left
265	Curve east of MP 24	24 - 23	1° 27′ [1204 m]	5 1/4"	90 mph	130 mph	Right

Travelling West in the direction of New Brunswick on Track #3, the detailed test curves are encountered as follows:

Curve Number	Curve Name	Location MP	Curvature/ [Radius]	Super elevation	Posted Speed	12" UB Speed	Direction
265	Curve east of MP 24	23 - 24	1° 26′ [1221 m]	6"	90 mph	134 mph	Left
266	Curve west of MP 24	24 - 25	1° 30′ [1164 m]	5 1/4"	90 mph	128 mph	Right
268	1st Curve west of Lincoln	26 - 27	1° 56′ [905 m]	6*	80 mph	115 mph	Right

3.4.3 300 Series Test Runs, Trenton to New Brunswick, MP 55 - 32

The test zone between Trenton (MP 55) and New Brunswick (MP 32) comprised 22 miles (35 km) of electrified quadruple track. The two center high speed tracks consisted of concrete mono-block ties with Pandrol rail fasteners. The majority of rail was CWR with a 140 RE profile. The interlockings (cross-overs) were on wooden ties with tieplates and cut spike rail fasteners. At approximate intervals of two miles, a 30 foot cut section (insulated joint) was welded into the track for signalling (cab signal) purposes. The track was well bedded in stone ballast. The maximum line speed was normally 125 mph but had been raised to 150 mph for the X2000 tests only.

Of the 6 curves within this test zone, two large radius curves were passed at the Eastern one-third of the test zone on each of the high speed Tracks # 2 and 3. Travelling East in the direction of New Brunswick on Track # 2, these higher radius curves are encountered as follows:

Curve Number	Location MP	Curvature/ [Radius]	Super elevation	Ord Speed	UB at 150 mph	Direction
276	41 - 39	0° 32′ [3274 m]	3 5/8"	125 mph	4.6"	Left
275	39	0° 19′ [5514 m]	2"	125 mph	2.9*	Right

Travelling West in the direction of Trenton on Track #3, the higher radius curves are encountered as follows:

Curve Number	Location MP	Curvature/ [Radius]	Super elevation	Ord Speed	UB at 150 mph	Direction
275	39	0° 20′ [5238 m]	2 1/8"	125 mph	3.0*	Right
276	39 - 41	0° 31′ [3379 m]	3 1/2"	125 mph	4.5*	Left

3.4.4 400 Series Test Runs, Washington, DC to New York Penn Station

The test zone between Washington and New York comprised 225 miles (362 km) of electrified double track, quadrupled where possible between Washington DC and Newark, New Jersey. The two high speed tracks consisted predominantly of concrete mono-block ties with Pandrol rail fasteners. The majority of rail was CWR with a 140 RE profile. All but a few interlockings (cross-overs) were on wooden ties with tieplates and cut spike rail fasteners. At approximate intervals of two miles, a 30 foot cut section (insulated joint) was welded into the track for signalling (cab signal) purposes. The track was well bedded in stone ballast. The maximum line speed was normally 125 mph but was often restricted to less due to Metroliner trains not allowed linespeeds for more than 4 inches of unbalance. The 150 mph test speed for the X2000 between Trenton and New Brunswick was not in force during the 400 Series long distance test runs. Turnouts (switches) and numerous curves of different radii and superelevation were encountered along the route. See Appendix B for a full curve and speed profile description.

Track data in space-curve form has been supplied by Amtrak for various portions of the test zones. These data will be described in more detail in the final analysis.

3.5 TEST SEQUENCE

The test sequence is described in the Test Event Log of Appendix A and is summarized in Table 3.3.

3.6 METHOD FOR DETERMINATION OF CANT DEFICIENCY/UNBALANCE

Unbalance has been calculated from the lateral acceleration signal generated by an accelerometer installed on the axle box lower damper bracket of axle (wheelset) number 2 of the locomotive. Location magnets were installed on the track at the entry and exit spirals of each test curve on which a detailed analysis was to be performed. These magnets were detected by the passing train and informed the onboard computer of the time each curve was entered and exited for each test run on a consistent basis. From such acceleration signals it has been possible to determine the duration of wheelset 2 in the full body of each test curve. The portion of the axle box lateral acceleration signal so identified was averaged in order to determine the mean track-plane lateral acceleration or cant deficiency of the train in the full body of each curve.

The effect of wheelset lateral displacement relative to the track causing a slight change in cant of the wheelset on the track (due to conical type wheel profiles) has been ignored. Where magnets did not identify curves, manual inspection of the signal was used to determine the duration of the full body of the curve.

The full body of any curve is judged to exist where the steady state values of both curvature and superelevation have been reached at two points in the curve between

which the sum of the fluctuations of the actual curvature and actual superelevation from their intended steady state values respectively tend to zero.

TABLE 3.3 X2000 TEST RUNS IN CHRONOLOGICAL ORDER

Date	Run #	Line	Direction/ Track	Track Condit	Scheduled Unbalance/Speed	Leading Car/ Axle
Nov 30/92	101	Ph - Hrsbg	W / Trk 4	Dry	3"	Cab Car / Axle 24
7	102	Hrsbg - Ph	E / Trk 1	Dry	5"	Locomotive / Axle 1
Ħ	103	Ph - Hrsbg	W / Trk 4	Dry	6"	Cab Car / Axle 24
7	104	Hrsbg - Ph	E / Trk 1	Dry	6"	Locomotive / Axle 1
	105	Ph - Hrsbg	W / Trk 4	Dry	7"	Cab Car / Axle 24
#	106	Hrsbg - Ph	E / Trk 1	Dry	7"	Locomotive / Axle 1
Dec 1/92	107	Ph - Hrsbg	W / Trk 4	Damp	7"	Cab Car / Axle 24
w	108	Hrsbg - Ph	E / Trk 1	Damp	7"	Locomotive / Axle 1
**	109	Ph - Hrsbg	W / Trk 4	Wet	8"	Cab Car / Axle 24
PT	110	Hrsbg - Ph	E / Trk 1	Wet	8*	Locomotive / Axle 1
Ħ	111	Ph - Hrsbg	W / Trk 4	Wet	9*	Cab Car / Axle 24
11	112	Hrsbg - Ph	E / Trk 1	Wet	9"	Locomotive / Axle 1
Ħ	113	Ph - Hrsbg	W / Trk 4	Wet	10"	Cab Car / Axle 24
#	114	Hrsbg - Ph	E / Trk 1	Wet	10"	Locomotive / Axle 1
Dec 2/92	115	Ph - Hrsbg	W / Trk 4	Dry	10"	Cab Car / Axle 24
19	116	Hrsbg - Ph	E / Trk 1	Dry	10"	Locomotive / Axle 1
•	117	Ph - Hrsbg	W / Trk 4	Dry	11"	Cab Car / Axle 24
	118	Hrsbg - Ph	E/Trk 1	Dry	11#	Locomotive / Axle 1
и	119	Ph - Hrsbg	W / Trk 4	Dry	12"	Cab Car / Axle 24
₩ .	120	Hrsbg - Ph	E / Trk 1	Dry	12"	Locomotive / Axle 1
Dec 3/92	121	Ph - Hrsbg	W / Trk 4	Dry	9"	Locomotive / Axle 1
w	122	Hrsbg - Ph	E / Trk 1	Dry	10"	Cab Car / Axle 24
77	123	Ph - Hrsbg	W / Trk 4	Dry	10"	Locomotive / Axle 1
**	124	Hrsbg - Ph	E / Trk 1	Dry	11"	Cab Car / Axle 24
*	125	Ph - Hrsbg	W / Trk 4	Dry	9*	Locomotive / Axle 1
#	126	Hrsbg - Ph	E / Trk 1	Dry	9"	Cab Car / Axle 24
	127	Ph - Hrsbg	W / Trk 4	Dry	12"	Locomotive / Axle 1

Date	Run #	Line	Direction/ Track	Track Condit	Scheduled Unbalance/Speed	Leading Car/ Axle
*	128	Hrsbg - Ph	E / Trk 1	Dry	12"	Cab Car / Axle 24
7	129	Ph - Hrsbg	W / Trk 4	Dry	9"	Locomotive / Axle 1
	130	Hrsbg - Ph	E / Trk 1	Dry	9"	Cab Car / Axle 24
Dec 7/92	300	Ph - NYP	E / Trk 3	Dry	130 mph	Cab Car / Axle 24
*	200	Ph - NYP	E/Trk3	Dry	5"	Cab Car / Axle 24
*	201	NYP - Ph	W / Trk 3	Dry	7"	Locomotive / Axle 1
н	202	Ph - NYP	E / Trk 3	Dry	9"	Cab Car / Axle 24
Ħ	203	NYP - Ph	W / Trk 3	Dry	10"	Locomotive / Axle 1
#	204	Ph - NYP	E / Trk 3	Dry	11"	Cab Car / Axle 24
77	205	NYP - Ph	W / Trk 3	Dry	12"	Locomotive / Axle 1
=	301_	NYP - Ph	W / Trk 3	Dry	140 mph	Locomotive / Axle 1
Dec 8/92	302	Ph - NYP	E / Trk 3	Dry	150 mph	Cab Car / Axle 24
	206	Ph - NYP	E/Trk3	Dry	9"	Cab Car / Axle 24
स	207	NYP - Ph	W / Trk 2	Dry	9".	Locomotive / Axle 1
**	208	Ph - NYP	E / Trk 2	Dry	10"	Cab Car / Axle 24
Ħ	209	NYP - Ph	W / Trk 2	Dry	11"	Locomotive / Axle 1
77	210	Ph - NYP	E / Trk 2	Dry	12"	Cab Car / Axle 24
*	211	NYP - Ph	W / Trk 3	Dry	at profile	Locomotive / Axle 1
*	303	NYP - Ph	W / Trk 3	Dry	150 mph	Locomotive / Axle 1
Dec 12/92	304	Ph - NYP	E / Trk 3	Wet	140 mph	Cab Car / Axle 24
•	305	NYP - Ph	W / Trk 3	Wet	150 mph	Locomotive / Axle 1
Dec 14/92	400	Wa - Ph	N / Trk 2	Dry	9*	Cab Car / Axle 24
	402	Ph - NYP	E / Trk 2	Dry	9*	Cab Car / Axle 24
W	401	NYP - Ph	W / Trk 3	Dry	9"	Locomotive / Axle 1
"	403	Ph - Wa	S / Trk 3	Dry	9"	Locomotive / Axle 1
Dec 15/92	404	Wa - Ph	N / Trk 2	Dry	9" + 5 mph	Cab Car / Axle 24
	406	Ph - NYP	E / Trk 1,2	Dry	9" + 5 mph	Cab Car / Axle 24
я	405	NYP - Ph	W / Trk 3	Dry	9" + 5 mph	Locomotive / Axle 1
	410	Ph - Tren	E / Trk 2	Dry	9" + 5 mph	Cab Car / Axle 24
77	411	Tren - Ph	W / Trk 3,4	Dry	9" + 5 mph	Locomotive / Axle 1
π	407	Ph - Wa	\$ / Trk 3	Dry	9" + 5 mph	Locomotive / Axle 1

4. RESULTS

Preliminary test results are presented herein to examine the safety aspects and the safety margin involved with the high cant deficiency operation of the X2000 train. During each test run, measured peak values of the safety parameters were compiled on a mile by mile basis. A summary of the peak values, closest to the safety limits, recorded over all the cant deficiency and high speed test runs and over all test zones is given in Table 4.1. Each safety parameter will be addressed in turn in this section.

4.1 MAXIMUM UNBALANCE RECORDED

The lateral accelerometer installed on Axle #2 of the locomotive was used to indicate the degree of unbalance or cant deficiency. The maximum quasi-steady lateral acceleration recorded from all test runs was 2.07 m/s². This occurred during Test Run 128 on the Philadelphia - Harrisburg line while travelling east on Track #1 in curve 662 (Gap, 4° curvature) at a speed of 78 mph. This lateral acceleration translates to an unbalance or cant deficiency of 12.5 inches.

4.2 MINIMUM VERTICAL WHEEL-RAIL FORCE (VEHICLE OVERTURN), Vmin

A composite plot of the minimum vertical wheel force peaks measured from each test run and over all test zones on both the Philadelphia - Harrisburg and NEC mainlines is shown in Figure 4.1. It should be noted in this plot that individual wheels are not distinguished; these peak values were drawn from each test run at any location within the test zone (not necessarily in a curve) and may be for any wheel (of the 8 instrumented wheels). In addition, the peak values are plotted against the intended or scheduled test run cant deficiency (not necessarily the actual cant deficiency when the peak was recorded) and no trend line should be drawn from this composite.

During these test runs, cant deficiencies up to 12.5 inches and speeds up to 154 mph were achieved. The results indicate that no measured wheel approached the minimum allowable unloading at any time throughout the tests. From the lowest values recorded, a safety margin of about 14% from the allowable limit is apparent for cant deficiencies up to 12.5 inches on representative track. No appreciable crosswinds were encountered during these test runs.

A more detailed examination of the minimum vertical wheel force is given as an example in Figure 4.2. Peak values on the left wheel of trailing axle 1 (locomotive) measured in test curve 671 (Ronks, 2° curvature) of the Philadelphia - Harrisburg Line, westbound on track #4, are plotted as a function of the quasi-steady cant deficiency measured in the circular portion of the curve. This plot includes the lowest vertical wheel force ever measured throughout the tests runs, and also includes values measured under both wet and dry track conditions. Extrapolation of these results indicate that the safety limit would be reached at a cant deficiency of about 15 inches for similar conditions.

TABLE 4.1 PEAK VALUES MEASURED FROM ALL TEST ZONES, HARRISBURG and NEC LINES

Safety Criteria	Messured Value	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Intended Cant Def	Intended Measured Cent Def Cent Def	Measured Speed	Leeding Axle	Comments
Min Vertical Wheel Force	23 KN	83%	Left Wheel Axle 1 (Loco)	101 Hrsbg	West Track 4	51 - 52	Dry	3"	3.1"	57 mph	Axle 24 (Cab)	Axle 24 In curve 662 (Gap - 4°) (Cab)
V min	20 KN	86%	Left Wheel Axle 1 (Loco)	113 Hrsbg	West Track 4	60 - 61	Wet	10*	11"	108 mph		Axle 24 In curve 671 (Ronks - 2°) (Cab)
	22 KN	84%	Left Wheel Axle 1 (Loco)	119 Hrsbg	West, Track 4	60 - 61	ρίλ	12"	11.7"	111 mph	Axle 24 (Cab)	Axle 24 In curve 671 (Ronks - 2°) (Cab)
	23 kN	83%	Left Wheel Axle 1 (Loco)	204 NEC	East Track 3	25 - 24	Dry	11"	12.4"	125 mph	Axle 24 (Cab)	Axle 24 In curve 266 (1.5°) (Cab)
Max Net Axle Lateral	66 kN	84%	Axle 24 (Cab)	113 Hrsbg	West Track 4	51 - 52	Wet	10"	11"	77 mph	Axle 24 (Cab)	Axle 24 In curve 662 (Gap - 4°) (Cab)
Force NAL	68 KN	87%	Axle 24 (Cab)	114 Hrsbg	East Track 1	62 - 61	Wet	10"	10"	106 mph	Axle 1 (Loco)	In curve 672 (Bd Hnd - 2º)
	-66 kN	85%	Axle 24 (Cab)	120 Hrsbg	East Track 1	53 - 52	Dry	12"	12.1"	80 mph	Axte 1 (Loco)	In Curve 663 (EBYs - 4°)
	63 KN	70%	Axle 1 (Loco)	204 NEC	East Track 3	25 - 24	Dry	11"	12.4"	125 mph	Axle 24 (Cab)	Axle 24 In curve 266 (1.5°) (Cab)
Max Wheel	0.61	76%	Left Wheel Axle 1 (Loco)	120 Hrsbg	East Track 1	53 - 52	Dry	12"	12.1"	80 mph	Axle 1 (Loco)	In Curve 663 (EBYs - 4°)
}	0.60	75%	Left Wheel Axie 24 (Cab)	122 Hrsbg	East Track 1	53 - 52	Dry	10"	9.8.	75 mph	Axle 24 (Cab)	(Cab)
	0.60	75%	Left Wheel Axle 24 (Cab)	128 Hrsbg	East Track 1	53 - 52	Dry	12"	10.9"	78 mph	Axle 24 (Cab)	In Curve 663 (EBYs - 4°)
	0.56	%02	Right Wheel Axle 1 (Loco)	205 NEC	West Track 3	23 - 24	h Dry	12"	8.8"	125 mph	Axle 1 (Loco)	In curve 265 (1.5°)

Safety Criteria	Measured % of Value Limit	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Intended Cant Def	Run No/ Direct/ Track Track Intended Measured Measured Line Track Milepost Condit Cant Def Cant Def Speed	Run No/ Direct/ Track Track Intended Measured Measured Leading Line Track Milepost Condit Cant Def Cant Def Speed Axle	Leading Axle	Comments
Max Truck Side L/V	0.44	88%	Left Side Truck 12 (Cab)		West Track 4	113 West 61 - 62 Hrsbg Track 4	Wet	10"	10.1"	108 mph	Axle 24 (Cab)	108 mph Axle 24 in curve 672 (Bd Hnd - 2°) . (Cab)
 }	0.46	92%	Left Side Truck 12 (Cab)	122 Hrsbg	East Track 1	East 53 - 52 Track 1	Dry	10"	9.8.	75 mph	Axle 24 (Cab)	75 mph Axle 24 In Curve 663 (EBYs - 4º) (Cab)
	0.45	90%	Left Side Truck 12 (Cab)	126 East Hrsbg Track 1		53 - 52	Dry	.6	9.2"	72 mph	Axle 24 (Cab)	72 mph Axle 24 In Curve 663 (EBYs - 4º) (Cab)
	0.45	%06	Left Side Truck 12 (Cab)	128 Hrsbg	East Track 1	East 53 - 52 Track 1	Dry	12"	10.9"	78 mph	Axle 24 (Cab)	10.9" 78 mph Axle 24 In Curve 663 (EBYs - 4º) (Cab)

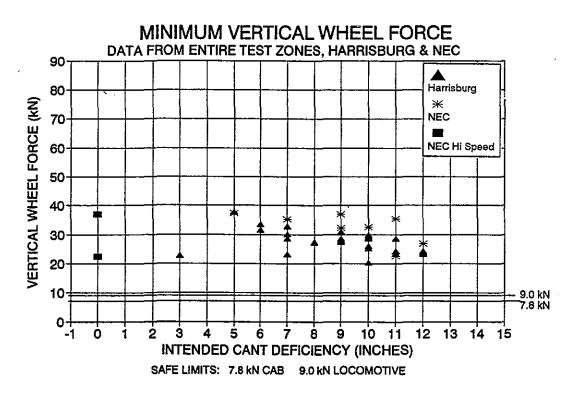


Figure 4.1: Minimum Vertical Wheel Forces Measured During X2000 Test Runs

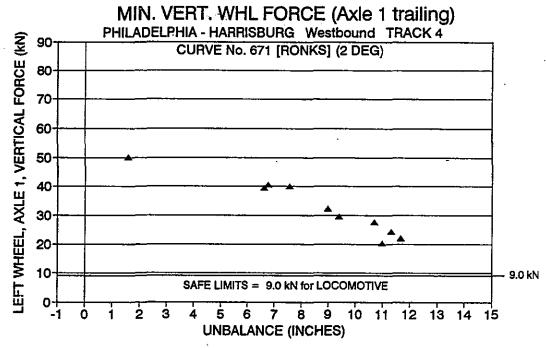


Figure 4.2: Minimum Vertical Wheel Force, Measured In Curve 671, Westbound

4.3 NET AXLE LATERAL FORCE (TRACK PANEL SHIFT), NAL

A composite plot of the peak net axle lateral forces measured for the locomotive (axles #1 and #2) from each test run and over all test zones is given in Figure 4.3a. A similar plot for the cab car axles (axle #23 and #24) is given in Figure 4.3b.

It is evident that the net lateral forces measured for the locomotive axles were significantly lower than the allowable safety limit of 90 kN, with a substantial margin of safety. For the axles of the lighter weight cab car, similar forces were observed although the allowable safety limit is less (78 kN). A margin of safety of about 15% is evident in this case.

A more detailed examination of the net lateral force for axle #24 (cab car) is given in Figure 4.4. Peak values measured in test curve 671 (Bird-in-Hand, 2° curvature) of the Philadelphia - Harrisburg line, westbound on track #4, are plotted as a function of the quasi-steady cant deficiency measured in the circular portion of the curve. This plot includes one of the highest forces measured throughout the tests runs during test run #113 under damp rail conditions. Extrapolation of these results indicate that the safety limit would be reached at a cant deficiency of about 14 inches for similar conditions.

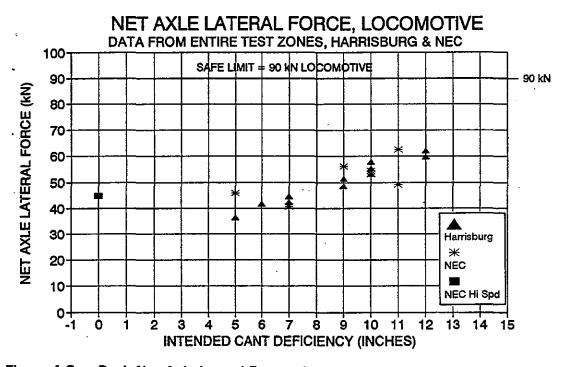


Figure 4.3a: Peak Net Axle Lateral Forces, Locomotive (Composite of Test Runs)

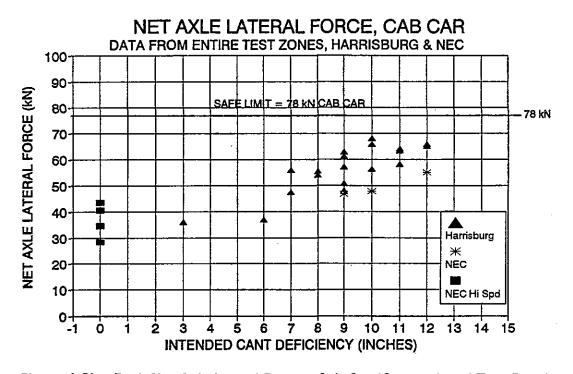


Figure 4.3b: Peak Net Axle Lateral Forces, Cab Car (Composite of Test Runs)

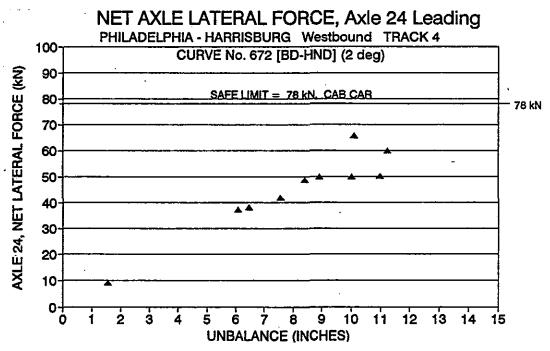


Figure 4.4: Peak Net Axle Lateral Force, Axle 24, In Curve 672, Track 4

4.4 L/V DERAILMENT QUOTIENT (WHEEL CLIMB), L/V

A composite plot of the maximum wheel L/V ratios measured from each test run and over all test zones is shown in Figure 4.5. It should again be noted that individual wheels are not distinguished in this plot; these peak values were drawn from each test run and may be for any wheel (of the 8 instrumented wheels). In addition, the peak values are plotted as a function of the intended test run cant deficiency (not measured cant deficiency when the peak occurred) and no trends should be drawn.

The highest wheel L/V ratios measured during the cant deficiency and high speed runs were about 0.6, approximately 75% of the allowable (Nadal) single wheel limit of 0.8. As a result, the axle sum L/V ratio (Weinstock) was not examined. A safety margin of about 25% is apparent for cant deficiencies up to 12.5 inches for similar track and vehicle conditions.

A more detailed examination of a single wheel L/V ratio is given in Figure 4.6 for the left wheel of axle #1 (locomotive). Peak values measured in test curve 663 (Eby's, 4° curvature) of the Philadelphia - Harrisburg line, eastbound on track #1, in which axle #1 was the leading axle, are plotted as a function of the quasi-steady cant deficiency measured in the circular portion of the curve. This plot includes two of the highest wheel L/V values measured throughout the tests runs, with cant deficiencies up to 12 inches. For similar conditions, extrapolation of these results indicate that the safety limit would be reached well above a cant deficiency of 15 inches.

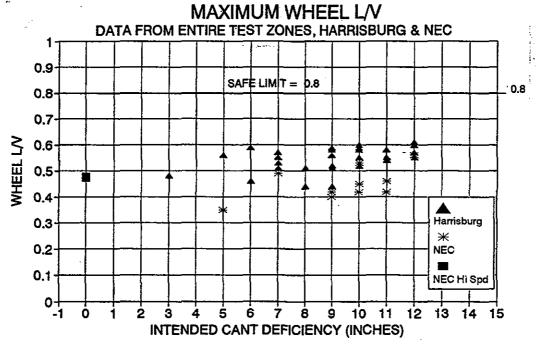


Figure 4.5: Peak Maximum Wheel L/V Ratios (Composite, All Wheels, Test Runs)

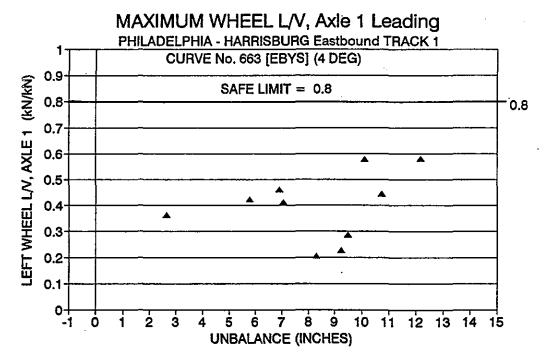


Figure 4.6: Peak Maximum Wheel L/V Ratios, Left Wheel, Axle 1, Curve 663

4.5 TRUCK-SIDE L/V RATIO (RAIL ROLL-OVER), T-L/V

A composite of the maximum truck side L/V ratios, which includes both left and right sides for truck #1 (locomotive) and truck #12 (cab car), measured from each test run and over all test zones, is given in Figure 4.7. No peak values were measured that exceeded the allowable limit of 0.5. At cant deficiencies above 9 inches, some peak values of truck side L/V were observed around 90% of the allowable limit during test runs on the Philadelphia - Harrisburg line.

A more detailed examination of the truck side L/V ratio is given in Figure 4.8. Peak values on the left side of truck #12 (cab car) measured in test curve 672 (Bird-inHand, 2° curvature) of the Philadelphia - Harrisburg Line, westbound on track #4, are plotted as a function of the quasi-steady cant deficiency measured in the circular portion of the curve. This plot includes one of the highest truck side L/V ratios measured throughout the tests runs, and also includes values measured under both wet and dry track conditions. A margin of safety of about 10% is apparent for cant deficiencies up to 12 inches for similar track and vehicle conditions.

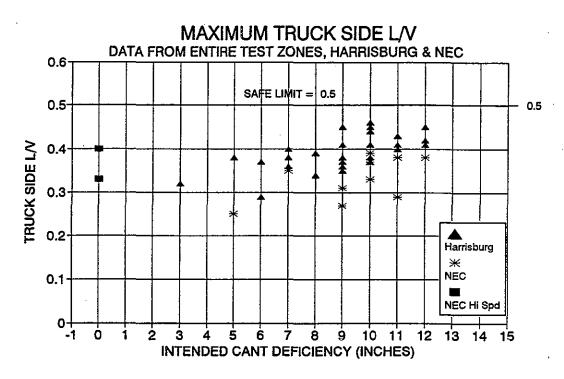


Figure 4.7: Peak Maximum Truck Side L/V Ratios (Composite of Test Runs)

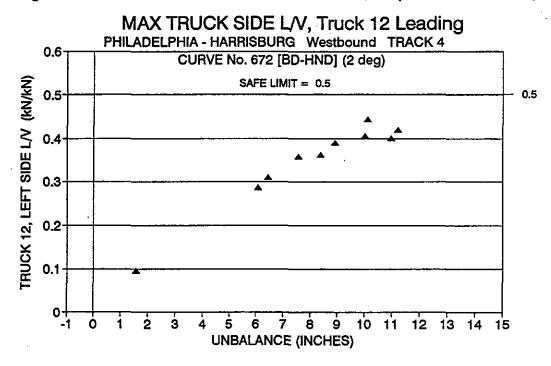


Figure 4.8: Peak Maximum Truck Side L/V Ratios, Truck 12 (Cab) in Curve 672

4.6 FIELD OBSERVATIONS OF TRACK PANEL AND TIE-PLATE SHIFT

Track panel shift and rail movement were monitored during high cant deficiency test runs by surveying from lineside structures. No permanent deformation of track or rail was registered during any of the trials on both wooden ties with cut spikes and tie plates or concrete monoblock ties with pandrol fasteners.

4.7 MAXIMUM SPEED RECORDED

The maximum speed recorded from the high speed test runs was 154 mph. This occurred during Test Run 305 on the NEC Philadelphia - New York Penn line while travelling west on Track #3 at MP 51 near Trenton. This was a scheduled 150 mph run under wet track conditions, in which a 150 mph or greater speed was sustained for over 8 miles. A speed of 152 mph was also recorded at the same location under dry track conditions during Test Run 303.

4.8 TRUCK FRAME ACCELERATION, TA

The truck frame lateral accelerations of truck #1 (locomotive), truck #5 (coach car), and truck #12 (cab car) were monitored throughout the trial period. No evidence of truck instability (hunting) was observed in any test run, including high speed test runs at speeds up to 152 mph in tangent track under dry track conditions.

4.9 SIMULATED REVENUE EARNING SERVICE RUNS

After a data review of the cant deficiency and high speed test runs, a speed profile was prepared by Amtrak for a simulated revenue service round trip from Washington to New York Penn Station. This speed profile was based on a maximum cant deficiency of 9 inches, and accounted for actual allowable speeds dependent on signal spacings and other local restrictions.

Using this speed profile, a simulated revenue service round trip was made with full instrumentation. For data recording, the trip was segmented into 4 test zones (runs):

- 1) Washington Philadelphia, northbound, principally on track 2
- 2) Philadelphia New York Penn, eastbound, principally on track 2
- 3) New York Penn Philadelphia, westbound, principally on track 3
- 4) Philadelphia Washington, southbound, principally on track 3

On a mile-by-mile basis, the peak values of each safety parameter were recorded in each test zone. A composite plot of the four highest recorded values of each safety parameter in each test zone is shown in Figures 4.9 - 4.12 as a function of vehicle speed. More detailed information on the location and conditions for these peak values are given in Table 4.2.

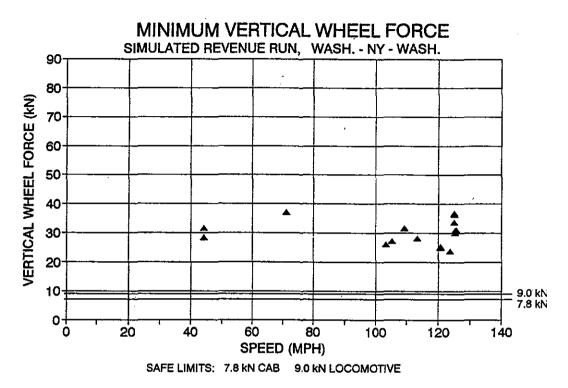


Figure 4.9: Minimum Vertical Wheel Forces, Simulated Revenue Service Run

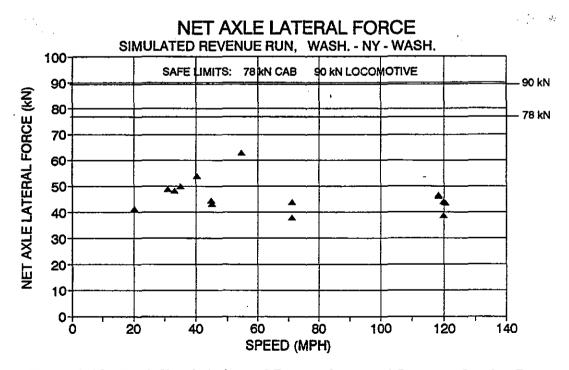


Figure 4.10: Peak Net Axle Lateral Forces, Simulated Revenue Service Run

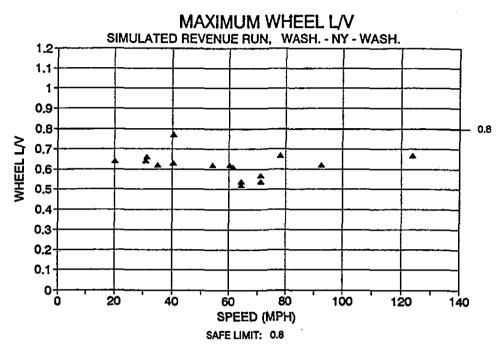


Figure 4.11: Maximum Wheel L/V Ratios, Simulated Revenue Service Run

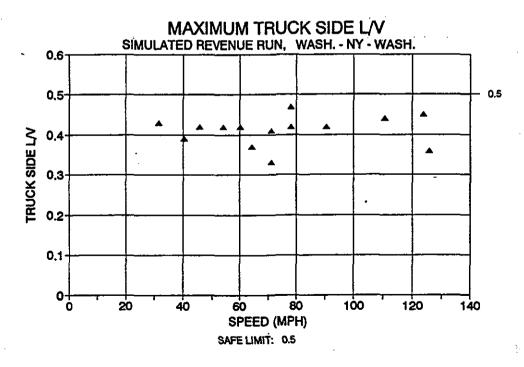


Figure 4.12: Maximum Truck Side L/V Ratios, Simulated Revenue Service Run

TABLE 4.2 PEAK VALUES, SIMULATED REVENUE RUN, NEC, WASHINGTON - NEW YORK R/t

A) MINIMUM VERTICAL WHEEL FORCE, Vmin

Comments	Tangent track												
Leading	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)
Measured	Speed 125 mph	126 mph	105 mph	126 mph	125 mph	125 mph	44 mph	44 mph	103 mph	124 mph	121 mph	121 ուքի	114 mph
Measured	180 NBO												
Track	Dry	Dry	Dry	Dry	Drγ	Dry	Dry	Dry	Dry	Dry	Dry	Dry	Dry
Track	76 - 75	63 - 62	59 - 58	39 - 38	66 - 65	66 - 65	22 - 23	22 - 23	57 - 58	35 - 36	55 - 56	55 - 56	62 - 63
Direct/	North Track 2	North Track 1	North Track 2	North Track 2	East Track 2	East Track 2	West Track 3	West Track 3	West Track 3	South Track 3	South Track 3	South Track 3	South Track 4
Run No/	400 Wa-Ph	400 Wa-Ph	400 Wa-Ph	400 Wa-Ph	402 Ph-NYP	402 Ph-NYP	401 NYP-Ph	401 NYP-Ph	401' NYP-Ph	403 Ph-Wa	403 Ph-Wa	403 Ph-Wa	403 Ph-Wa
Vehicle Element	Right Wheel Axle 1 (Loco)	Left Wheel Axle 1 (Loco)	Left Wheel Axle 23 (Cab)	Left Wheel Axte 1 (Loco)	Right Wheel Axle 1 (Loco)	Left Wheel Axle 2 (Loco)	Left Wheel Axle 1 (Loco)	Left Wheel Axle 2 (Loco)	Left Wheel Axle 24 (Cab)	Right Wheel Axle 24 (Cab)	Right Wheel	Right Wheel Axle 2 (Loco)	Left Wheel Axle 23 (Cab)
% of	74%	73%	72%	73%	%99	%99	76%	72%	74%	77%	%08	%08	%92
Measured	30 kN	31 kN	27 kN	31 kN	37 KN	36 KN	28 kN	32 kN	26 kN	24 kN	25 kN	25 kN	28 kN

TABLE 4.2 PEAK VALUES, SIMULATED REVENUE RUN, NEC, WASHINGTON - NEW YORK R/t

B) MAXIMUM NET AXLE LATERAL FORCE, NAL

·													
Comments								2000					
Leading Axle	Axle 1 (Loco)	Axle 1 (Loco)	Axfe 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axte 1 (Loco)	Axfe 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axte 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)
Measured Speed	55 mph	33 mph	35 mph	120 mph	120 mph	45 mph	118 mph	118 mph	40 mph	120 mph	45 mph	20 mph	31 mph
Measured Cant Def													
Track Condit	Dry												
Track Milepost	86 - 66	98 - 97	27 - 26	75 - 74	75 - 74	7 - 8	74 - 75	74 - 75	87 - 88	50 - 51	94 - 95	96 - 96	96 - 97
Direct/ Track	North Track 2	North Track 2	North Track 2	East Track 2	East Track 2	West Track 3	West Track 3	West Track 3	West Track 4	South Track 3	South Track 3	South Track 3	South Track 3
Run No/ Line	400 Wa-Ph	400 Wa-Ph	400 Wa-Ph	402 Ph-NYP	402 Ph-NYP	401 NYP-Ph	401 NYP-Ph	401 NYP-Ph	401 NYP-Ph	403 Ph-Wa	403 Ph-Wa	403 Ph-Wa	403 Ph-Wa
Vehicle Element	Axle 1 (Loco)	Axie 24 (Cab)	Axle 24 (Cab)	Axle 1 (Loco)	Axle 23 (Cab)	Axle 1 (Loco)	Axle 2 (Loco)	Axle 24 (Cab)	Axle 1 (Loco)	Axle 24 (Cab)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)
% of Limit	20%	62%	64%	49%	50%	49%	52%	29%	60%	60%	48%	46%	54%
Measured Value	63 kN	48 KN	50 kN	44 KN	39 kN	45 KN	47 kN	46 kN	54 kN	47 kN	43 KN	41 kN	49 kN

TABLE 4.2 PEAK VALUES, SIMULATED REVENUE RUN, NEC, WASHINGTON - NEW YORK R/t

C) MAXIMUM WHEEL L/V RATIO, L/V

TABLE 4.2 PEAK VALUES, SIMULATED REVENUE RUN, NEC, WASHINGTON - NEW YORK R/t

D) MAXIMUM TRUCK SIDE L/V RATIO, T-L/V

Comments													
Leading Axfe	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axfe 24 (Cab)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axte 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)
Measured Speed	46 mph	60 mph	91 mph	64 mph	71 mph	78 mph	78 mph	40 mph	40 mph	124 mph	32 mph	54 mph	111 mph
Measured Cant Def													
Track Condit	Dry	Dry	Dry	Dry	Dry	Dry	Dry						
Track Milepost	95 - 94	94 - 93	13 - 12	86 - 85	82 - 81	10 - 11	10 - 11	87 - 88	87 - 88	35 - 36	97 - 98	98 - 99	128 - 129
Direct/ Track	North Track 2	North Track 2	North Track 1	East Track 2	East Track 2	West Track 3	West Track 3	West Track 4	West Track 4	South Track 3	South Track 3	South Track 3	South Track 3
Run No/ Line	400 Wa-Ph	400 Wa-Ph	400 Wa-Ph	402 Ph-NYP	402 Ph-NYP	401 NYP-Ph	401 NYP-Ph	401 NYP-Ph	401 NYP-Ph	403 ['] Ph-Wa	403 Ph-Wa	403 Ph-Wa	403 Ph-Wa
Vehicle Element	Left Side Truck 12 (Cab)	Left Side Truck 1 (Loco)	Right Side Truck 1 (Loco)	Left Side Truck 1 (Loco)	Right Side Truck 1 (Loco)	Left Side Truck 1 (Loco)							
% of Limit	84%	84%	84%	74%	82%	84%	94%	78%	78%	90%	%98	84%	88%
Measured Value	0.42	0.42	0.42	0.37	0.41	0.42	0.47	0.39	0.39	0.45	0.43	0.42	0.44

A maximum top speed of 125 mph was attained during the simulated revenue service round trip, and no transgressions of any safety limits were observed.

A second simulated revenue service round trip was made between Washington and New York Penn Station. In this case, the trip was made at speeds 5 mph above the 9 inch cant deficiency baseline speeds, except where other restrictions were applied. A composite plot of the four highest recorded values of each safety parameter in each test zone is shown in Figures 4.13 - 4.16 as a function of vehicle speed. More detailed information on the location and conditions for these peak values is given in Table 4.3.

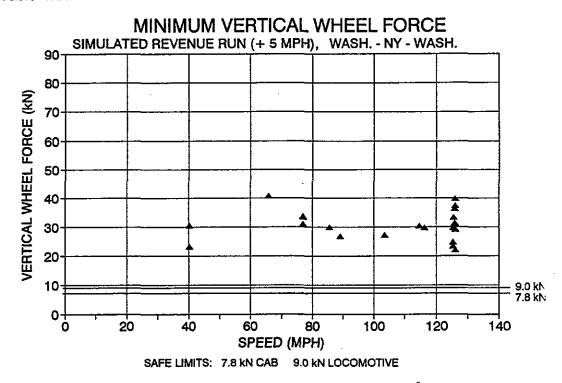


Figure 4.13: Minimum Vertical Wheel Forces, Simulated Revenue Run + 5mph

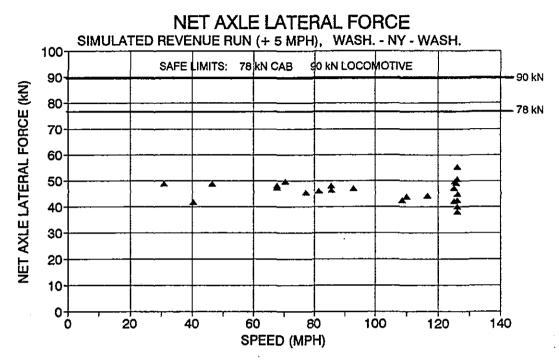


Figure 4.14: Peak Net Axle Lateral Forces, Simulated Revenue Run + 5mph

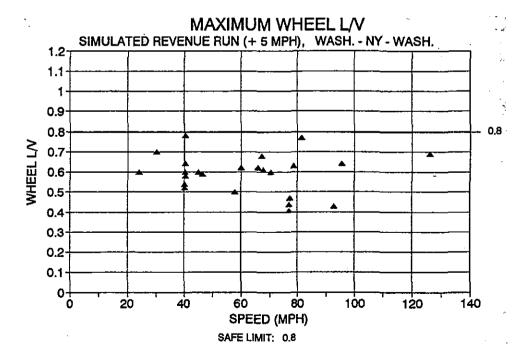


Figure 4.15: Maximum Wheel L/V Ratios, Simulated Revenue Run + 5mph

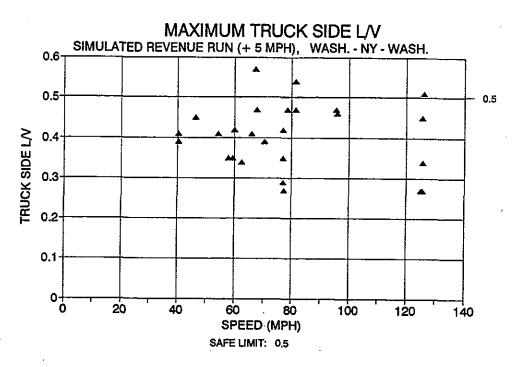


Figure 4.16: Maximum Truck Side L/V Ratios, Simulated Revenue Run + 5 mph

For this second higher speed round trip, no transgressions of any safety limits were observed during any of the transits of approximately 400 different curves at or below the intended +5 mph speed profile. Of the total of 448 miles of track tested, only three transgressions of the locomotive truck-side L/V limit of 0.5 were registered:

- 0.57 at 60 mph, 1 mile south of 30th Street Station in Philadelphia, past a turnout at the end of a curved section (curve 305) adjacent to a bridge
- 0.54 at 81.5 mph, done deliberately at 6.5 mph above the simulated engineer 5 mph excess-speed profile for a section of 1° (1746m radius) curve with four switches in the curve at Hunter interlocking
- 0.51 at 126 mph, on tangent track while transiting a switch for the Harmony Industrial Track, south of Stanton

No transgression of any other safety limit was recorded.

It should be noted that the force ratio required to roll over a rail on tangent track, even if worn, is likely to be closer to 0.6 (new rail limit) than the 0.5 limit used in trials for worn curve rail. Any rail bolted to a nearby switch crossing will probably tolerate force ratios in excess of 0.6 without rolling over.

TABLE 4.3 PEAK VALUES, SIMULATED REVENUE RUN (+5 mph), NEC, WASHINGTON - NEW YORK R/t

A) MINIMUM VERTICAL WHEEL FORCE, Vmin

ehic	Vehicle Element	Ē	Direct/	Track	Track		- P	Leading	Comments
-∦	4	ō 4 i	North	75 - 74	Dry	Cant Der	Speed 126 mph	Axie 24	
Left Wheel 404 Axle 1 (Loco) Wa-Ph	407 Wa-F	ء ۾ ا	North Track 1	62 - 61	Dry	6.0	126 mph	Axle 24 (Cab)	
	404 Wa-P	ے ا	North Track 2	50 - 49	Dry	9.0	125 mph	Axle 24 (Cab)	
Left Wheel 404 Axle 1 (Loco) Wa-Ph	404 Wa-P	ے	North Track 2	29 - 28	Dη	4.8"	89 mph	Axle 24 (Cab)	
Left Wheel 406 Axle 2 (Loco) Ph-NYP	406 Ph-NY	۵	East Track 1	88 - 87	Drγ	1.2"	40 mph	Axle 24 (Cab)	
Left Wheel 406 Axte 24 (Cab) Ph-NYP	406 Ph-NY	۵	East Track 1	88 - 87	Dry	1.2"	40 mph	Axle 24 (Cab)	
Left Wheel 406 Axle 1 (Cab) Ph-NYP	406 Ph-NYF		East Track 1	71 - 70	Dry	3.0"	104 mph	Axle 24 (Cab)	
Left Wheel 406 Axle 2 (Loco) Ph-NYP	406 Ph-NYF		East Track 2	11 - 10	Dry	0.0"	86 mph	Axte 24 (Cab)	
Right Wheel 405 Axle 24 (Cab) NYP-Ph	405 NYP-P	_	West Track 3	24 - 25	Dry	10.8"	115 mph	Axte 1 (Loco)	
Left Wheel 405 Axle 24 (Cab) NYP-Ph	405 NYP-P		West Track 3	25 - 26	Dry	6.0"	116 mph	Axle 1 (Loco)	
Left Wheel 405 Axle 23 (Cab) NYP-Ph	405 NYP-F	ř	West Track 3	32 - 33	Dry	0.0"	126 mph	Axfe 1 (Loco)	
Right Wheel 405 Axle 2 (Loco) NYP-Ph	405 NYP-F	ج	West Track 3	74 - 75	ρι	10.8"	126 mph	Axfe 1 (Loco)	

Measured Value	% of Limit	Vehicle Element	Run Nof Line	Direct/ Track	Track Milepost	Track Condit	Measured Cant Def	Measured Leading Speed Axle	Leading Axle	Comments
29 kN	%02	Left Wheel Axle 24 (Cab)	407 Ph-Wa	South Track 3	35 - 36	Dry	.0.0	126 mph	Axle 1 (Loco)	
22 kN	80%	Right Wheel Axle 24 (Cab)	407 Ph-Wa	South Track 3	35 - 36	Dry	0.0"	126 mph	Axle 1 (Loco)	
23 kN	82%	Right Wheel Axle 2 (Loco)	407 Ph-Wa	South Track 3	55 - 56	Dry	0.0"	126 mph	Axle 1 (Loco)	
25 kN	76%	Right Wheel Axle 24 (Cab)	407 Ph-Wa	South Track 3	55 - 56	Drγ	0.0*	126 mph	Axfe 1 (Loco)	
33 KN	70%	Right Wheel Axle 1 (Loco)	410 Ph-Tre	East Track 2	82 - 81	Dry	6.0"	77 mph	Axle 24 (Cab)	
31 KN	73%	Right Wheel Axle 2 (Loco)	410 Ph-Tre	East Track 2	82 - 81	Dry	6.0"	77 mph	Axte 24 (Cab)	
34 kN	63%	Right Wheel Axle 24 (Cab)	410 Ph-Tre	East Track 2	82 - 81	Dry	6.0"	77 mph	Axte 24 (Cab)	
33 KN	%02	Left Wheel Axle 2 (Loco)	410 Ph-Tre	East Track 2	66 - 65	Dry	4.8"	126 mph	Axle 24 (Cab)	
36 kN	29%	Left Wheel Axle 24 (Cab)	411 Tre-Ph	West Track 3	99 - 99	Dry	3.6"	126 mph	Axle 1 (Loco)	
40 kN	62%	Left Wheel Axle 2 (Loco)	411 Tre-Ph	West Track 3	70 - 71	Dry	9.0"	126 mph	Axle 1 (Loco)	
37 kN	28%	Left Wheel Axfe 24 (Cab)	411 Tre-Ph	West Track 3	70 - 71	Dry	9.0"	126 mph	Axle 1 (Loco)	
41 kN	61%	Right Wheel Axte 1 (Loco)	411 Tre-Ph	West Track 3	85 - 86	Dry	0.0"	66 mph	Axle 1 (Loco)	

TABLE 4.3 PEAK VALUES, SIMULATED REVENUE RUN (+5 mph), NEC, WASHINGTON - NEW YORK R/t

B) MAXIMUM NET AXLE LATERAL FORCE, NAL

								-				
Comments												
Leading Axle	Axle 24 (Cab)	Axle 1 (Loco)	Axle 1 (Loco)	Axte 1 (Loco)	Axle 1 (Loco)							
Measured Speed	46 mph	68 mph	68 mph	125 mph	109 mph	117 mph	86 mph	86 mph	82 mph	126 mph	126 mph	70 mph
Measured Cant Def	0.0"	4.2"	4.2"	9.0"	9.0"	10.8"	0.0"	.0.0	3.0"	10.8"	10.8"	9.0
Track Condit	Dry	Dιγ	Dry	Dry	Drγ	Dry	Dry	Dry	Drγ	Dry	Dry	ριλ
Track Milepost	94 -93	93 - 92	93 - 92	50 - 49	27 - 26	25 - 24	11 - 10	11 - 10	10 - 11	74 - 75	74 - 75	81 - 82
Direct/ Track	North Track 2	North Track 2	North Track 2	North Track 2	East Track 2	East Track 2	East Track 2	East Track 2	West Track 3	West Track 3	West Track 3	West Track 3
Run No/ Line	404 Wa-Ph	404 Wa-Ph	404 Wa-Ph	404 Wa-Ph	406 Ph-NYP	406 Ph-NYP	406 Ph-NYP	406 Ph-NYP	405 NYP-Ph	405 NYP-Ph	405 NYP-Ph	405 NYP-Ph
Vehicle Element	Left Wheel Net Axle 24 (Cab)	Left Wheel Net Axfe 1 (Loco)	Left Wheel Net Axle 24 (Cab)	Left Wheel Net Axle 24 (Cab)	Left Wheel Net Axle 1 (Loco)	Left Wheel Net Axle 1 (Loco)	Left Wheel Net Axle 1 (Loco)	Left Wheel Net Axle 24 (Cab)	Left Wheel Net Axle 1 (Loco)	Left Wheel Net Axle 2 (Loco)	Left Wheel Net Axle 24 (Cab)	Left Wheel Net Axle 24 (Cab)
% of Limit	63%	53%	62%	64%	48%	49%	23%	%69	51%	61%	%59	64%
Measured Value	49 kN	48 kN	48 kN	50 KN	43 kN	44 kN	48 kN	46 kN	46 kN	55 kN	51 kN	50 kN

Measured Value	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Measured Cant Def	Measured Speed	Leading Axle	Comments
44 kN	49%	Left Wheel Net Axle 2 (Loco)	407 Ph-Wa	South Track 3	23 - 24	Dry	8.4"	110 mph	Axle 1 (Loco)	
49 kN	63%	Left Wheel Net Axle 24 (Cab)	407 Ph-Wa	South Track 3	50 - 51	Drγ	11.4"	126 mph	Axle 1 (Loco)	
43 kN	48%	Left Wheel Net Axle 1 (Loco)	407 Ph-Wa	South Track 3	75 - 76	Dιγ	0.0"	126 mph	Axle 1 (Loco)	
49 kN	54%	Left Wheel Net Axle 1 (Loco)	407 Ph-Wa	South Track 3	97 - 96	Dry		31 mph	Axle 1 (Loco)	
46 kN	59%	Left Wheel Net Axle 24 (Cab)	410 Ph-Tre	East Track 2	82 - 81	Dry	6.0"	77 mph	Axle 24 (Cab)	
47 kN	52%	Left Wheel Net Axle 1 (Loco)	410 Ph-Tre	East Track 2	81 - 80	Dry	6.0"	93 mph	Axle 24 (Cab)	
47 kN	52%	Left Wheel Net Axle 1 (Loco)	410 Ph-Tre	East Track 2	75 - 74	Dry	11.4"	125 mph	Axle 24 (Cab)	
42 kN	54%	Left Wheel Net Axle 23 (Cab)	410 Ph-Tre	East Track 2	75 - 74	Dry	11.4"	125 mph	Axle 24 (Cab)	
38 kN	42%	Left Wheel Net Axle 1 (Loco)	411 Tre-Ph	West Track 3	70 - 71	Dry	9.0.	126 mph	Axle 1 (Loco)	
45 kN	20%	Left Wheel Net Axle 2 (Loco)	411 Tre-Ph	West Track 3	70 - 71	Dry	9.0"	126 mph	Axle 1 (Loco)	
40 kN	51%	Left Wheel Net Axle 24 (Cab)	411 Tre-Ph	West Track 3	70 - 71	Dry	9.0"	126 mph	Axle 1 (Loco)	
42 kN	47%	Left Wheel Net Axle 1 (Loco)	411 Tre-Ph	West Trck 3,4	87 - 88	Dry	0.0"	40 mph	Axle 1 (Loco)	

TABLE 4.3 PEAK VALUES, SIMULATED REVENUE RUN (+5 mph), NEC, WASHINGTON - NEW YORK R/t

C) MAXIMUM WHEEL L/V RATIO, L/V

		 ,				- ,						
Comments												
Leading Axte	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axle 24 (Cab)	Axte 24 (Cab)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)	Axle 1 (Loco)
Measured Leading Speed Axle	30 mph	24 mph	46 mph	68 mph	40 mph	40 mph	40 mph	58 mph	4dm 09	45 mph	82 mph	70 mph
Measured Cant Def	0.0"	4.8"	0.0"	4.2"	1.2"	1.2"	1.2"	0.0"	4.8"	3.0*	3.0"	9.0.
Track Condit	Dry	Dry	Dry	Dry	Dry	. Dry	Dry	Dry	Dry	Dry	Dry	Dry
Track Milepost	96 - 95	95 - 94	94 - 93	93 - 92	88 - 87	88 - 87	88 - 87	86 - 85	1-2	7-8	10-11	81-82
Direct/ Track	North Track 2	North Track 2	North Track 2	North Track 2	East Track 1	East Track 1	East Track 1	East Track 1	West Track 2	West Track 3	West Track 3	West Track 3
Run No/ Line	404 Wa-Ph	404 Wa-Ph	404 Wa-Ph	404 Wa-Ph	406 Ph-NYP	406 Ph-NYP	406 Ph-NYP	406 Ph-NYP	405 NYP-Ph	405 NYP-Ph	405 NYP-Ph	405 NYP-Ph
Vehicle Element	Right Wheel Axle 24 (Cab)	Right Wheel Axle 2 (Loco)	Left Wheel Axle 24 (Cab)	Left Wheel Axle 24 (Cab)	Left Wheel Axle 2 (Loco)	Left Wheel Axle 24 (Cab)	Right Wheel Axle 24 (Cab)	Left Wheel Axle 24 (Cab)	Right Wheel Axle 1 (Loco)	Right Wheel Axle 1 (Loco)	Right Wheel Axle 1 (Loco)	Left Wheel Axle 1 (Loco)
% of Limit	%88	75%	74%	%92	75%	65%	%89	63%	78%	75%	%96	75%
Measured Value	0.70	0.60	0.59	0.61	09:0	0.52	0.54	0:20	0.62	09.0	0.77	09.0

Measured Value	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Measured Cant Def	Measured Speed	Leading Axte	Comments
0.68	%98	Right Wheel Axle 1 (Loco)	407 Ph-Wa	South Track 3	2-3	Dry	3.0"	67 mph	Axle 1 (Loco)	
0.63	79%	Right Wheel Axle 1 (Loco)	407 Ph-Wa	South Track 3	3-4	Dry	3.0"	79 mph	Axle 1 (Locol	
0.64	80%	Right Wheel Axle 1 (Loco)	407 Ph-Wa	South Track 3	13-14	Dry	0.0"	96 mph	Axle 1 (Loco)	
0.69	86%	Right Wheel Axle 1 (Loco)	407 Ph-Wa	South Track 3	35-36	Dry	.0.0	126 mph	Axte 1 (Loco)	
0.47	29%	Left Wheel Axle 24 (Cab)	410 Ph-Tre	East Track 2	83-82	Dry	.0.0	77 mph	Axle 24 (Cab)	
0.41	51%	Left Wheel Axle 2 (Loco)	410 Ph-Tre	East Track 2	82-81	Dry	6.0"	77 mph	Axle 24 (Cab)	
0.44	92%	Right Wheel Axle 24 (Cab)	410 Ph-Tre	East Track 2	82-81	Dry	6.0"	77 որի	Axle 24 (Cab)	
0.43	54%	Right Wheel Axle 24 (Cab)	410 Ph-Tre	East Track 2	81-80	Dry	6.0"	93 mph	Axle 24 (Cab)	
0.62	78%	Right Wheel Axle 1 (Loco)	411 Tre-Ph	West Track 3	85-86	Dry	.0.0	99 ubh	Axle 1 (Loco)	
0.58	73%	Left Wheel Axle 1 (Loco)	411 Tre-Ph	West Trck 3,4	87-88	Dry	0.0"	40 mph	Axle 1 (Loco)	
0.78	%86	Right Wheel Axle 1 (Loco)	411 Tre-Ph	West Trck 3,4	87-88	ρυ	0.0"	40 mph	Axle 1 (Loco)	
0.64	80%	Right Wheel Axle 23 (Cab)	411 Tre-Ph	West Trck 3,4	87-88	Dry	0.0"	40 mph	Axle 1 (Loco)	

TABLE 4.3 PEAK VALUES, SIMULATED REVENUE RUN (+5 mph), NEC, WASHINGTON - NEW YORK R/t

D) MAXIMUM TRUCK SIDE L/V RATIO, T-L/V

Measured Value	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Measured Cant Def	Measured Speed	Leading Axle	Comments
0.45	%06	Left Side Truck 12 (Cab)	404 Wa-Ph	North Track 2	94-93	Dry	4.8"	46 mph	Axle 24 (Cab)	
0.47	94%	Left Side Truck 12 (Cab)	.404 Wa-Ph	North Track 2	93-92	Dry	4.2"	68 mph	Axte 24 (Cab)	
0.45	%06	Left Side Truck 12 (Cab)	404 Wa-Ph	North Track 2	62-61	Dry	6.0"	126 mph	Axle 24 (Cab)	
0.46	92%	Left Side Truck 12 (Cab)	404 Wa-Ph	North Track 2	12-11	Dry	2.4"	96 mph	Axle 24 (Cab)	
0.35	%02	Left Side Truck 12 (Cab)	406 Ph-NYP	East Track 1	86-85	Drγ	0.0"	58 mph	Axle 24 (Cab)	
0.35	%02	Left Side Truck 12 (Cab)	406 Ph-NYP	East Track 1	85-84	Dry	.0.0	59 mph	Axle 24 (Cab)	
0.41	82%	Left Side Truck 12 (Cab)	406 Ph-NYP	East Track 1	82-81	Dry	1.2"	54 mph	Axle 24 (Cab)	
0.34	%89	Left Side Truck 12 (Cab)	406 Ph-NYP	East Track 2	42-41	Dry	0.0"	126 mph	Axle 24 (Cab)	
0.42	84%	Right Side Truck 1 (Loco)	405 NYP-Rh	West Track 2	1-2	Drγ	4.8"	60 mph	Axle 1 (Loco)	
0.47	94%	Left Side Truck 1 (Loco)	405 NYP-Ph	West Track 3	10-11	Dry	3.0.	82 mph	Axle 1 (Loco)	70 mph posted speed, Class 4 Track, interlocking in middle of 1° curve, Hunter
0.54	108%	Right Side Truck 1 (Loco)	405 NYP-Ph	West Track 3	10-11	Dry	3.0"	82 mph	Axle 1 (Loco)	70 mph posted speed, Class 4 Track, interlocking in middle of 1° curve, Hunter
0.39	78%	Left Side Truck 1 (Loco)	405 NYP-Ph	West Track 3	81-82	Dry	9.0"	70 mph	Axte 1 (Laco)	

Measured Value	% of Limit	Vehicle Element	Run No/ Line	Direct/ Track	Track Milepost	Track Condit	Measured Cant Def	Measured Speed	Leading Axle	Comments
0.57	114%	Right Side Truck 1 (Loco)	407 Ph-Wa	South Track 3	2-3	Dry	.9.0	60 mph	Axle 1 (Loco)	Switch, in a spiral adjacent to bridge. Posted Class 3
0.47	94%	Right Side Truck 1 (Loco)	407 Ph-Wa	South Track 3	3-4	Dry	3.0"	79 mph	Axle 1 (Loco)	
0.47	94%	Right Side Truck 1 (Loco)	407 Ph-Wa	South Track 3	13-14	Dry	.0.0	96 mph	Axte 1 (Loco)	
0.51	102%	Right Side Truck 1 (Loco)	407 Ph-Wa	South Track 3	35-36	Dry	0.0"	126 mph	Axle 1 (Loco)	Switch, tangent track, Class 5 profile exception
0.27	54%	Left Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	83-82	Dry	0.0	77 mph	Axle 24 (Cab)	
0.35	70%	Left Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	82-81	Dry	6.0"	77 mph	Axle 24 (Cab)	
0.42	84%	Left Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	82-81	Dry	6.0″	77 mph	Axle 24 (Cab)	
0.29	28%	Right Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	82-81	Dry	6.0"	77 mph	Axle 24 (Cab)	10.00
0.27	54%	Left Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	75-74	Dry	11.4"	125 mph	Axle 24 (Cab)	
0.27	54%	Left Side Truck 12 (Cab)	410 Ph-Tre	East Track 2	66-65	Dry	4.8"	126 mph	Axte 24 (Cab)	
0.34	%89	Right Side Truck 1 (Loco)	411 Tre-Ph	West Track 3	84-85	Dry	0.0"	63 mph	Axle 1 (Loco)	
0.41	82%	Right Side Truck 1 (Loco)	411 Tre-Ph	West Track 3	85-86	Dry	0.0	66 mph	Axte 1 (Loco)	
0.41	82%	Left Side Truck 1 (Loco)	411 Tre-Ph	West Track 3	87-88	Dry	0.0"	40 mph	Axle 1 (Loco)	
0.39	78%	Right Side Truck 1 (Loco)	411 Tre-Ph	West Track 3	87-88	Dry	0.0"	40 mph	Axle 1 (Loco)	

5. DISCUSSION OF RESULTS

5.1 TEST HIGHLIGHTS AND SIGNIFICANT EVENTS

- 12.5" maximum average cant deficiency achieved in a test curve.
- 154 mph maximum speed attained; no instability observed.
- No safety criteria exceeded during cant deficiency test runs on the Harrisburg line and the NEC test zone between Trenton and Newark.
- The main circuit breaker, left open for an extended time, resulted in loss of tilting at one occasion during a test; no safety criteria were exceeded.

5.2 MAXIMUM THEORETICAL CANT DEFICIENCY

Based on the trends exhibited for the safety related criteria, it could be expected that the X2000 would not exceed any of the safety criteria in the test curves for cant deficiencies of up to 15 inches. While extrapolation of the test data to this extent assumes linearity and is not truly valid, it is useful in assessing the relative margin of safety which is likely to exist for the proposed revenue service.

5.3 EFFECTS OF TILT

During two test runs on the Philadelphia - Harrisburg line, the tilt system was deactivated on the cab car and on the 2 adjacent cars (#2810 & 2609). These test runs (129,130) were carried out at 9 inches of cant deficiency, with the locomotive leading westbound and the cab car leading eastbound. A preliminary comparison of results for the cab car with those obtained from similar 9 inch cant deficiency test runs (125,126) with normal tilting shows little difference in the derailment related safety parameters.

The maximum steady state carbody lateral acceleration recorded with the tilt system deactivated was 0.19g on the cab car above truck #12 while traversing curve 662 (4°). The maximum peak lateral acceleration observed with no tilting was 0.33g while traversing curve 672 (2°).

A more detailed comparison will be carried out in the final analysis.

5.4 EFFECTS OF WET RAIL

During the test it was observed that the amount of lateral load sharing by the wheel on the low rail, due to radial steering, was reduced when the rail was wet. As a result the lateral force applied to the high rail increased. This was felt to have little or no impact regarding wheel climb due to the reduction in the coefficient of friction on the

high rail. While no hazards are anticipated in any way, further analysis to determine the effect on truck side L/V ratio is recommended to fully describe the effect of wet rail conditions on performance.

5.5 EFFECTS OF SIDE WIND ON ATTAINABLE CANT DEFICIENCY

The effect of side winds on vehicle overturning can be expressed in terms of vertical wheel force unloading. An estimate of the unloading experienced by the cab car, the worst case vehicle for the X2000 in the leading position, predicts the vertical wheel force will unload by 5.7 kN (1280 pounds) with a 40 mph side wind applied. This is roughly equivalent to the unloading experienced by the X2000 when operating at 1.5" of cant deficiency around a curve.

The effect of sidewinds on the attainable cant deficiency can also be expressed by the weight vector intercept (WVI) value. Since the wind conditions during the tests have been negligible, the measured WVI values have been low. In order to draw conclusions as to the influence of higher sidewinds on the WVI, simulations using wind tunnel test results have been made by ABB. In principle, the calculated effect of a sidewind (in an ideal curve) is added to the actual measured values.

At this preliminary stage, no calculations from a specific curve including track irregularities (e.g. from the NEC) have been done. Nevertheless there is a high degree of confidence in the method used. One uncertainty is the assumption that the dynamic variation of the WVI with sidewind is not higher than without sidewind (as in tests). Since the dynamics that are essential with respect to vehicle overturning are of rather low frequency (a very short duration wheel unloading will not result in overturning), it is likely that the low frequency variations of the WVI will not be higher than without sidewind. However, this has still to be proven through calculations.

Investigations have shown that for the X2000, the most exposed car during sidewinds is the cab car in the leading position. Preliminary results of this case were derived by adding the effect of a 45 mph sidewind on the WVI to the measured values for the curves 662, 663, 671, and 672 on the Harrisburg line, as well as for the curves 265, 266, and 268 on the Trenton-Newark line. With the above assumptions, the maximum expected dynamic value of the WVI for a 45 mph sidewind and at 10" cant deficiency is about 24.5" for curve 663 and about 23" for the other curves on the Harrisburg line. On the Trenton-Newark curves, the maximum expected WVI is about 22".

The limit of 26.5" assumes a 10% margin remaining on the inner wheels before total unloading occurs. This and the fact that the WVI values are derived with a filter frequency of 25 Hz (in Sweden 1.5 Hz is used in these cases) and most likely contains high frequency components, gives an additional safety margin against vehicle overturning at 10" unbalance and 45 mph sidewind.

5.6 EFFECT OF TRACK GEOMETRY VARIANCE ON ATTAINABLE CANT DEFICIENCY

To describe the full effect of various track geometry variations on the performance relative to the safety criteria is a major task well beyond the scope of this effort. Realistic, performance based limits for track geometry for high speed passenger train operations in the United States have yet to be developed and will be addressed in the final test report. An anomaly which reduces the crosslevel by one inch in the body of a curve will be used as a convenient estimate of the likely contribution of the 'realistic worst case' track geometry. Although it is unlikely such an anomaly would exist on Amtrak's high speed track, it is considered a reasonable indicator of the maximum track geometry related effect. The net effect of such an anomaly would be to increase the actual cant deficiency by 1 inch. Deviations in curvature or crosslevel could realistically be expected to increase the cant deficiency by this amount.

5.7 EFFECT OF SPEED VARIANCE ON ATTAINABLE CANT DEFICIENCY

Operating at speeds greater than intended due to speedometer or operator error is a likely occurance. The effect of overspeed operation is a function of both curve geometry and the planned operating speed. In general, the higher the degree of curvature and the greater the operating speed, the greater the effect overspeed operation will have on safety. The change in cant deficiency for an overspeed of 5 mph is shown as a function of operating speed for various curvatures in Figure 5.1.

5.8 EFFECT OF VEHICLE CONDITION ON ATTAINABLE CANT DEFICIENCY

Obviously the range of possible effects of vehicle maintenance condition on performance is unlimited. As a realistic worst case condition, it is conceivable that the radial steering ability of the truck would be lost.

Much experience gained from a wide variety of radial steering trucks in service (in particular, the X2000) has indicated that the components most likely to suffer from sub-standard maintenance are the dampers. Extensive trials were carried out during 1989 in Sweden to verify the effects of removing up to half of any one group of dampers, often in combinations of several groups together. It was found that under such conditions of only 50% damping, safety criteria at high cant deficiencies in curves were little affected. Stability at high speed on tangent was affected negatively, but even with truck hunting, all safety criteria were still fulfilled. However, ride comfort did degenerate more significantly with 50% damper unavailability. This supports the conclusion that damper failure is primarily a comfort and wear problem rather than a safety risk. A 1 inch cant deficiency margin should be ample to account for damper degradation.

Another area requiring maintenance is that of wheel profiles. Careful follow-up programs in Sweden during X2000 revenue service have shown that the wheel profiles maintain a fairly stable worn shape after an initial period of wear-in.

CHANGE IN CANT DEFICIENCY FOR A 5 MPH OVERSPEED

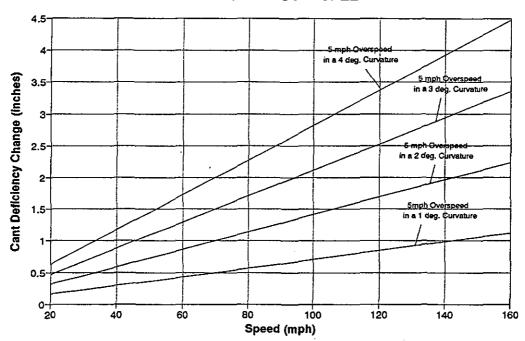


Figure 5.1: Effect of 5 mph Overspeed on Cant Deficiency

Inspection of the profiles chosen for running in the U.S. after some 5000 miles suggests this pattern would be repeated for Amtrak track conditions. Again, a 1 inch cant deficiency margin on safety should provide adequate margin for the eventuality of turning different wheel diameters and other such errors, and for a likely worst case worn wheel profile shape.

5.9 SUMMARY OF EFFECTS ON SUSTAINABLE OPERATIONAL CANT DEFICIENCY

The sum total of the above effects would be to increase the effective cant deficiency by 5.9 inches. A discussion of these effects is presented in **Section 6**.

6. PRELIMINARY RECOMMENDATIONS AND CONCLUSIONS

As previously stated, the purpose of this report is to provide a basis for establishing procedures and limits for the safe operation of the X2000 by Amtrak in the NEC. In developing the conclusions and recommendations presented here the authors have attempted to strike a balance between performance and safety. Where either the available data or time for analysis was limited, conservative judgement has been applied in the interest of safety.

The X2000 has been thoroughly analyzed and tested in Europe and has compiled a successful operating and safety record in service in Sweden. The fundamental question addressed by the tests and analysis supporting operations in the United States is how the X2000 would respond to the track conditions here.

The tests here were conducted by Amtrak over specific test zones on Amtrak's Harrisburg line and on the NEC between Trenton and Newark. Specific test curves chosen for detailed analysis ranged from 4° 16′ (409m radius) to 1° 26′ (1221m radius) giving a theoretical cant deficiency of 12" at speeds ranging from 77 mph to 134 mph respectively. Trials were carried out in each of these selected curves at up to 12" of cant deficiency or at a maximum of 125 mph, whichever limit was reached first. During the 42 test runs, from which 156 curve transits were analyzed in detail, not one safety limit was exceeded. The highest average cant deficiency recorded by the axle mounted accelerometer through an entire curve during trials was 12.5". The test runs were made in conditions varying from dry to wet and with the tilt activated and deactivited on separate runs.

The following recommendations were developed from the preliminary analysis of the test results. A brief reference to the relevant and supporting analysis, test results and conclusions is included with each recommendation.

6.1 RECOMMENDATION FOR OPERATION AT 9" OF CANT DEFICIENCY

Test results show the X2000 radial truck to be effective in transferring lateral loads from the high rail to the low rail at elevated cant deficiency. Vertical load transfer and vehicle overturning are effectively controlled by the truck design which incorporates a roll stabilizer. These design features allow the X2000 to operate in regular service at 9.6 inches of cant deficiency in Sweden (1.6 m/s² lateral acceleration), based on the design curve geometry.

The test results from both the Harrisburg line and the NEC test zones indicate the peak dynamic responses for the safety relevant parameters never reached more than 92% of the stop test criteria at up to 12" of cant deficiency.

The Harrisburg test zone was believed by the Amtrak test planners to be representative of the 'realistic worst case' Amtrak track conditions. A linear projection of the trends established from the test data suggest that, for the conditions

tested, somewhere around 15 inches of cant deficiency could be attained before the safety criteria would have been exceeded.

Several factors which were not evaluated during the test, will affect the margin of safety for high cant deficiency operation. A summary of these factors, and their estimated likely contributions, in terms of equivalent cant deficiency, is shown below.

Primary Factors Influencing the Margin of Safety for High Cant Deficiency Operations

Factor	Calculated/Estimated Equivalent Cant Deficiency				
-40 mph Side Wind	1.5"				
-Track Geometry Variations (FRA cant deficiency enforcement limit)	1.0"				
-5 mph Overspeed	1.4"				
 Vehicle Maintenance Condition (Preliminary estimate based on worst vehicle condition with sub-standard materials) 	-				

Taken in combination these effects would yield an equivalent increase in cant deficiency of 5.9 inches. While the probability of each of these negative factors existing simultaneously is considered extremely remote, planned operations at 9 inches of cant deficiency based on average geometry would produce a total equivalent cant deficiency of just below 15 inches.

While it is impossible to know the precise contribution of each of these factors and their combinations under actual service conditions, this type of assessment demonstrates that operating the X2000 at 9 inches of cant deficiency over Amtrak track can be considered safe with the following conditions.

6.2 RECOMMENDED CONDITIONS FOR 9 INCH CANT DEFICIENCY OPERATION

Condition (1) Track Geometry/Structure for 9" C.D. - The track geometry in the curves over which 9" C.D. operation is allowed should meet all applicable FRA Track Safety Standards. The limiting speed for each curve will be calculated based on a 9 inch cant deficiency using average geometry with a 1 inch tolerance limit for the worst case combination of curvature and crosslevel as measured by monthly inspections an automated Track Geometry measurement car.

- Track structure, ballast, ties and fasteners must meet the FRA regulations for the planned operating speed.

Condition (2) Wind - Should wind speeds be predicted in excess of 40 mph, X2000 speeds should be restricted to those for Metroliner operations under the same conditions.

Condition (3) Vehicle Conditions - While wheel wear has been reported from service experience in Sweden to be very light, it is considered prudent, due to the different rail profiles which exist on Amtrak rail, that wheel profiles be monitored to assure that accelerated tread and flange wear do not occur.

Dampers are used more extensively on the X2000 than on existing Amtrak equipment to limit undesired vehicle response. Evaluating the effects of degraded dampers was not part of the test program; therefore it is considered prudent that the condition of all vehicle suspension dampers be monitored to assure they are functioning properly by measuring vehicle carbody accelerations on a regular basis.

Condition (4) Speed Control - Amtrak should take steps to assure that the combined effects of speedometer error and engineer error will not result in more than 5 mph overspeed in the worst case. It is recommended that this be accomplished by careful implementation of Amtrak's and the equipment manufacturer's existing procedures for speedometer calibration and engineer training.

6.3 RECOMMENDATIONS FOR OPERATION AT 10" OF CANT DEFICIENCY IN SELECTED CURVES

From observations of both the measured track geometry and vehicle response, it is clear that some curves on the NEC could safely support operation at even higher cant deficiency. Curves which meet the following conditions should apply to safely support 10" C.D. operation:

Condition (5) Track Geometry/Dynamic Response Analysis -

Analog plots of both the track geometry and vehicle response should be analyzed to confirm that the following conditions exist:

- Relatively smooth and coordinated spirals and spiral/curve transitions
- No special trackwork or structures within 200 feet of the curve along the track (i.e.- switches, crossings, undergrade bridges, etc.)
- Limited dynamic response during simulated revenue test runs.

Condition (6) Strict speed control - Steps will be taken to ensure that the 10" unbalance speed, based on the limiting track geometry conditions, is never exceeded. Thus overspeed operation is prevented from impacting the margin of safety.

6.4 RECOMMENDATION FOR 135 MPH MAXIMUM OPERATION SPEED

The X2000 demonstrated stable operation at 150 mph over the NEC high speed stability test zone. Analysis performed by the equipment manufacturer has predicted stable performance, under normal conditions, for speeds up to 165 mph.

Both the data and the analysis support the operation at elevated speeds. Operation at speeds up to 135 mph would be considered conservatively safe under conditions 2, 3 and 4 above and the following:

Condition (7) Track Geometry/Structure for 125 mph - The track meets the conditions currently approved for 125 mph Metroliner operations.

Condition (8) Instability in Service - Any indications of instability during operation would be reported to the FRA and speeds for the X2000 would be restricted to 125 mph until the cause(s) of instability were identified and corrected.

APPENDIX A TEST EVENT LOG, X2000 U.S. DEMONSTRATION





Date	Time	MP	Run #	Direction	Un Balance	Track #	Rail Dry Wet	N2 2013 direction	Remarks
9/11 1231	1234	1	101	'W	2"	3	P	€	Old col. in computer
-		11							Lateral Arres OK
		20				4			Accelerometer stands OK
		•							Problem with magnets, cab a
									No Filte on Truck acc.
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				-					
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ļ	1611		113	W	10 u	4	W	E	
	16.52		-						
	1710		114	(LL)	1109	•	W	-	
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LR 9223-12n

Date	Time	MP	Run	Direction	l in Balance	Track #	Rail Dry Wet	N2 2013 direction	Remarks
2/12	10-16		IIS	W	104	4	0	5	
	11 24								
	1/20		16	₿	104	1	р	E	
	1132								
	240		17	W	11	4	B	B	
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 		 _	╄-			<u> </u>	<u> </u>		
<u> </u>	 	4_	4_	<u> </u>	1		 	<u></u>	
	<u> </u>			<u> </u>	<u>. </u>	<u>.</u>	<u> </u>	<u> </u>	<u> </u>
						56			

Date	Time	M	Rug	Direction	Un Balance	Track #	Raii Dry Wel	X2 2013 direction	Remarks
3/12	1020		121	W	94	7	D	W	Train turned.
	1105							(Train turned. No Y-komputation boffor MPS
									on axle 21 and 24
	125		122	B	104		Q	W	
	1140						·	<u> </u>	
	1240		100		100 54		Ø	1	
	1255		123	W	10"	4	-	W	
	16								
-	14द		124	E	11"	1	D	W	
	1440					•		-	
	1018								
7/12	1122		125	M	9"	4	b	W	Riple on V24 before 48
	1139								
	12 **		126	K	9"	1	Ю	W	
		57	عن			J		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	She cha
	,	2-5		-	· · · ·				Stem stap Frice MP
	1342							 	
	1450		27	W	12"	4	0_	W	
	15ª								
				-				<u> </u>	
	15,		8	E	12"	l	0	W	100
	1546	Z ₹			_			ļ	1:23r, L23 Ladjusted
	, CI	-	\vdash				<u> </u>		
	16 ²⁰		127	W	7"	4	0	w	No till on 4 Sand C
		ß			-	7			10 1:11 car 4,5 and 6 123,1271 mijusks
	(35								
			138	K	9"		D	W	
	1715 1720	75				 	-		L24, L24 undjusted.
	Ľ <u>"</u>				<u> </u>	<u> </u>	<u> </u>	<u> </u>	



LR.9223-12n

	_				Ispeal)			
Date	Time	MP	Run	Direction	Un Balance	Track *	Rail Dry Wet	X2 2013 direction	Remarks
1/12	048	56	720	E	130	3	a	real	
	058	4	"						
9/12/	207	34.	ર્શ) II	5	3	D	real	1 folse mongrat My (1000
	216	,,-							
	-								
12	1/25	1/1	201	W	7"	3	D	(1011	1 double magnet M1 (loc
- ا	235	-80							1 take " M4 "
1/12	25 L	17	202	€	9"	3	D	1001	
77=	301	1							
				•					
1/12	ふん	1/3	25:	w	10"	3	D	4004	1 missing magnet
	410	•						· ·	1 false + M4/10
									Waiting For Freight
1/12	अन्स	3/4	24	E	111	3	D	regi	
	3 55								
		eeu maase							
1/12	424	11/2	205	W	13,"	3	D	front	
(13-	427	-/-						118	
711	420		36	W	140	3	D	11	changedaring ru
	446				1		1		
							 		
					 				
					1				i
·				<u> </u>	T		 		
	<u> </u>				1		1		
			 		 	 		1	
		\vdash		<u> </u>	 		1	 	
	<u> </u>	1			 				
	 	i	 	 	 	 	 		
	Ĭ	ı	Ī	l .	1		1	i	•

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LR-9223-12m

						_	7200	00	Demo
					speed	<u>/</u>			
Date	Time	M	Run	Direction	Un Balance	Track *	Rail Dry Wet	X2 2013 direction	Remarks
4/2	0,25		302	E	150	3	D	(cat	
	0.5								
8/17	029	<u> </u>	206	E	9"	3	D	reev	Chancel during run
	550						 		Chanced during 144 1 false magnet My after 5.
							ļ		
		├-		 -			 		No data on computer
 .							 		Chart recorders OK
8/12	105-		_	3	 	2		Cut. 1	Clearence run
7112	<u> </u>			- **	-		 	FLONE	CLEAIDAEEIM
8/12	112	-	267	W	0)"	2	D	Frank	V-113 instead of 117
,,,_	12/2		-					1	to stricted signal
,									3
1/12	7.17		108	6	10"	2	D	rear	One vertical hit
	24								
	ے۔								
412	235	<u> </u>	209	W	114	2	<u> </u>	frunt	VellGuph instead
	245	 -	-				 -		
u /_	465	 -		6	12"	7	<u>D</u>	. 4	
4/12.	305	 - -	210	E	12	2	_ D _	rear	
	7	├─					 		
412	21		211	W	linestend	9	D	fran	~ >95 mph
<u> </u>		┝			III-SERA	~_~			3
6/12	1573		50%	W	150	3	D	-	Changed during run
	350								at mp 31
P/12			131	W	9"	7	D	YRAY	المنطاب محمد المنطقات المنطقات المستحدال وستستطار
	Mus		7	W	911	4	Snow	"/	Dop from Downingtown
	1100						<u> </u>		
(K)		<u> </u>					 		
10/iL	13	 	12	E	9*	1	Snuy	Symit	Dep From Lancenter
	1315		 -	 -	 		 	 	2nd last non tilled
	 		-	 	 	}	-	 	First curve in thesperd
	<u> </u>		<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	<u> </u>	due to low retraice



LR 9223-12m

Dele	Time	MP	Rup	Direction	l in	Track #	Rail	7,5 5013	Remarks
i		Į I			l in Halance	'	Dry Wa	direction	·
12/12	905	54	304	E	140	3	W	rear	
	915	34		i i		:	 		End of run 304
									
2/0	0.55	2U	205	V	150	3	\	Const	Exty Englished Soli
2/12	7.61	AIA	203		(30	-2-	W	front	Extra for Thuman Edu 153 mph End of Yum 305
<u> </u>	10	31	<u> </u>						man de
L	1007	54					L	<u> </u>	tud of yun 305
	[``								
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j									
 	 -			 _		<u> </u>			
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<u> </u>		 	 	ļ					
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	<u> </u>		<u> </u>	L					<u> </u>
				_				[]	
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	 	!	<u> </u>	<u> </u>	 		<u> </u>	ļ	
L		<u>L</u> _				<u> </u>	L		
				I					
	1	1				 	·		
—	 -	+-	+-	 	 		 	}	<u> </u>
	 -	 	↓		 		<u> </u>	} -	
<u></u>		_	<u> </u>	<u> </u>	<u> </u>				
L	1	\mathbf{L}_{-}			L	L	L = =	_	
		Γ				1	<u> </u>		
	 	1	1	1		1	 	<u> </u>	
<u> </u>	<u> </u>		1	<u> </u>	<u></u>		L	<u> </u>	<u> </u>



LR-9223-12m

Date	Time	MP	Run	Direction	Un Balance	Track #	Rail Dry Wet	X2 2013 direction	Remarks
14/12	84	152	400	2	9"	2	0	rear	Washington-Philadelphia channel 17-32 are recorded with lawer sample
									channel 17-32 are
									recorded with lawer sample
									freq. (100H2) due to long rus
									(Run wunder 400 - 411)
		121							length for overspace
	3 35	113							-11 ~
									First time ever this driving!
									driver is driving!!
		1/2							High L/VIL on "TRAS, not on Brush
	916	63				1			High L/VIL on "TRAS" not on Bruch LIL False from 745-985 sele
	912	60				2			<u> </u>
	922	42							MY synchronied
	960	0				1:	n i	Phy	•
									The train statts be-
14/12	1000	88	482	TI.	9"	1	P	Year	fore the measurement
									without information
									without intormation
		31				2			
		8				1			Same Track, New Humber
			Ш						after Nownk
	1101	980				5			Stop al Pour Con
									
									MP last numbers
									906 -> 900 . 906
									resynchronisod
	Th	Į.	3/4	ar t	814	U	las	nea	the one minute
	00	rh	8	wit	hom	6	an	v n	tice.
							7	1	
l									

61



LR:9223-12m

Date	Time	MP	Run	Direction	Un Balance	Track #	Rail Dry Wet	X2 2013 direction	Romarks
14/12	13.10	920	401	W	9"	5	D	front	701 - 903
	7								901-903
							`		
		2				3			`
1212	1220	6				3			
روم موری	12.53	13							Jap Newsork
mong		,							· Melyo Park
المعلل	1317	85				4			
	1322					5			" Phaladelahia
									" Physical phis Check V221+V841
									Portograph drum for
									Pantograph down for
									D'engle
									Grounding problems to the Q: shaper.
									to the Of shaper.
									to the Q-shaper.
		-							
14/12	¥128	0	33	9	9"	3	D	frant	Track 5 : Philadelphia
		60				4			
		<u>(०</u> भ्र				3			
	1526					7			Stop Baltimore
									Stop Baltimore Glipsing device 4 [axle 2] changel to 5. Trainmoved to
	•								channel to 5. Train moved to
	1607					1			
	1608	-				3			
	1627					~			Rodsianol. Consult up drain TI
		-							Red signal. Congest up from T
	1646					V 0			Shop of Warlington
	100					, y			3100
		\vdash							Sligring device to late 24
		 	$\vdash \vdash \mid$				-	 	Shiftingdevice 10 (axte 24) canged to 6.
	 	-				 -	 	 	CANGEL TO G.
	i	1							

LR 9223-12m

Date	Time	МР	Run	Direction	Un Ralance	Track #	Rail Dry: Wes	X2 2013 direction	Remarks
15/12	815	185	404	N	9:500	2	D	rear	Recorded from start
									L23224 LRY not OK from sta
		133							All signals OK
		128							Temporary stop
		122							Ponally dueraperd 129mg
	44	90							Stop a Balimore work #6. 2min
		67	av	d no	oth	٧ وم	npa	25	FYOST
		67				1_1_			
		60				2			
		18							Arrival Willmington
	929								Stop 24 Willmington Imic
	वभ					1			1 1
	1947	0				4			Stop at Vm Hadalphia
	100		406			1			Stop at Philladelphia
				<u> </u>		1			We are on wrong in
		L_	<u> </u>						and miss the high UB.
Ĺ <u>.</u>	10	158				2		<u> </u>	Back to #1
									Chand 12-32 loct
	<u> </u>	<u> </u>		<u> </u>				<u> </u>	chand 12-32 loct mpa60-57 on TRAS
							<u> </u>		but not on Brush Changed 15V supply Fabre signal me 57 = 926
					<u></u>				Charged 15V supply
<u> </u>		_		} _					Fabr signel me 57 = 906
	<u> </u>							<u> </u>	1901 CH 24466 17 JA .UFIC
<u> </u>	<u> </u>						<u> </u>		Rikked signahare (1-16) OK Readled 125m fin
	<u> </u>	49				2	<u> </u>		Readred 125mfg
<u> </u>	<u> </u>			<u> </u>				<u> </u>	Slow accoleration due to
<u> </u>	<u> </u>		<u> </u>	<u> </u> _					law line voltage 10ky
			_				<u></u>		\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
	1050	19	L			1		<u> </u>	Stop at Newark Bridge
	1059	L		<u> </u>					
	1142	1							Dep -11 - Original Contraction of the Contraction o
	1125					6			Stop on bridge " Stop in New York Channel 17-32 OK
	1124		<u> </u>						Channel 17-32 OK
<u></u>		_	<u> </u>]	 			
<u> </u>	<u> </u>	_					 	<u> </u>	
	1	1	1	.	1	}]	

Def

LR.9223-12m

Dete	Time	MP	Run	Direction	Un Italance	Track #	Rail Dry Wet	N2 2013 direction	Remarks
15/12	1212		45	W	9.5-4	6	D	front	Leque NYP
	1214					23			
	ļ,	6				3			
]		24						<u> </u>	One Calse magnet before 1
 	.052	60					<u> </u>		1 · 1
 -	255	8 6~				3	 -		Stop for restrictive signal
 -	1317	85	-			2	 		Just before PhiladelHa
 -	12.1	زو				3	}		Bust before Imitacina
			-	 -			 -	 	
15/12	128	85	40	5	9"+5-0	A	D	YEST	Verebban of the
			10		1 13 047			1-	marning textrus
									Kepetition of the morning test run but on the right To
								 	
	1344	8				2			5h1/4
									4
15/12	1354	58	411	W	75~	3	D	front	Cross aut to # 3
<u> </u>							<u> </u>		
]	1413	왕.				4			Step at . Philadolphia tra
 	-						 	 	
3	1041	 		S	9150ph	3	6	Les A	D-0 - 10 - 14 - 14 - 1
15/12	177.	-	161	3	1+3-4-		<u> </u>	(4004	One falit mp before no
-		├─							One fait mp before no
 	1454	15	-			3	 		Stop at Wilmington 2 min
	-	60		,		4	 		345-34-31
		73				3	-		
	159								Stop Balhmore TK#7 11
		11/2							Power-alf twice to 144
		119							Strip charl teconders.
									TRAS OK
	1543	145}							TRAS OK Stop 2 min outside Washingh Stop in Washington
<u></u>	1557	<u> </u>	 		L	16			Stop in Washington
 	-	├]	 -		ļ	<u> </u>
-	 	 	 -	<u> </u>			 		
L	<u> </u>	<u> </u>	<u> </u>	l	<u> </u>	<u> </u>	<u> </u>	<u> </u>	L

APPENDIX B TRACK CURVE INFORMATION

	TIMETABLE	MRE	MREPOST	ð	CURVE DECMETRY	<u>~</u>			MOR	多田公司	PANCE SP	PROPOSED CURVINO SPEED FOR X-2000 TEST	X-2001	83		_	PROPOSED MAXIMUM
2	DESCRIPTION	200	LOCATION	DEGREE	RADIUS	3	2	2	8n.s	2	2	82	2	. g	11.CB	17.08	TESTING SPEED
		West	East	(decimal)	[jee[]	[inches]	[udur]	[mbu]	[mpm]	[mph]	[mph]	[udu]	[wdw]	[hdm]	[wbu]	[tydw]	[wbu]
119		68.58	92'99	090	8)248	1.875	1 06	110	110	윤	110 1	19 10	110	유	5	₽	5
676.1		68.22	66.17	0.37	15,628	0.750	5	5	5	£	읃	5	2	110	욷	\$	•
£		88	£.79	0.32	18,094	0.750	5	5	ŧ	1	19	5	+	1 5	1 0	\$	•
678		63.87	83.51	8,	6,730	3.375	8	額	69	110	110	110	110	£	110	2	•
674		63.21	62.97	0.45	12,733	0.500	8	5	110	\$	£	5	. 운	10	2	\$	•
E		8	61.64	1.02	5,636	3250	ಹ	ē	\$	110	우	2	1	5	5	\$	•
219	Curve west of MP 61	61.48	60.97	500	2,818	6250	2	84	8	28	8	97	\$	₫	107	5	•
67.	Curve west of MP 60	80,62	26 63	200	2,866	5.500	22	83	87	2	88	88	苕	葛	5	2	•
929	Curve west of MP 59	28	33	1.	5,209	3,000	88	88	ā	\$	우	£	읒	\$	£	2	•
8		88	27.85	1,52	3,778	9:200	8	88	8	₹	2	110	ŧ	110	\$	5	•
88		57.64	67.36	90	8,815	1250	16	107	110	읃	2	15	\$	110	阜	\$	•
299		3 98	62.73	860	5,827	220	84	88	葛	5	110	1	5	110	110	₽	•
8		25.58	54.38	0.45	12,733	0.875	\$	1 0	5	1 0	110	110	110	110	10	₽	•
8		88	53.66	0.47	12,278	0.875	<u>\$</u>	110	5	2	110	1	5	110	1	5	•
<u>*</u>		63.25	52.74	206	2,785	9,629	22	8	8	8	3.	26	ē	호	\$	2	•
8	Curve west of Gap	25	25.00	8	1,0	5.750	8	8	Ø	8	<i>1</i> 9	2	2	22	11	æ	•
8	Curve at Gep	51.63	20.73	4	38	5.625	ঠ	25	8	8	8	88	7	R	ĸ	1	•
8		50.61	50.03	200	2,865	5.875	8	ᇗ	8	8	88	8	葛	107	1 0	\$	•
88		90.08	49.81	100	5,730	3.375	8	該	8	읃	₽	5	\$	5	£	\$	•
8		49 16	18.84	1 ,00	6,730	3.375	88	葛	8	유	\$	110	£	£	5	£	•
8		8 72	48.36	5 .	6,730	3.125	ಹ	₽	\$	10	5	9	110	2	5	\$	•
8	Curve west of Algien	82.89	47.50	200	2,865	5.750	2	\$	8	8	88	83	衰	5	\$	\$	•
8		98 99	46.77	0.30	17,189	0.375	ŧ	5	2	\$	윤	110	\$	10	\$	윤	•
8		£.34	4524	9,0	14,324	0,750	운	\$	5	5	110	£	5	110	#	Ş	•
<u>8</u>		4.8	44.61	0.46	12,733	0.875	5	£	110	10	10	5	1 0	19	10	\$	•
8		62 Z	83.68	0.32	18,094	0.750	5	5	5	110	5	5	1	5	5	2	•
8		43.97	88	0.37	15,628	0.750	*	약	5	5	5	5	1	110	1 0	운	•
8		2 .83	4.32	9.0	8,815	2250	6	5	5	110	1 0	1 10	110	#	110	5	•
8		41.00	40.84	0.73	7,640	1.875	8	5 0	5	110	110	5	110	5	5	£	•
8		8 8	38.42	0.67	8 ,564	2250	\$	5	110	£	1 0	5	1	1 5	5	5	•
8		8	98.30 38.30	990	#.468	<u> </u>	5	5	110	110	110	5	5	110	1 0	5	•
3		37.80	37.33	13	e es	-		•	3	;				;			

X2000HBE XLS

Eastbound

	THETABLE	MILEPOST	POST	3	CURVE GEOMETRY	≥			PROP	PROPOSED CURVING SPEED FOR X-2000 TEST	RVING SE	EDFO	3 X-2000 1	ESI			PROPOSED MAXIMUM
Š	DESCRIPTION	100	LOCATION	DEGREE	RADIUS	SE	2		3		2		2 8	配	1178	₹	TESTING SPEED
		West	East	[decima]]	(Jeal)	(inches)	[mph]	[mph]	(mph)	[tudus]	[mph]	[mph]	[mph]	[udur]	[mph]	(mph)	[wdw]
35		37.30	36.77	86.0	5,827	3.500	28	\$	110	110	110	윤	110	110	110	110	110
249		36.67	8.3	0.37	15,626	1,250	5	110	110	110	110	유	1	유	110	13	•
949		35.55	35.43	0.32	18,094	1.125		5	110	#	운	우	4	5	운	5	•
33		35.13	3,3	0.32	18,094	1.500	2	\$	110	욷	2	무	2	皇	읃	110	•
75		34.58	31.15	0.92	6251	3,000	83	ş	12	5	1 0	÷	110	110	운	110	•
3		30.00	33.55	0.72	2,996	2250	ħ	1	110	5	5	읃	110	1	#	5	•
25		33.16	32.88	0.82	7,016	2500	88	107	\$	우	110	운	110	110	110	\$	•
2		32.56	32.18	0.97	2832	3,375	26	호	5	110	110	은	110	1	110	91	•
95		31.58	31.27	£.	3,370	6.000	83	8	8	\$	\$	\$	5	1	10	110	•
88	1st & 2nd curve 1200" west of Signal 295	30.84	30.34	2.37	2,421	5625	2	æ	8	ಪ	81	5	3,	26	6	흄	•
88	1st & 2nd curve 1200" west of Signal 295	30.28	29.81	3.00	1,910	9:200	2	<i>1</i> 9	z	7	Ħ	8	8	98	8	91	•
837		28.28	28.29	0.20	28,648	1.250	110	10	5	110	110	110	110	1 0	5	110	•
88		28.71	25.55	97:0	12,733	1.500	5	#	110	1 5	5	운	#	110	5	110	•
82		24.50	24.15	0.50	## 664.	1,750	2	10	5	\$	5	읒	110	410	110	110	•
喜		23.60	23.30	850	38,648	0.750	5	110	110	110	£	5	110	10	5	110	•
8	First 3 curves west of MP 21	22.74	23	502	2,736	922	4	듄	88	8	83	6	5	호	6	#	•
83	First 3 curves west of MP 21	22.31	21.97	585	2,736	5.750	æ	83	87	6	ಹ	88	10	\$	\$	#	•
8	First 3 curas used of MP 34	2.5	28	212	2707	5695	٤	æ	æ	8	8	ន	8	Ę	Ş	Ç	•

X-2000 TEST PROGRAM HARRISBURG LINE SPEEDS

Westbound

	THETABLE	MILEPOST	 g	20	CURVE GEOMETRY		_			CALCIEA	CALCULATED CURVING RPEEDS		8				PROPOSED MAXIMIM
Š	•	TOTAL STATE	3	Second	4		1	1	•								TOTOGO MANIMOM
			£ ₹	[decima]	(Jeef.)	(inches)	1 1 1 1 1 1 1 1 1 1							17 Sept. 18		T Town	TESTING SPEED
8	First 3 curves went of MP 21	21.64	21.88	2.13	2,686	5.750	12	듄	æ	ı	1	1	1	1		2	110
829	First 3 curves west of MP 21	22.01	233	2.10	2,728	5.750	<u>u</u>	2	8	88	83	26	8	707	107	9	•
<u>8</u>	First 3 curves west of MP 21	22.37	22.76	28	2,818	6.750	æ	8	18	ಹ	88	88	豆	15	8	2	•
8		83	23.60	0.20	28,648	1,000	1 0	皂	2	유	110	5	욛	100	2	-	•
8		24.63	24.85	1.17	4,911	4.126	8	葛	氢	\$	110	5	台	5	皂	2	•
 §		22,23	34.85	0.63	13,222	052.0	ŧ	1	110	110	110	110	150	100	윤	=	
<u>\$</u>		88	83	0	13,751	.	£	5	₽	1 5	110	유	5		윤	-	•
8		83	8.8	0.23	33. 33.	0.875	19	1 0	19	150	110	19	16	150	읃	5	*
8		38.43	8.8	0.27	21,486	100	110	5	1	1 5	110	110	₽	130	윤	<u></u>	•
8		88	88	80	28,648	5 <u>5</u>	110	#	110	1 10	110	110	\$	100	욛	£	
3	1st & 2nd curve 1200' weet of Signel 296	28.8	838	3.07	1,968	5625	ន	6 2	2	74	11	8	83	18	88	<u>ਨ</u>	•
8	1st & 2nd curve 1200* west of Signal 295	30.32	30.81	236	2,438	5825	2	11	8	\$	8	<u>8</u>	ま	88	₽	<u></u>	
9		3122	31.56	1	3,697	5.875	8	88	葛	磊	1 09	우	9		문	-	•
<u> </u>		32.16	32.56	80	6,139	3,500	8	107	1	1 5	100	10	110	150	5	£	
3		32.87	33.15	28.0	7,016	3500	10	5	\$	1	100	윤		-	우	₽	
2		33.57	33.87	0.27	2,486	125	9	110	1 0	110	9	5	110	110	읃	£	•
*		88	34.61	0 32	18,084	1.135	운	ŧ	£	110	5	5	150	110	10	2	•
9 9 0		36.06	35.19	93	10,418	1.375	1 0	5	유	1 10	110	皇	윤	110	19	<u></u>	•
3		85. 88.	36.02	98	14,947	82	\$	우	+	110	110	110	5	150	110	<u></u>	•
3		38.1	36.26	0.37	15,628	1,500	\$	#	1 5	110	110	19	5	110	\$	£	•
3		£ 8	37.31	8.	5,730	320	8	1 02	\$	\$	110	110	55	110	15	<u>۽</u>	•
3 8		37.34	37.83	96.0	5,827	3.375	88	₽	우	110	110	2	2	110	우	2	•
8		8 9	38.	0.47	12,278	1.375	\$	\$	£	£	1 50	1 0	5	150	110	皇	•
<u> </u>		30.45	36.90	679	7,640	2.500	萄	5	1 10	1 0	110	110	5	110	£	£	•
8 8		8	8	20	7,813	2.500	≱	2	5	5	110	110	5	150	110	2	•
3		# 8	2 8	2	7,813	2.375	葛	\$	2	유	1 0	110	1 5	150	110	<u></u>	•
8		43.60	17.04	3 .0	13,751	0.500	유	110	5	110	1 0	5	5	110	윤	₽	
8		45.13	45.34	0.45	12,733	0.750	\$	\$	1 0	110	5	5		110	₽	-	•
8		46.76	46.87	0.37	15,628	900	ŝ	1	5	5	15	5	5	150 1	£	 \$	•
8	Curve went of Atglen	47.41	48.21	202	2,841	9:500	æ	8	8	8	ぁ	88	5	·	8	-	•
8		48.28	59.87	0.97	5,927	3000	ぁ	苕	5	5	5	5	5	15	₽ •	<u>-</u>	•
2 3		5 6.76	80.08	효	909'9	3.375	8	笤	\$	51	19	2				 \$	•
<u>2</u>	•	\$ 12	5. 5.	80	6,486	27.50	8	\$	5	5	110	10				- 2	•
	•		•			-	_			!	!	<u>:</u>					

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	TIMETABLE	INCENT	SS	85	CURVE GEOMETR				-	ALCULA)	ED CURY	ALCULATED CURVING SPEED	S			PROPOSED MAXIMUM
Š	DESCRIPTION	LOCATION	ğ	DEGREE	RADIUS	6	2	1 8	_		TUB ELL	_	8 10'UB	B true	12°UB	TESTING SPEED
		East	West	[decimal]	[[00]]	(inches)	[mph]	(mph)	1	il [hqm]	_	[udw] [udw]	l (mph)	7	[mph]	[mph]
28	Curve east of Gep	20.22	50.64	2.06	2,786	5.750	28	æ	87					ľ	110	110
88	Curve at Gap	50.78	51.73	9	1,415	923	ヹ	21	8					æ	æ	•
8	Curve west of Gap	20:29	52.46	4.13	1386	5.875	28	28	5	*	9 /9	22 89	*		2	•
3	Curve at MP 53	22.77	63.27	202	2,841	9.500	2	2	28			6 101	•	\$	£	•
88		88	27.02	0.45	12,733	0.75	\$	5	1	\$	15	110 110	5	100	\$	•
8		¥.	54.68	0.45	12,733	0.750	\$	5	110	110	110 11		100	±	110	•
88		28.82	88.88	8:	5,730	3,000	8	ŝ	701	110				110	5	•
8		62,79	67.66	88.0	8,815	98.1	83	1	5		12 11	110	1	1 0	#	•
88		S. C.	88.88	8.	3,820	5.500	8	88	<u>\$</u>					100	5	٠
929		35 .52	89.68 89.68	0.97	5,927	3.125	88	衰	1						110	•
꾪	Curve west of MP 60	26.93	60.61	203	2,818	5.625	22	8	28	83	8	98 101	100	5	410	•
8	Curve west of MP 61	80.98	61.48	200	2,865	5.625	ድ	æ	83						110	•
E		61.63	17.23	1.00	5,730	320	88	효	5	1 0	110				110	•
25		82.38	8322	0.43	13,222	0.500	8	8	8	8				8	8	8
£		63.53	63.87	8.	5,730	2.625	8	8	8	8	8			8	8	•
8		2	65.51	0.33	17,189	0.750	8	8	8	8	8	86	8	8	8	•
<u> </u>		98.36	93.98	990	6,741	2.875	8	8	8	8	8	8		8	8	•

69

	THETABLE	IN EPOST	<u>وا</u>	5	CURVE GEOMETRY		!	į		STOR	CALCULATED CURVING SPEEDS	MING SPI	SU				PROPOSED MAXDRUM
7	DESCRETION	LOCATION West En	10 E	DEGREE (decimal)	PADRUS (Fer)	S.E. (Inches)	3 5	2 3						facti	#178 (mph)	17.18 [for]	TESTING SPEED
305		95.40	85.30	8.	2,889	200	8	88	=	۶	2	88	88	ន	ន	ន	8
동		86.08	86.00	1.47	3,907	<u>5.</u>	8	ĸ	≅	87	8	8	8	8	8	8	•
8	Curves at east & west ends of N. Phila. sta. pitfim.	8.83	25.02	0.63	6,876	500	8	8	8	8	88	8	8	8	8	8	•
8	Curves at east & west ends of N. Phile, ste. ptffm.	8£.78	84.70	1.03	5,545	8	4	88	8	8	8	8	8	8	8	8	
8	Curve MP 84.0 to 2nd Street overhead bridge	88	83.08	252	2277	200	29	<u>_</u>	ĸ	æ	8	88	28	8	8	8	•
8	Curve between Shore and Ford	87.75	81.38	4.02	\$	25.	8	38	5	ま	67	88	2	2	11	æ	6
8	Curve eastward from Ford	81.30	80.80	1.80	3,163	200	8	8	æ	8	88	22	8	88	\$	5	•
8		8 8	\$5. \$5.	09:0	9,549	58	8	葛	\$	6	8	葛	\$	葛	8	8	•
8		78.51	8.80	0.32	18,094	8	8	\$	\$	8	≅	乭	8	5	\$	8	•
র		13.0	89 .92	8.	6,730	£7.	衰	12	138	124	恏	8	恏	83	छ	8	125
8		78.47	36 ±	99.0	8,386	3.25	=	8	稅	冠	泵	稻	稫	窈	छ	×S	•
8	First curve west of MP 75.0	75. 65.	75.08	0.75	7,640	8	115	23	ね	恏	83	恏	8	窈	弦	82	•
ষ	Reverse curves between MP 74.0 and MP 75.0	75.08	74.62	5 .	3,667	573	8	88	\$	호	葛	5	117	8	124	83	•
8	Reverse curves between MP 74.0 and MP 75.0	74.47	74.07	1.47	3,907	8	8	88	ŝ	荵	5	₹	118	苕	恏	83	•
28		12.57	11.27	0.33	17,189	15	恏	冠	₹ <u>3</u>	恏	恏	1 5	恏	15	稅	ĸ	•
8	Curve weet of Croydon	70.61	90:02	5.18	4,842	57	意	\$	7	1 19	124	恏	恏	恏	स्र	83	•
28		2.38	88.89	0.17	34,378	8	窓	2	₹	窓	\$£	\$	窓	窓	窓	\$	150
8		68.78	22.89	0.47	12,278	8	121	8	\$	3	\$	\$	2	窓	窓	8	•
8	Curve weet of Grundy	88.33	29.53	2.0	988'	Ę	12	뚕	8	₹	2	8	2	8	2	8	•
র্	Curve east of Grundy	25.	9	0.65	8,815	3.75	<u> </u>	뜐	2	5	₹	SE	\$	窓	\$	8	•
8	Curve between MP 61.0 and MP 62.0	61.83	61.36	0.72	7,986	ख	8	5 2	2	吞	. ই	2	8	\$	窓	8	•
8		8	22.09	0.36	16,370	8	恏	₹	窓	恏	2	8	\$	35	毰	8	•
R	First curve west of Montis	57.13	97.00	0.57	10,111	28	12	包	8	ā	ठ्ट	乭	苍	窓	\$	2	•
8	First curve weet of Trenton	88.33	20.95	0.67	9 5.6	23	\$	5	恏	8	Ξ	\$	苕	33	蓉	<u>\$</u>	•
2		8	90.36	0:30	19,009	8	窸	乭	窓	8	\$	\$	容	恏	憝	超	•
E		40.24	39.48	0:30	600'61	8	2	2	33	8	8	嶅	2	2 5	<u>হ</u>	8	•
38		38.38	# #	80	11,090	8	<u>5</u>	ā	\$	3 5	33	35	3 5	33	乭	<u>₹</u>	•
	Page 1 of 2															. Š	XYMMEE YI S

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Eastbound

	THETABLE	TSOGE MA	158		CHAVE GEOLETRY	¥				CALCON	ATEDICA	CALCULATED CURVING SPEEDS					PROPOSED MAXIMUM
EV.	DESCRIPTION	LOCATION		DEGREE	RADRIS	#4 #4		8		5	2	2			11"LB 42	17.08	TESTING SPEED
		West	*	[decimal]	[heet]	[inches]	[mph]	[mph]	(mph)	[mph]	1	Ì		1		[wow]	[mph]
272		34.21	33.75	0.30	19,089	13	12	2	150	35	<u>8</u>	弦	55	2 5	150	窓	150
27.4		31.34	31.12	0.45	12,733	2.75	1 3	2	<u>₹</u>	窓	憝	窓	5 5	窓	₹	窓	•
273		30.68	30.28	0.43	13,222	2.78	签	₽	窓	憝	窓	窓	2	窓	₹	2	•
w		28.83	88	50	12,278	23	424	83	2	इ	झ	झ	इ	छ	₹	इ	
27.1		27.65	27.03	970	20,222	15	2 5	3	窓	窓	ŝ	3 5	2	3 5	\$	<u>\$</u>	•
270 Third curve w	Third curve weet of Lincoln	27.17	28.7	11.0	7,473	3.75	42	\$	\$2	8	ā	₹	2	苕	\$	₹ 	•
269 Second curve	Second curve west of Lincoln	88	28.38	 85	3,861	5.75	83	88	萄	\$	112	116	₽	5 2	8	寂	22
268 First curve w	First curve west of Lincoln	28.64	27.68	1.87	3,069	83	ಪ	8	8	26	₽	₫	\$	112	115	#	•
267 Curve at MP 25.0	25.0	24.53	24.11	1.18	4,842	4.75	8	葛	墓	#	£	124	恏	恏	恏	₹ S	•
266 First curve in	First curve west of MP 24.0	23.88	23.61	55.1	3,697	57.5	8	88	乭	≱	\$	113	117	8	124	K	•
265 First curve et	First curve east of MP 24.0	23.51	288	1.6	3,961	22	8	8 8	喜	衰	5	¥	118	怒	商	恏	•
*		22.81	22.45	11.0	7,43	8	#	寂	寂	恏	恏	短	恏	恏	冠	泵	
88		202	21.88	0.72	7,996	4	8	恏	恏	83	83	\$3	恏	恏	恏	छ	•
2 8		21.84	21.68	27.0	286 286	3.25	112	8	稏	2 2	83	弦	恏	恏	恏	农	•
1 28		99 90 90 90 90 90 90 90 90 90 90 90 90 9	20.71	290	9 60	328	1	졍	졄	\$3	졄	83	短	恏	恏	寂	•
38		89.	20.38	939	22,919	0.50	恏	恏	碗	2 3	82	Ħ	窊	83	稻	83	•
229		19.74	19.61	Q.	13,751	15	恏	寂	弦	1 3	冠	短	恏	恏	恏	稻	•
328		19.41	19.28	82.0	20,222	£.	窈	র	8	2 3	₹ 2	恏	稏	恏	켮	窓	•
526		18 .94	18.04	0.42	13,751	300	瓦	稻	磊	恏	恏	1 2	恏	玆	₹ <u>3</u>	宛	•
3 2		18.50	18.20	80	88.68 8.68	8.0	ফ	稏	寂	83	茲	短	恏	恏	恏	短	•
蒸		15.10	27	0.20	28,646	0.50	冠	短	稫	1	恏	恏	弦	恏	窓	82	•
253 Curves betw	Curves between Eizzbeth & Elmora Block Station	14.26	14.03	2.37	2,421	2.50	8	ន	<i>1</i> 9	2	æ	8	82	84	8	ぁ	110
252 Curves betw	Curves between Elizabeth & Emors Block Station	13.to	13.06	1.97	2,913	23	R	=	8	88	8	35	88	嘉	葛	8	•
3 2		12.54	12.29	820	28,648	8	유	\$	웃	5	£	\$	5	110	£	9	•
88		5 .68	10.24	0.32	18,094	200	\$	우	皇	5	\$	5	=	\$	2	_	•
249 Curve at Hunter	1	874	9.19	25	909'5	272	8	-8	8	8	8	8	8	8	8	8	8
248		930	930	1.0	3,907	238	2	æ	8	æ	8	8	8	8	8	8	•
Page 2 of 2	42															X20	X2000NEE.XI.S
1																	

	THETABLE		MKEPOST	3	CURVE GEOMETRY	È				CAIGH	CALCIII ATED CIRVING SPEEDS	MAINS SO	1 26				THE COURT OF THE C	_
8	DESCRIPTION	3		DEGREE	RADIUS	F.	2	2	378	2	2	2	_	19.18	#2.E	立る	TESTING SPEED	
		E	¥ SE	(decime)	(Jeof)	(Inches)	(mph)	[lydw]	[mph]	[mph]	[mbh]	[udu]	[wbh]		[moh)	[mph]	[wbw]	
5 78		9.20	83	0.95	6,031	1.000	82	18	8	8	8	8	8	8	8	8	8	_
28	Curve at Hurter	10.24	10.56	0.97	25'5	2.750	8	8	8	8	8	8	8	8	8	8	•	
প্ত		12.28	12.56	0.32	18,094	82	2	£	£	+	9	#	£	5	5	5	110	
ছ		13.05	13.10	0.20	28,648	0.50	5	2	1	5	5	5	5	\$	5	2	•	
Ø	Curves between Elizabeth & Elmona Block Station	14.05	#Z3	8:	2,938	88	æ	æ	8	87	22	8	88	葛	8	8	•	
Ø	Curves between Eizzibeth & Elmora Block Station	14.28	2,7	2.40	2,367	88	19	2	ĸ	æ	83	88	88	83	88	83	•	
র		18.20	18.48	0.20	28,648	0.500	恏	贫	1 8	恏	恏	83	1 5	恏	1 3	8	22	
8		18.85	18.86	0.20	28,648	0220	寂	稻	恏	83	怒	充	恏	1 3	83	1 3	•	
8		19.25	19.45	0.20	28,648	0.500	恏	छ	冠	怒	恏	恏	窓	恏	8	13	•	
8		19.75	69.69	0.20	28,648	0.500	恏	ষ্ট	轻	8	젻	窓	恏	恏	8	Ŕ	•	
8		20.38	20.7	0.48	11,864	1.500	115	1 3	紹	稻	稻	恏	恏	恏	<u>₹</u>	ख	•	
8		20.74	80	0.28	20,222	90	ই	稅	2	1 3	弦	恏	恏	稻	1	स्	•	
Ŕ		21.67	28	0.70	8,185	4 000	\$	稻	怒	র	稅	恏	1 5	窓	恏	Ŕ	•	_
Ħ		28	208	0.70	9,186	3,000	Ξ	笤	恏	恏	恏	恏	\$3	恏	恏	ĸ	•	
8		22.47	22.84	99.0	8,815	3.500	52	恏	恏	2 3	恏	₹ <u>3</u>	恏	恏	恏	Ŕ	•	
Ŕ		22.87	23.57	0.62	7,016	65.	115	苕	兹	恏	83	恏	恏	窥	\$6	8		
8	First curve east of MP 24.0	23.66	2322	1.42	4,04	0009	88	\$	衰	읃	15	1	恏	1 33	2	8		
8	First curve west of MP 24.0	24.15	24.59	150	3,820	9.500	8	88	乭	\$	\$	#3	##	2	<u> 18</u>	18	•	_
282	Curve at MP 25.0	24.73	25.52	£ 23	£77.	5	88.	窝	\$	1 3	118	豆	恏	1 83	8	18	•	
8	First curve west of Lincoin	88	8.8	1.83	2,964	6.000	8	28	8	ã	88	葛	衰	8	12	5	•	_
8	Second curve west of Lincoln	22.82	27.18	1.63 53.1	3,997	9009	88	\$	磊	8	¥	*	22	8	<u> </u>	8	•	_
8	Third curve west of Lincoln	27.48	27.68	0.77	7.473	3.750	12	8	\$	8	ã	₹	蓉	<u> </u>	\$	8	051	
£		88	29:03	0.20	28,648	1.500	3	2	窓	35	3	乭	乭	8	3	8	•	
£		30.27	30.68	0.43	13,222	2.750	8	\$	憝	2	2 5	窓	2	乭	₹ 2	8	•	
8		31.13	3.33	0.45	12,733	3,00	恏	₹	憝	\$	2	<u>₹</u>	衮	苕	\$	8	•	
3 2		39.71	34.22	0.45	12,733	300	恏	5	窓	₹	窓	₹	8	乭	₹ 2	8	•	_
8		38.08	30.37	0:30	19,089	93:1	5	5	乭	乭	<u>\$</u>	33	35	\$	5	Ē	•	
	Dan 4 260					•							<u>:</u>	<u>}</u>	<u>}</u>	<u>-</u>		_

Page 1 of 2

Westbound

	TIMETABLE	IN 690ST	¥	2	CURVE GEOMETRY	_ ≥				CALCAL	CALCH ATED CURVING SPEEDS	WWG SP	Sta				PROPOSED MAXIMUM
į	TO CONTROL OF THE PARTY OF THE		_	Š			=	5			4		_	9	9	9	TOTAL COCO
\$	DESCRIPTION	East	#			e.c. (inches)	s OB [mph]	(mph)	(mph)				(mph)	1		(moh)	(mph)
238		39.49	40.28	0.52	11,090	3250	131	142	8	2 5	1 50	650	2	2 5	2	<u>₹</u>	150
#		50.38	90.50	0.30	19,059	991	\$	乭	贫	2	द्ध	₹	2	弦	<u>₹</u>	2	•
338		56.13	98.36	0.27	21,486	98	2	\$	2	2	嶅	窓	2	2	嶅	इ	•
8	First curve west of Trenton	88 98	57.12	0.67	8,594	2500	\$	#	121	8	5	窒	窓	2	乭	इ	•
8	First curve west of Morris	28 .42	83	0.82	7,016	8	Ξ	1	<u>83</u>	<u> </u>	85	5	2	<u>₹</u>	窓	इ	•
Ħ		29 .50	8 .	0.17	34,378	0.750	苕	乭	2	35	\$	8	₹	<u>35</u>	\$	8	•
8		60.24	25.09	0.37	15,628	2280	5	窓	2	35	弦	8	乾	2	苍	<u>₹</u>	•
8	Curve between MP 61.0 and MP 62.0	61,40	97.94	673	7,813	957	121	82	2	<u>5</u>	5 5	2	5	2 5	窓	ই	•
Ŕ	Curve east of Grandy	8	8	990	8,815	89	₹	ফ্র	Ξ	*	2	乭	乾	8	\$	द्ध	
8	Curve west of Grundy	86.63	86.33	0.73	7,813	4.500	121	82	8	5	憝	忞	₹	窓	\$	ই	•
**		68.72	67.68	0.47	12,278	2250	127	8	₹	乭	≅	졄	憝	8	\$	\$	•
8		88	88.73	0.17	34,378	020	苕	恏	窓	窓	苕	乾	2	\$	贫	恏	•
8	Curve west of Croydon	80.00	93.02	1.1	4,911	9009	72	₽	48	₹	窈	恏	恏	83	恏	83	\$7
8		1221	2.60	93	16,370	1,500	贫	恏	窊	র	恏	充	恏	83	র	紹	
8	Reverse curves between MP 74.0 and MP 75.0	74.08	74.49	1.6	3,951	5.750	83	88.	흄	\$	4 2	116	₽	农	ফ	ফ	
Ŕ	Reverse curves between MP 74.0 and MP 75.0	74.64	15.11	4.	40,4	2,000	8	88	\$	葛	윷	11 5	119	8	র	83	•
8	First curve west of MP 75.0	75.14	₹9	6.73	7,640	3.500	Ξ	8	প্ত	恏	衮	83	83	恏	2 2	83	•
8		78.14	38.46	9.0	8,	3250	113	豆	恏	恏	恏	冠	恏	恏	铳	稻	•
₹ -		28.20	4.0	8.	5,730	00,4	8	107	13	笠	젻	恏	恏	恏	恏	沒	•
8		78.21	28.50	0.30	17,189	<u>8</u>	乭	葛	葛	\$	8	ŝ	\$	\$	\$	\$	100
8		22.87	20.73	200	9.291	1500	\$	\$	8	葛	\$	5	喜	\$	\$	\$	
*	Curve between Shore and Ford	91.39	81.75	4.07	1,409	2000	ន	28	8	8	88	8	2	R	æ	"	•
8	Curve MP 84.0 to 2nd Street overhead bridge	8 .	83.	2.47	2,323	200	8	2	æ	8	83	₩	8	8	8	8	8
8	Curves at east and west ands of N. Phile. station pl	87.7	87.8	9 7	5,289	80	æ	æ	82	8	8	8	8	8	8	8	•
8	Curves at east and west ends of N. Phile. station pl	8	8 6.04	0.80	7,162	228	8	8	8	8	8	8	8	8	8	8	•
ਫ਼		20.03	35	1.37	4,182	98.	88	æ	8	82	8	8	8	8	8	8	•
8		86.38	29	8	3,016	2250	8	83	*	R	8	8	8	8	8	8.	•
7	- Page 2 of 2															\$	X2000NEW.XLS
X.F	O															•	

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PREPARED BY: Conrad J. Ruppert, Jr. Mgr. Field Engineering

EASTBOUND - TRACK NO.2 Washington DC to New York, NY

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NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

WAS to NYP

MILEPOST TIMETABLE CURVE GEOMET 138.00 134.50 WASHINGTON TERMINAL LA AVENUE DEGREE SUFE 138.00 134.50 WASHINGTON TERMINAL LA AVENUE 280 134.60 134.50 WASHINGTON TERMINAL LA AVENUE 280 134.60 1																								126		85		TIMETABLE SPEED	LINE SPEED	MAXIMUM
HILEPOST HILEPOST THEFTARE CURVE GEOMETRY UNBALANCE CURVE GEOMETRY UNBALANCE CURVE GEOMETRY UNBALANCE CURVE GEOMETRY CUR	5	. Y	R	0	w	*		\$	9	90	\$	S	6	2 .	10	15	35	S	8	2	ĸ	10	0	Ī	o		0		INCREASE (moh!	8
High Post THEFOST THEFOSE CURVE GEOMETRY UNBALANCE COMPOSITION UNBALANCE COMPOSITION UNBALANCE COMPOSITION UNBALANCE COMPOSITION UNBALANCE COMPOSITION UNBALANCE UNITY UNBALANCE UNITY UNBALANCE U	1 18 18 18	3 1 3	8	ž	83	82	82	82	8	82	<u>8</u>	X	23	8 1	- 1	138	135	83	<u>ਲ</u>	133	138	83	£26		88		45		IRCHOSED [mohl	WING SPEE
MILEPOST MILEPOST THEFTABLE CURNE GEOMETRY UMBAJA	2 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2	8	<u>.</u>	82	8	2	8	8	83	28	8	8	2 :	9	110	110	110	9	110	8	8	128		88		45			= "
MILEPOST THINETABLE CURVE GEOMETRY MILEPOST THINETABLE LOCATION DEGREE SUPPRELEIA AVER LOCATION DEGREE SUPPRELEIA AVER LOCATION LOCATIO	5.0 6.0 2.0	30	9.3	3,3	46	4.9	07	4.6	2.5	63	2	3	3.9	0 v	80	62	5.8	ះ	28		2	83	5.3		0.5		22		(inches!	200
MILEPOST TIMETABLE CURVE GR	1 7 8 8	Ñ	8.8	8 N	26	ਜ	32	3.5		Ž	33	3.3	26	97	9 0	7.2	5.3	8.6	8.	9.	7.0	78	29		0.5		22		Average Inchesi	UNBALA
MILEPOST TIMETABLE CURVE OF CURVE OF LUCATION DESCRIPTION DESCRI	55 55 55 55 55 55 55 55 55 55 55 55 55	78.	839	282	452	6.63	5.01	808	5.4 0	5.31	5.97	3.07	***		231	38	S83	8	012	240	88	860	4.54		4.45		1.75		firches!	OMETRY
136.00 134.50 WASHINGTON TERMINAL IS AN IS 19 134.50 134.50 WASHINGTON TERMINAL IS AN IS 194.50 133.00 AVENUE to MILEPOST 133.0 134.50 133.00 AVENUE to MILEPOST 133.0 133.00 99.80 MILEPOST 133.0 to FREDERICH 133.00 133.70 Curve at Lancover 133.00 133.70 Curve at Lancover 133.00 133.71 Curve at Lancover 133.00 133.71 Curve at Lancover 133.00 133.71 At curves 134.00 134.71 At curves 135.00 135.00 At curves 136.00 136.00 At curves 137.00 137.00 At curves 138.00	0.0 1.06 0.20	3	2.	. •	99.	28.0	80	0.87	0.07	0.67	28.	85.0	0,82	22.5	82	8	8.	1:10	0.18	0.37	0.97	0.35	99.0		0.97		2.80			5
135.00 135.00 135.00 133.00 133.00 12	Curve at Winama		Curve south of MP 106.0						Alcanes 4P 110.0 to 4P 118.0		_										Curve at Landovec	Curve at Landover		MILEPOST 133.0 to FREDERICK ROAD		AVENUE to MILEPOST 133.0		WASHINGTON TERMINAL 16 AVENUE	DESCRIPTION	TIMETABLE
	103.86 103.85 102.86	10 10 10 10	106.48	28 12	110 f8	11071	1197	13.78	115.16	116.27	11872	17.61	1	98 E	8 2 3	182	28.83	138.67	27.18	au	28.52	22 83	129.28	99.86	18334	133.00			5	ost
and the control of th	\$ 1000000000000000000000000000000000000	7. 10. 10.	105.83	8 8	9	æ ₹	1361	11.39	115 82	118.67	#	17.7B	11837	S 5	922	<u>x</u> 8	438.28	138 38	177 26	127.14	28	×	• •	133.00	133.91	134.50	136,19	136.00	3	
CV# TRK ALL TRACKS 415. 2 1FACK # 2 416. 2 416. 2 416. 2 417. 2 4	0 2 2	٠ ٨	~ <u> </u>		7	.		~		Y			. .	94. 234.	?		2		Perof.	S.	.		100		2	3K#2	.2		<u> </u>	i

1 Page 1 of 7

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WAS to NYP .

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

		TIMETABLE	מחצוג	CURVE GEOMETRY	UNBALANCE	ANCE	3	77. L	S	MAXIMUM
LOCATION DESCRIPTION	DESCRIP	ION.	DEGREE	SUPER-ELEV	Average	LIMITING	CURRENT	PROPOSED (mohit	INCREASE (mohi)	LINE SPEED
99.80 MILEPOST 133.0 to FREDERICH	33.0 to FREDERIC	K ROAD (continued)								125
101.45 First curve south of MP 101.0 100.20 First curve south of MP 100.0 99.81 First curve south of MP 100.0	th of MP 101.0 th of MP 100.0		1.02 0.20 1.12	4.80 0.75 3.91	14.	7.3 1.4 9.0	125 125 100	138 128	8 - 8	
98.10 FREDERICK ROAD to FULTON	ROAD to FULTON									80
89.38 First curve north of Frederick Road Station 88.18 First curve south of Bridge	th of Frederick Road Sta th of Bridge	iton at Section 18	1,75 3.75	436 4.77	3.5	. 4.2 5.3	. 75 50	98 98	ے 5 10	
94.60 FULTON to NORTH PORTALS OF	VORTH PORTALS OF	F UNION TUNNEL								TIMETABLE SPEED
97.63 Curve at Fulton 97.38 96.94 96.71 96.70			4.22 0.80 7.52 7.67	1.65 010 185 1.88 0.36	3.1 2.8 3.1 2.4	3.8 0.5 3.2 3.6	3 8 8 8	5 % % %		
91.70 NORTH PORTALS OF UNION TUN		JNNEL to BAY								09
9124 First curve north of Union Tunnels 9182 Curve at MP 94.0 92.85 91.86 Reverse curves at Bey Infertocking 91.82 Reverse curves at Bey Interlocking	th of Union Tunnels 4.0 e et Bay Inferlocking e et Bay Interlocking		5.00 4.20 2.05 1.90	258 4.53 2.88 3.04 0.85	62 61 23 1.7	2.7 2.7 2.7 1.9	48888	3 2 2 2 3	v 5 0 0 0	
85.00 BAY to MILEPOST 85.0	POST 65.0				-					110
90.38 86.40 86.40 86.03			280 280 280 280	2.40 3.68 4.80 5.47 6.30	0.6 0.7 2.2 1.4	1.5 1.5 2.3 3.1 2.4	100 110 110 110	61 61 65 65	0 0 0 0	
71.50 MILEPOST 85.0 to BUSH	55.0 to BUSH									125
90.51 19.57 77.59 First curve modifi of Gurpow 77.57 First curve south of Megnote 77.57	th of Garpsow th of Magnothe		8 8 2 8 8 8 8 2 8 8	2.19 1.38 6.22 1.88	0.8 1.5 7.1 1.1	0.9 2.9 2.1 1.1	ឆ្ឆស្នស្	ទទួសស្សស	000%00	

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NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

Eastbound

WAS to NYP

1		UII EDOCT	THETACHE	S BVE	1 CHEVE ACOUSTON		INDAI ANCE	19E	CHIDAING COCCAC	2	MAVIMILI
-		3		1	CCMEIN			3	THE OFFICE	3	EDEISCE
Ĕ		LOCATION	DESCRIPTION	DEGREE	<u>~</u>	AVERAGE	CIMITING.	CURRENT	급 급	2	CINE SPEED
ı			~~	(000000000	Incresi	INSTANT	inchesi	imomi.	ingui.	(MODI)	imomi
RACK#21	7. 8.	60.70	BUSH to GRACE								125
100	71.30	72.69	Curve north of Bush	0.27	2.85	1.0	3.5	27 ·	135 1	0 (
- 989002	5 8 8 8	2 S		8 8	5.87	3 .	90	91	<u> </u>	- *	
Sec. 3.	1828	1029		990	83	28	9	83	<u> 18</u>	0	
8	61.35	80 45	First curve south of Grace	0.72	1.17	3.9	6.1	8	100	9	
TRACK#2	60.70	59.70	4								06
TRACK#2	59.70	28.30	SOUTHWARD LIMITS OF PERRY to YARD								125
₹.	27.90	57.69		0.45	1.75	32	4.2	110	125	15	
١.	•	58.7		_	6.07	8.0	8.7	8	5		
1	₹1.¥6	53.61	Curves MP 53.0 and 1,000 feet south of MP 54.0	8	291	28	3.4	100	133	12	
9000	8	R 3	Curves MP 53.0 and 1,000 fast south of MP 54.0	- 12	602	62	7.3	110	<u> 88</u>		
64	2819	51.14		6.75	534	29	4.3	1 28	-18 -18	•	
3	8	88	(Curve at MP 50.0	96.	5.83	7.9	1.0	8	8	ജ	
8093	S) (S)	2987	Consultation 46.0	980	29.9	9	5.5	110	8 2	15	
eri di	18 2	£13 4	Curre at MP 47.0	0.92	5.80	4.2	3	115	-128	9	
Sec. 3	68.85	92 92		80	886	7.7	3.1	82	8 8	•	
CAR.	507	28 9		ĸ	1.18	9:	9.	83	83	.0	
86 S	1614	# TE		0.38	238	1.8	3,	83	- 23	0	
:	9 9	83 83	First curve south of Davis	0.55	262		7	1 0	83	22	
8 × × * *	8	38 80		80	0.75	**	**	8	<u>8</u>	•	
	오 용	878		8	258	•		82	33	•	
. Se (c.)	12.00	3328		8	282	26	32	R		0	
46	8 8	32.68	Curve north of MP 33.0	18	5.73	5.8	7.0	110	8	10	
WX	8	30.85		0.48	284	2.4	9	83	. 23	•	
17.7.5	88	2000	Curve at MP 30.0	8	9 19	3	63	2	8	•	
100	2882	20.85		0.27	0.30	22	3.2	88	<u> 18</u>	0	
200	8			4.0	05.0	97	9	8	<u>8</u>		
± ⊜	88 -		28.00 (Curve at MP 29.0	280	3	; -	200	10	8	•	

WAS to NYP

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

E	品															_							T						
MAXIMUM	LINE SPEED	fmohl	80		8	80		110										90					5						
CURVING SPEEDS	CURRENT PROPOSED INCREASE	[thotal] [thotal]		45 5			9 5		110 5		110 0		0 011			0 01				0 06	0 06	88		0 001					82
3	CURRENT	fmohl		40			07		- 105	8	110	110	110	110	110	110	110		8	8	8	8.8		100	82	8	8	8	8 8
SKCE.	LIMITING	(inches)		4.9			5.4		3.7	7.	0	25	3.8	27	2.7	3.5	3.7		° 0.4	9 0	۲:	883		23	33	4.1	60	6.	6.
UNBALANCE	AVERAGE	[inches]		4.9			5.0			S	2.6	1.9	20	20	20	28	3.1		~~>0	0.4	70	1.9		1:8	1.9	3.6	4.2	7	0;
DMETRY	SUPER-ELEV	[inches]		0.01			1.76		191	8	4.18	X 0	3.47	920	0.58	38	5.54		0.75	0.78	217	282		623	524	3.33	204	388	7.7
CURVE GEOMETRY	DEGREE S	(dec degrae)		3.48			4.77		0.43	8 .	0.00	0.27	0.72	80	80	201	1.02		0.20	83	0.4S	0.80		1.8	18	8	1,82	8	8 8
TIMETABLE	DESCRIPTION		YARD to BRANDY	Curve at MP 27.0	BRANDY to WINE	WINE to LANDLITH	Curve north of Wilmington Station	LANDLITH to HOOK		First curve south of Bell								HOOK to BALDWIN					BALDWIN to MILEPOST 3.0			Reverse curves between Britt and Sharon Hitt	Reverse curves between Drift and Staron Hill	Reverse curves between that and Sharon Hall	
MILEPOST	LOCATION		27.00	26.98	26.80	0 25.50	9 26.17	0 16.50	1118 2	8 22	7 2122	8 228	3 2088	5 2021	0.00	7 19.51	8 17 <i>07</i>	50 11.50	0,810	15.00	1891 4	20 13 13 13 13 13 13 13 13 13 13 13 13 13		2 60.45	3 94	E. 6.78	909	88 0	22
		1	28.30		27.00	26.80		8	25 12	20.78	22	87 X	8 7	8	88	19.87	18.48	2 16.50		5	2 4697	2 23		2 11.02	este. veni	72	8	8	ਲ ਨ
-	CW	4	TRACK#2	328 2	TRACK#2	TRACK#2	327 2	TRACK#2	338	×	°	322	2	200.2	₹	7	316	TRACK#2	120	317	316	315	Š	313	312	311	30	<u>``</u>	7 ? 2 ? 8 %

NATIONAL RAILROAD PASSENGER CORPORATION

Eastbound

X-2000 Proposed Revenue Service Speed Profiles

(125 mph Maximum Speed)

			<u> </u>		\Box				_		7	
MAXIMUM	LINE SPEED	[mah]	TIMETABLE SPEED		70		09		70		110	
8	INCREASE	fmohl		000000000000000000000000000000000000000		0		0000		5		885555
CURVING SPEEDS	CURRENT PROPOSED INCREASE	[wow]		5588488855		∴70		8888		≥ 02		8 8 2 2 2 <u>2</u>
2	CURRENT	(moh)		55885388855		02		8888		8		8 8 <u>8 8 8 8</u>
NCE	LIMITING	fachest		2.7 2.6 2.7 4.3 5.9 0.1 2.4 2.4		. 29		3.6 2.2 0.7 1.9		4.9		88 98 22 3.7 3.3
UNBALANCE	AVERAGE	finches		21 22 86 86 51 5.1 -1.0 -0.8 22 28 7.2		2.4		30 1.8 0.3		3.7		77 178 88
METRY	SUPER-ELEV.	Inches!		2.78 5.20 3.00 0.21 1.70 1.34 0.78		3.74		202 1.82 1.88		90'9		24 4 4 4 8 8 8 3 4 4 4 4 8 8 8 8 8 8 8 8
CURVE GEOMETRY	DEGREE	dec decree!		1.42 2.50 2.05 4.70 4.78 6.07 0.97 2.80 6.35 0.085	Y	1.78		2.00 1.42 6.87 1.00		2.55		8 8 8 8 8 8
TIMETABLE	DESCRIPTION		MILEPOST 3.0 to EASTWARDLIMITS OF ZOO	All curves between 34th St. OH Bridge & Pern M. Signel loc All curves between 34th St. OH Bridge & Pern M. Signel loc All curves between Zoo and 34th St. OH Bridge All curves between Zoo and 34th St. OH Bridge	EASTWARD LIMITS OF ZOO to NORTH PHILADELPHIA		THROUGH NORTH PHILADELPHIA INTERLOCKING	Curve at west and North Philadelphia Sta. platform Curve at east and North Philadelphia Sta. platform	NORTH PHILADELPHIA to SHORE	Curve MP 84 to 2nd Street OH Bridge	- 6	Curve between Shore and Ford Curve eastward from Ford
MILEPOST	LOCATION		88.75	286 234 196 114 067 88.78 88.44 87.77	85.50	68.31	84.50	85.27 94.89 84.84 84.70	50 82.00	8009	- 1	8137 8089 7819 78.20 78.68
E			3.00	204 204 231 1.56 1.23 0.88 88.99 88.73 (97.52 67.23	86.75	88.45	85.50	88 88 28 28 88 88 28 75	64.50	Н	ŀ	2 2 2 2 2 2 2 3 4 4 4 4 4 4 4 4 4 4 4 4
-	C		ALL TRACKS	300 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TRACK#2	303	TRACK#2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TRACK#2	2 882	ٳڎؚ	22222 2222

X2RV125E.XLS

WAS to NYP

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles

(125 mph Maximum Speed)

LOCATION DESCRIPTION DEGREE SUFFER-ELEV.	ॖ 🗆	UNBALANCE AVERAGE LIMITING	CURRENT PROPOSED INCREASE	MAXIMUM LINE SPEED
(dec decree)		finches! [inches] [inches]	fmohl fmohl	luopj
58.40 MILEPOST 76.0 to MORRIS				125
0.75		3.6 3.4 5.4 5.4	125	
74.0 and MP 75.0		6.00 8.3 8.8 80	115 23	
74.05 Reverse curves between MP 74.0 and MP 75.0		5.49 6.2 8.7 80	115 23	
7.18		204 1.8 1.8	- R	
70.08 Claime weed of Chaydon			82	
		1.3		
		26 33	- 133	
86.02 Curve west of Grundy 0.73		4.1 6.2	125 10	
64.83 Curve exect of Grundy	8.5	3,71 3.4 4.1 120	38	
6136 Curve behvoor UP 610 and UP 620	0.72	27	128 - 15	
0.35	80	22 31	125 15	
58-05 First curve west of Marris 0.58	95.0	1,72 4.6 6.5 110	125 15	
54.00 MORRIS to MILEPOST 54.0				110
58.00 [Morris Interlocking		001	100 001	
5674 Presque vest of Trentan	28'0	2.61 5.2 6.0 110	110 0	
1860° 0.32	0.32	1:37 1:3 2:3 1:10	110 0	
25,00 MILEPOST 54,0 to MILEPOST 28.0				125
(A.35)	0.32	21. 1.7. 1.7. 1.25.	125	
200	020	32 1.6 25 1.3	83	
250 D22	220	3.6	.0	
23.1 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4	0.47	21 28		
33.1		2.73 2.2 3.3 1.25	125 0	
	<i>1</i> 00	2.6 3.8		
	0.28	1.87	0 22	
20.00 MILEPOST 28.0 to MILEPOST 20.0				110
27.45 Third curve west of Lincoln 0.77	220	3.83 2.7 3.1 110	0 0tb	
26.75 Second curre west of Lincoln	ę.	5.89 6.5 7.2 90	450 SP	
First curve west of Lincoln	1.67	6.1 6.5) (
	3	no no	110	
FIRE CARVE WEST OF MIP 24.0	35	8	110 82	
22.66 FIREGING CORT OF MP 24.0	9	1 00 1	5 8	

Eastbound

NATIONAL RAILROAD PASSENGER CORPORATION

WAS to NYP .

X-2000 Proposed Revenue Service Speed Profiles

(125 mph Maximum Speed)

THETABLE CUING GEOMETRY UNBLAMOR CUING GEOMETRY UNBLAMOR CUING GEOMETRY UNBLAMOR CUING GEOMETRY CUING GEOME	The FLORE CHINE GEORGE STERRED AND MALANCE CHINE GEORGE LIMING CHERT INCRESS NATIONAL	Name	MAXIMUM	LINE SPEED	ido Ido	110						125		_			110					-		TIMETABLESPEED							_				
NULEPOST 28.0 to BLANCK CURNE GEOMETRY UNBALANCE CURNANS SPEEL MARCH CURNAL SPEEL MARCH CURNAL SPEEL MARCH CURNAL CU	Post	Null-POST THUETABLE CUINNA SPEEL CUINNA SPE	HAX	EN I	Ŋ	1				_		_					-							TIMETAL									_		
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TIMETABLE CURVE GEOMETRY UNBALA MILEPOST 28.0 to MILEPOST 20.0 (continued) MILEPOST 28.0 to ELMORA MILEPOST 28.0 to MILEPOST 28.0	Time Cultive GEOMETRY UNBALA UN	MILEPOST MILEPOST 20.00 MILEPOST 20.0 (continued) MILEPOST 20.0 MILEPOST 20.0 (continued) MILEPOST 20.0 MILEPOST 20.0 (continued) MILEPOST 20.0 (continued	뜅	CURRENT	qouj		110	010	2 :	2 5	2 9		125	- 23	8			æ	18	8	310	e .	29		2	×	×	8	8 8	.	8	8 8	8	75	
MILEPOST 28.0 to MILEPOST 20.0 (continued) MILEPOST 28.0 to MILEPOST 20.0 (continued) MILEPOST 28.0 to MILEPOST 20.0 (continued) O.78 4.72 1.1 O.89 4.33 2.24 2.24 2.24 2.24 2.24 2.24 2.24	CURPOE GEOMETRY TIMETABLE CURPOE GEOMETRY Average CURPOE GEOMETRY Average CURPOE GEOMETRY Average Curpoe Curp	#1 LOCATION MILEPOST 28.0 Fig. 1987 2. 23.95 22.85 2. 23.95	焸	LIMITING	finchesi		3.3	3.0			29		27	30	6	· 0.0			3.5	3.	*:	9.0	1.8		5.5	₽ 0	60	0.5	0.7	0.	22	0.	13	5.8	7 / The state of t
MILEPOST 28.0 to MILEPOST 20.0 (continued) Continued) Continued) Continued Conti	Time Curve Geometry Curve Geometry	RILEPOST WILEPOST 28.00 CURVE GEOMETRY CONTRICTOR CURVE GEOMETRY CONTRICTOR CONTRI	CNBAL	WERAGE	[inches]		1.9	*	7,7	3 -	9		1.7	•	.	25			3.3	2.7	*	90	9.8		2.9	0.2	7		50			03 80	6.0	3.8	
TIMETABLE CURVE GEOGRAPHICAN DEGREE	POST TIMETABLE CURVE GE	WILEPOST TIMETABLE CURVE GREEN	ETRY	2	-		4.72	433	\$;	3 2	 88 88		1 85	S S	7	0.75			2.68	69.	o.73		2.74		05:0		0.0	2 2 2	8		8	<u>्</u> ४८ १८	101	4.12	
MILEPOST 28.0 to MILEPOST 20.0 (continued) MILEPOST 28.0 to MILEPOST 20.0 (continued) MILEPOST 20.0 to ELMORA ELMORA to HUNTER Emora Interiodating Curve east of Emora First curve west of MP 14.0 Curve at Hariter HUNTER to PENNSYLVANIA STATION, NEW YORK Curve west of the west portal North River Turnels Curve west of the west portal North River Turnels	TIMETABLE TIMETABLE TOWN TOWN	#2 28.00 20.00 MILEPOST 28.0 to MILEPOST 20.0 (continued) 2 7256 2266 2 7256 7256 7256 2 7256 7256 7256 2 7256 7256 7256 2 7256 7256 7256 2 7256 7256 7256 7256 7256 7256 7256 725	JIRVE GEOM	\vdash	╛		0.78	880	3 E	600	340		0.32	240	020	0.30			2.37	38 .	0.25	Z Z	22.		81		8	16	290	190	22	* 	0.47		
		MILEP MILEP 2 28.00 2 27.64 2 27.65 2			7	MILEPOST 28.0 to MILEPOST 20.0 (continued)						MILEPOST 20.0 to ELMORA					- 1			First curve west of MP 14.0			Curve at Hunter	HUNTER to PENNSYLVANIA S								Portal Manable Bridge		Curve west of the west portel North River Tunnels	

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PREPARED BY: Conrad J. Ruppert, Jr. Mgr. Field Engineering

WESTBOUND - TRACK NO.3 New York, NY to Washington DC

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Westbound

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles

NYP to WAS

(125 mph Maximum Speed)

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4,120 2.6 3.2 65 70 5 4,580 1.5 1.9 55 60 5 0,750 2.8 2.8 125 0 1,500 2.7 2.7 175 125 0 1,300 2.7 2.7 175 0 0 1,300 2.7 3.4 110 110 0 1,100 1,4 2.2 110 110 0 2,500 2.8 3.9 110 110 0 3,500 2.0 3.0 110 0 0 5,570 2.0 3.0 110 0 0 5,570 2.0 3.0 110 0 0 5,570 2.0 3.0 110 0 0 5,570 2.0 3.0 110 0 0 0 5,570 2.0 3.0 110 0 0 0 0 </td
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5.130 7.6 7.9 90 110 4.290 6.7 6.8 65 110

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NATIONAL RAILROAD PASSENGER CORPORATION

X-2000 Proposed Revenue Service Speed Profiles
(125 mph Maximum Speed)

MAXIMUM	LINE SPEED	fmohl	110				126							110				125				•			·					
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SOS	INCREASE	fmohl		R	8	· 0		0	0	0	ø	<u>.</u>	٥,		0	52	٥		9 1%	2	2	3	\$	10	•	R	•	ĸ	18	
CURVING SPEEDS	PROPOSED	fmohl		2 01	10	110		125	8	23	<u>8</u>	8	ž ;	3	110	110	8		135	82	8 2	<u>x</u>	83	<u> 8</u>	8	8	138	115	115	
ਤੋ	CURRENT	[thom]		80	06	110		125	83	83	83		125 25	3	110	8	100		110	01	91	-10	8	115	**	8	125	8	8	
ANCE:	LIMITING	finches		9.4	2	33		0.5	2.7	20	2.9	87			21	3.6			62		2.5	30	3.7	•	3	82	3.1	7.9	9.6	各名 衛用人以及不
UNBALANCE	AVERAGE	[inches]		8.7	6.1	2.8		0.5	6:1	9	5.	6	- C	3	12	32			~~~~	£3	2:	P.	27	32	3.5	6.2	2.4	7.8	6.2	CO. C. C. CO. CO.
METRY	SUPER-ELEV.	[inches]		6.190	000 g	3,900		1.680	2890	300	3230	.	ş (1,200	2.510			3.680	0830	8	28.¥	4.180	8	3	5.330	1.680	5.820	5.330	
CURVE GEOMETRY	DEGREE	féec degreel		1.83	27	0.77		0.20	0.63	.	8	030			0.28	890			0.77	0.17	8 .0	£.0	80,0	57.0	80	8.	0.37	34.	54.1	· · · · · · · · · · · · · · · · · · ·
TIMETABLE	DESCRIPTION	7	MILEPOST 20,0 to MILEPOST 28.0 (continued)	First curve west of Lincoln	Second curve west of Lincoln	Third curve west of Lincoln	MILEPOST 28,0 to MILEPOST 54.0							MILEPOST 54.0 to MORRIS		First curve west of Transon	Monts Interlocking	MORRIS to MILEPOST 76.0	First curve west of Marris			Curve between MP 61.0 and MP 62.0	Curve east of Grundy	Curve west of Grundy		Cure west of Craydon		Reverse curves between MP 74.0 and MP 75.0	Reverse curves between MP 74.0 and MP 75.0	
MILEPOST	LOCATION		20.00 28.00	26.40 28.67		27.46 27.87	28.00 54.00	28.67 29.07	30.25 30.65				92.04 T-92.	- 188	56-10 68-33	57.12	58.40	58.40 76.00	58.41 59.06	59.44 59.60		91.40 OF 94	B162 6498		68.72 67.85	da 70.60	2.19 7260	74.08 74.50	74.66 75.09	2000年の日本の大学の大学
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	# # # # # # # # # # # # # # # # # # #		TRACK#3	: 882	3900; 8860;	270	TRACK#3	Z)		00 30	32		ĸ	18	3118	612		TRACK#3		Ä	R	æ	Ř	æ	<u>*</u>	8	&	8	8	

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NATIONAL RAILROAD PASSENGER CORPORATION

Westbound

X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

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MAXIMUM	LINE SPEED	ldami	110							70		09					70		CURRENT TIMETABLE					100	
8	INCREASE	fmant		10	2	2	•	ક	8		S		0	6	•	· 0 ·		01		·	0	0	00		c 2 2 2 c c
CURVING SPEEDS	CURRENT PROPOSED INCREASE	(moh!		110	9	\$10	- -	88	2		70		8	8	8	.		0.0		96	Ş	8	2 Z		888888
ਤ	CURRENT	fmohl		91	8	8	8	8	ଝ		8 8		8	8	8	8		80		30	\$	ន	RR		88888
UNBALANCE	LIMITING	finchest		3.4	\$ \$	82	87	9.7	9.5		3.9		2.8	.0	25	3.1		2.4		4,4	4.2	60	2.8 1.8		1.7 50 53 2.4 3.5
UNBA	_	finches		2.4	2.9	1 26	7	8.6	8.7		3.3		23	4.0	9	2.5		1.8		2.7	3.5	90	23		31312X
OMETRY	SUPER-ELEV.	finchesi		3.480	2730	8	्र • • • • • • • • • • • • • • • • • • •	2.470	5.320		5.190		0880	2.370	1,520	2.300	CKING	3,440	(MP 3.0)	0.340	1.340	282	6.130 3.180		2,480 3,410 2,440 5,860 4,380
CURVE GEOMETRY	DEGREE	[dec decree]		0.70		0.35	000	1,75	4.10		2.47		127	080	1.37	1.80	OO INTERL	1.52	S OF PENN	\$8.4	4.32	202	2.47		889 101 102 103 103 103 103 103 103 103 103 103 103
TIMETABLE	DESCRIPTION		MILEPOST 76.0 to SHORE					Curve eastwict from Ford	Curve between Share and Ford	SHORE to NORTH PHILADELPHIA	Curve MP 84 to 2nd Street OH Bridge		Curve at east end North Philadelphie Station platform		Curve at west and North Philadelphia Station platform		NORTH PHILADELPHIA to EASTWARD LIMITS OF ZOO INTERLOCKING	86.38 Curve at Bridge 86.11 (Ridge Ave.)	EASTWARD LIMITS OF ZOO to SOUTHWARD LIMITS OF PENN (MP 3.0)	All curves between Zoo and 34th St. OH Bridge	All curves South St. OH Bridge to Signal Br. 2.0-2.1	All curves South St. OH Bridge to Signal Br. 2.0-2.1		MILEPOST 3.0 to BALDWIN	Reverse curves between Brill and Sharon Hill Reverse curves between Brill and Sharon Hill Reverse curves between Brill and Sharon Hill
MILEPOST	LOCATION		76.00 82.00	76.13 76.47	าลาด กาณ	78.21 78.50	78.20 EM		81.39 81.79	82.00 84.50	83.16 83.84	84.50 85.50	64.74 84.81		1000 2514	85.38 65.49	85.50 86.75	17.98	86.75 3.00	87.68 89.76	-	8	231 2 2 224 305	3.00 11.50	3.16 3.24 5.38 6.02 6.09 881 6.8) 7.22 9.41 8.05 11.04
	C¥ TRK		TRACK#3	283	्र	 %	٠ 3	3	33	TRACK#3	299 3	TRACK#3	299 M 3	2000	36	302 3	TRACK#3	300	ALL TRACKS	7 Z EOE			306 3 307 3	TRACK#3	306 K 3 306 K 3 312 3 313 3 313 3

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NYP to WAS

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

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		MILEPOST	IMEI ASIE	3	CMETRY	UNBALANCE	ANCE	B	CURVING SPEEDS	8	MAXIMOM
\$	¥	LOCATION	DESCRIPTION	DEGREE	SUPER-ELEV.	AVERAGE	LIMITING	CURRENT	PROPOSED	INCREASE	LINE SPEED
				free degreef	firchesi	finches	forhest	(moh)	[moh]	[thotal]	fmohi
TRACK#	(#3	11.50 16.50	BALDWIN to HOOK								06
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30									40		
ر و د				¥	989 0		3	3	8	- - - -	
31		15.80 15.95		620	8 8	0.0	 	8	8	0	
318		16.40 16.50		0.20	1.000	0.1	0.1	8	86	.0	
TRACK#	(#3	16.50 25.50	HOOK to LANDLITH								110
319	8	17.96 18.51		1.00	5.800	27.		110	110	0	
8				- 28	5.280	48	9	20	110	0	
300				92.0	980	00	00	0.1	910	•	
2 02				630	82	07		91	014		
Ş				Fe	3.440	3.6	7	9			
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3				3		9	0	2	110	5	
ž	S	294 2577	First curve south of Bell	9	4.820	0.7.	8	8	9	R	
83	•	24,20 25.16		0.42	2.030	9:	26	8	110	so	
TRACK#3	(#3	25,50 26.80									80
327	2	26.19 26.80	Curve north of Wilmington Station	3.42	1.210	3.6	3.8	45	45	0	
TRACK#3	(#3	26.80 27.00	WINE to BRANDY								30
327 M	3	26.88 26.80		1.37	0.580	6.0	9.0	8	œ	0	
327 N		26.99 26.97		1.10	0.320	0.4	0.1	30	30	0	
TRACK #	K#3	27.00 28.30	BRANDY to YARD								စ္ဆ
328	3	27.09 27.53	Curve at MP 27.0	3.95	2.960	2.6	2.9	45	\$	0	
TRACK#	£#3	28.30 59.70	YARD to SOUTHWARD LIMITS OF PERRY								125
828	. 3 ×	ଅଟେ ଅନ	Curve at MP 29.0	980	4 850	77	6.3	110	125	15	
8	?		Constant MP 30.0	8	6,230	899	8.5	9.	X 2	2	
ğ				77.0	3,530	9 2	2.8	8	8	٥	
8			Curve north of LIP 33.0	<u>.</u> 8	6.730	**	••	91	33	£5	
æ				80	2860	2.5	93	Ā	23	٥	
ౙౢ				Q	2080	23	33	<u> 8</u>	2 3	0	
æ			400	& 0	0.750	*	¥.	×	233	•	
8	9		First curve south of Davis	80	3110	7	3.5	<u> </u>	_ 125	•	
8	: :	# # # # # # # # # # # # # # # # # # #				20	**************************************	<u>8</u>	2	•	
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NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

Westbound

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MAXIMUM	LINE SPEED	Inoni 1	07			90	125		125		110	
8	INCREASE			0 0 8 8 8	• & & c & st			10 51 0 0		0 % 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
CURVING SPEEDS	CURRENT PROPOSED INCREASE	illioni.		8	ង់និងនិង			106 128 128 125		<u> </u>		01 10 10 10 10 10 10 10 10 10 10 10 10 1
8	CURRENT	luoui		8	ឆ្នេស្ន			8 83 5 53 53		មិន ខេង		011 012 013 014 003
UNBALANCE	<u> </u>	(manasi)		0.0 0.1 0.0 0.0 0.0	38 78 47 63 44			62 64 54 37 40		1.7 0.8 7.8 2.7 3.8		3.8 4.5 2.0 4.9 3.3
ANS	<u> </u>	in and a		27 4.4.4.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8.8	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9			3.6 3.3 4.6 2.3 1.6		1,7 0.0 0.3 1.6 2.2		27 28 17 28 23 23 23 23
CURVE GEOMETRY	SUPER-ELEV	incres.		1.780 3.620 6.040 4.800	5.780 2.390 0.500 6.130 1.590			2.110 3.760 5.960 3.350 1.440		0.500 0.46.1 0.48.0 0.48.0		5.360 5.380 3.840 3.480 0.780
CURVE	DEGREE	Nec decree	_ 4	0.22 0.57 0.85 0.83	0.00 1.12 0.50 0.30 1.37			0.77 0.05 0.97 0.52 0.28		0.25 0.25 1.17 0.35		0.05 0.05 0.47 0.37
TIMETABLE	DESCRIPTION		TAKD to SOUTHWARD LIMITS OF PERRY (Continued)	Curve at MP 47 0 Curve at MP 48 0 Curve at MP 50.0	many of the comment o	-	GRACE to BUSH	First curve south of Grace Curve north of Bosh	BUSH to MILEPOST 85.0	First curve south of Magnotis First curve north of Gurpow Mininocking	MILEPOST 85.0 to BAY	
KILEPOST	LOCATION	H	26.30 39.70	4401 4421 45.7 45.85 48.72 45.07 48.62 45.07 48.65 50.67			60.70 71.50	60.53 61.35 62.05 62.05 62.05 65.00 66.00	71.50 85.00	766 7380 7781 7707 7780 782 7648 762	85.00 91.70	66.73 86.37 86.62 88.16 86.41 86.73 86.77 86.83 90.16 91.03
-	TRK.	-	- 1		****	1						
-	***		IKACK # 3	2 2 2 2 X	933353	TRACK#3	TRACK#4	2222	TRACK#3	*******	TRACK#3	8 7 8 8 8 8

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NYP to WAS

NATIONAL RAILROAD PASSENGER CORPORATION X-2000 Proposed Revenue Service Speed Profiles (125 mph Maximum Speed)

ි Westbound

MILEPOST TIMETABLE LOCATION TIMETABLE CURNING CINETIEN MILEPOST TIMETABLE CURNING CINETIEN MILEPOST M	MAXIMUM	LINE SPEED	(mohl	90						CURRENT TIMETABLE		•			200			125														
MILEPOST TIMETABLE LOCATION TIMETABLE CURNING CINETIEN MILEPOST TIMETABLE CURNING CINETIEN MILEPOST M	¥									CURREN																						
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MILEPOST TIMETABLE LOCATION DESCRIPTION DESCRIPT	AVING SPEE	PROPOSED	fmohl		8	8	8	8	8		œ 🤻	8	8 8	} ₽		8	960		129 129	52	83	ĸ	X	3	X	R R	115	£ 3	3	9	8 ¥	1 2
MILEPOST MILEPOST THINETABLE L.C. HIPTING SECRETARY LOCATION COCCURRENT COUNTY GEOMETRY	ਣ	CURRENT	fmphi		₩.	8	8 :	8	45		8	8	8 8	3 8		જ	75		<u>\$</u>	202	25	110	8	110	95	9	8	X :	₹ :	R !	8 8	
MILEPOST MILEPOST TIMETABLE CURNE GEOMETRY Mile CURNE GEOMETRY CURNE GEOMETRY Mile C	LANCE	LIMITING	finches		11. J.	20	8	(F)	5.0		2.0	20) }	35		7.5			8.8			7	7.0	9		 8:	8.3	3	• • • • • • • • • • • • • • • • • • •	•		•
MILEPOST WILEPOST TIMETABLE CURNO ECONE Supering CURNO ECONE Supering CURNO ECONE Supering	J	Į.			0.7	7.		9	*		27	2.5	9.9	2.7		0.7			8.5		9.0	7	8.0	**	57 %	22	9.3	22	, ·	•	, e	•
# MILEPOST TIMETABLE DESCRIPTION # 1 91.70 94.60 BAY to NORTH PORTALS OF UNION TUNNEL. # 2 91.70 94.60 BAY to NORTH PORTALS OF UNION TUNNEL. # 2 92.00 22.22 Reverse curves at Bay Interfocking # 2 92.03 22.23 Reverse curves at Bay Interfocking # 2 92.03 22.23 Reverse curves at Bay Interfocking # 2 92.03 22.23 First curve morth of Union Tunnels # 2 92.03 92.10 NORTH PORTALS OF UNION TUNNEL to FULTON # 3 92.03 92.03 First curve morth of Union Tunnels # 3 92.03 92.03 First curve morth of Union Tunnels # 3 92.03 92.03 First curve morth of Union Tunnels # 3 92.03 92.03 First curve morth of Union Tunnels # 3 92.04 92.03 Curve at Fulton # 3 92.04 92.05 First curve south of MP 108.0 # 3 100.27 102.03 First curve south of MP 108.0 # 3 100.27 102.03 Curve about of MP 108.0 # 4 100.27 102.03 Curve about of MP 108.0 # 5 100.27 102.03 Curve about of MP 108.0 # 5 100.27 102.03 Curve about of MP 108.0 # 5 100.27 102.03 Curve about of MP 108.0 # 5 100.28	SOMETRY	SUPER-ELEV	[inches]		1.850	3.040	9	00€¥	3320		0.00	8	1510	- 2		2.820			3.360	0.500	4.320	8	\$ 500 500 500 500 500 500 500 500 500 500	0.550	2620	20 20 20 20 20 20 20 20 20 20 20 20 20 2	9	288	7700	6070	5740	. S
#3 91.70 94.60 BAY to MORTH PORTALS OF UNION TUNNEL. 9 12.00 20.20 Reverse curves at Bay Interfolding. 9 22.00 92.10 Reverse curves at Bay Interfolding. 9 22.00 92.10 Reverse curves at Bay Interfolding. 9 22.00 92.10 Reverse curve at Futton. 9 3 92.10 99.80 First curve at Futton. 9 92.80 133.00 FIRST curve south of MP 100.0 9 00.20 100.20 First curve south of MP 100.0 9 00.20 100.20 Red Red Red Reverse south of MP 100.0 9 00.20 100.20 Red Reverse south of MP 100.0 9 00.20 100.20 Red Reverse south of MP 100.0 9 00.20 100.20 Red Reverse south of MP 100.0 9 00.20 100.20 Red Reverse MP 110.0 MP 110.0 9 100.20 100.21 Red curves MP 110.0 MP 110.0 9 100.71 100.80 Red Reverse MP 110.0 MP 110.0 9 100.72 1113.10 Reverse MP 110.0 MP 110.0 9 113.10 113.10 M Curves MP 110.0 M D 110.0 9 113.10 113.10 M Curves MP 110.0 M D 110.0 9 113.10 113.10 M Curves MP 110.0 M D 110.0 9 113.10 113.10 M Curves MP 110.0 M D 110.0 M D 113.0 9 113.10 113.10 M Curves MP 110.0 M D 113.0 M D 113.0	CURVEG	DEGREE	[dec degree]		1.00	2.02		₽ :	4.43		\$8.	7.8	8.8	4.15		3.88	1.72		1.18	R	9.1	0.27	₽ :	26'0		90	2. 78.	0.47	B :) } }	2 5	5
## LOCATION ## 3 91.70 94.60 BAY to MORTH PORTALS OF ## 2 91.80 BAY to MORTH PORTALS OF ## 2 92.00 22.02 Reverse curves at Bay infentoclung ## 2 92.00 22.02 Reverse curves at Bay infentoclung ## 2 92.05 94.12 Curve at MP 94.0 ## 3 98.10 MORTH PORTALS OF UNION ## 3 98.10 MORTH PORTALS OF UNION ## 3 98.10 Curve at Futton ## 3 98.10 99.80 FULTON to FREDERICK ROAD ## 3 98.10 99.80 FULTON to FREDERICK ROAD ## 3 98.10 Gurve at Futton ## 3 98.10 Gurve at Futton ## 3 98.10 Gurve at Futton ## 3 98.10 Curve at Futton ## 3 98.10 Gurve at Futton ## 4 98.80 Tits to Fret curve acuth of MP 101.0 ## 5 102.00 Gurve at Wheate ## 6 103.00 Gurve at Wheate ## 6 103.00 Gurve at Wheate ## 6 103.00 Gurve at Wheate ## 7 104.61 Gurve at Wheate ## 104.71 Tito At Curve at Wheate ## 106.40 Gurve at Wheate	200			NNEL.						FULTON																	Construction of the Constr					
## MILEPOST TIMETABLE ## 3 91.70 94.60 BAY to NORTH PORTALS OF SECRETIFIED SE	<u>.</u>	*			9					TUNNEL &	10.00							DST 133.0									To Charles of Prince of S					
#3 91.70 94.60 9 91.87 82.00 9 92.00 82.42 9 82.06 94.12 9 82.06 94.12 9 92.00 92.42 9 92.00 92.42 9 92.00 92.00 9 92.	TIMETABL	DESCRIPTIC			Inferbocking	Intertocking		•	on Tunnels						RICK ROA	8	derick Road	to MILEPK	2 100.0		_0.101 €						2	997-017) MI JUN		MP 1580	up ith n
#3 91.70 94.60 #3 91.70 94.60 #3 91.70 94.60 #3 91.70 94.60 #3 92.00 92.72 #3 92.05 94.12 #3 92.06 98.10 #3 92.06 98.10 #3 92.08 98.10 #3 93.10 92.10 #3 93.10 93.10 #3 93.10 #3				FORTH PO	urves at Bay	urves at Bay			s north of Un	PORTALS				-uffor	to FREDE	e south of Br	s north of Fire	LICK ROAD	e south of M		E SOUTH OF IN						ath of MP to	A CONTRACT			10015-011	II Grove MP 110 to MP 118 0
#3 91.70 94.60 9 91.87 82.00 9 92.00 82.42 9 82.06 94.12 9 82.06 94.12 9 92.00 92.42 9 92.00 92.42 9 92.00 92.00 9 92.			į	BAY to I	Reverse c	Reverse			First curv	NORTH				Cirs at	FULTON	First cury	FIRECUS	FREDER	Firstour		First Cury		******				Cure so					
	TSOS	NO									85.48	रू 88	23.25	8 8 5			86.03	133.00		98.90 1	102.10	100	2,8	5 5	22	8 8	58.95 26.95	8 5		•	3	148
	E	0		91.70	91.87	8 8	38 1	8 8	82	94.60	8.28	28 33	88 7 86 E	8	8.5 5.	98 19		99.86	89.B3	8 8	<u>5</u>	8	8	<u>8</u>	2	2	58.45 45	8 8			2 2	į
		1RX		TRACK#3	3	•	2		3	ALL TRACKS		6			TRACK#3	3	322	TRACK#3	9	es V		~	_	7	(a)		e .				, (n)	

NATIONAL RAILROAD PASSENGER CORPORATION
X-2000 Proposed Revenue Service Speed Profiles
(125 mph Maximum Speed)

MILEPOST	150	TINETABLE	CURVE GEOMETRY	CURVE GEOMETRY	UNBALANCE	ANCE	3	CURVING SPEEDS	8	MAXIMUM
LOCATION		DESCRIPTION	DEGREE	SUPER-ELEV.	AVERAGE	LIMITING	CURRENT	CURRENT PROPOSED INCREASE	INCREASE	LINE SPEED
			[dec degree]	finches!	finches	(inches)	[moh]	(mohi)	fmohl	fmohl
99.80 133	8	133.00 FREDERICK ROAD to MILEPOST 133.0 (continued)								125
116.78 11	#	117.46 Att curves MP 110.0 to MP 118.0	0.83	6.050	3.0	**************************************	120	125	9	
117.58 T	*	17.74 Attaine MP 110.0 to MP 118.0	0.65	3,910	7	→	8	8 2		
118.10	1 0	1634 First curve south of MP 118.0	0.0	5.89	25	38	8	82	•	
119.10	886		8	220:	36	\$		8	0	_
13861	202	12024 Curve south of MP 120.0	0.82	9829	17	2,7	813	8	9	
12188	8072		88	- 88 -	•	1	110	×	55	
£8.83	8		8	6.180	20	88	110	8	ž.	
1389 1	88.82		860	6200	5	5.2	110	73	5	
13854	2882		1.12	889	83	68	110	83	13	
17.44	10180		0.42	2.10	2.5	3.0	94	83	\$	
138.57	Z	CARPI Curve at Landons	800	272	3.0	6.2	8	82	18	
	13068		0,68	4.540	2.9	4.0	125	8	d	
133.00	34.50	133.00 134.50 MILEPOST 133.0 to AVENUE								85
414 3 133.34 133.91	133,91	A ROBERT BOOK STORY OF THE STOR	26.0	4.450	0.6	1.5	88	98	0	
134.50	36.00	134.50 136.00 AVENUE to WASHINGTON TERMINAL								CURRENT TIMETABLE
415 3 134.02 136.19	136.18		2.80	1.760	22	3.0	\$	3)	0	

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