



**UP 5802  
(AC44CWCTE – GE)  
Locomotive Noise Test Battery  
Report**

**CONTRACT NUMBER**

**FR-TEC-0003-11-01-00**

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## Table of Contents

Project Detail: .....	1
VSWR Test.....	5
TABLE A VSWR Plots.....	6
Insertion Loss .....	10
TABLE B Insertion Loss Plots .....	10
Antenna Isolation Test .....	12
TABLE C Antenna Isolation Plots .....	13
TABLE D Antenna Isolation Chart.....	37
Receive Intermodulation Test.....	53
Transmit Intermodulation Test.....	61
EMI Testing .....	65
BER Testing.....	80
TABLE E BER Test Results .....	81
Locomotive run through Stevens Pass.....	82
Summary: .....	89



**Project Detail:**

Contract Number	FR-TEC-0003-11-01-00
Dates of Survey	December 5 <sup>th</sup> to 16 <sup>th</sup> , 2011
Locations	BNSF Delta Facility Everett WA 47.99965 N LAT,-122.186202 W LON, elev. 31 ft
Test Engineers	Ramon Abelleyro, Derek Edmondson

The testing location for this locomotive was in Everett WA at the BNSF Delta yard. The locomotive was located on a siding near the entrance to the yard and was stationary throughout the testing period.



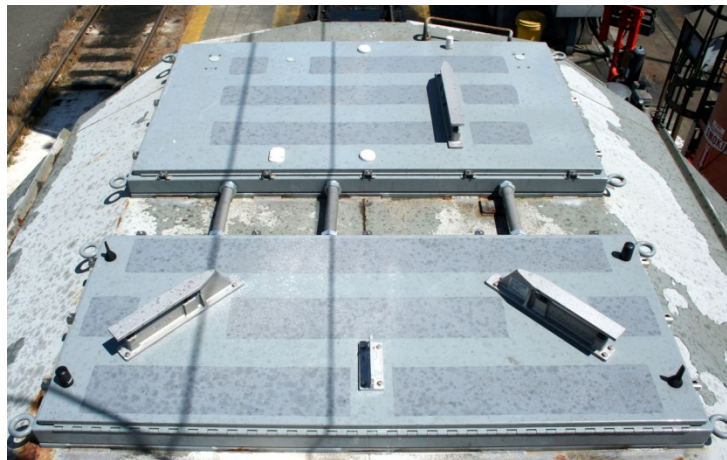
BNSF Delta Yard  
Figure 1



BNSF Delta Yard Testing Location  
Figure 2



Locomotive under test UP 5802  
General Electric C44-9-AC-CTE  
Figure 3



UP Antenna Array  
Figure 4

The antenna system was comprised of a UP designed “Hoffman Box” assembly. It included a single VHF, two Sinclair 220 MHz PTC antennas, three Sinclair UHF antennas for HOT, DPA, and DPB, LAIRD series 900 MHz antennas, and LAIRD series cellular antennas.



Sinclair EXCAL221-8952446 VHF  
Figure 5



Sinclair ST221-SF3SNF 220  
Figure 6



Sinclair ST321-SF3SUF HOT/EOT  
Figure 7



LAIRD PHANTOM TRAB8903  
Figure 8



LAIRD PHANTOM ELITE ETRAB8213NP  
Figure 9

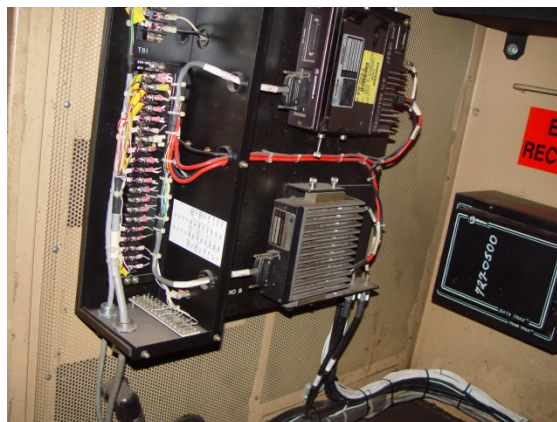


LAIRD PHANTOM TRA24003NP  
Figure 10

The radio systems included AAR Voice, distributed power radio assembly, a UHF HOT/EOT system as well as the YARD radio.



AAR Voice Radio  
Figure 11



Distributed Power Radio Assembly  
Figure 12



HOT/EOT Transmitter  
Figure 13



ATCS Yard Radio  
Figure 14



Mobile Data System  
Figure 15



## **VSWR Test**

This test is designed to collect VSWR data in several formats for use in locomotive noise and intermodulation reporting. The test involved collecting voltage standing wave ratio and return loss data in the following formats; VSWR, S1P scatter parameters, comma separated values, and a portable network graphics. It is important to know if the antenna system is properly matched to the transceiver equipment as this can be a source of intermodulation and/or standing waves in the RF system. The first set of data was collected at the RF port located closest to each antenna element in the locomotive radio frequency system to give an accurate picture of antenna matching. A second set of data recorded the VSWR at the end of the transmission line cable that connects to the radio transceiver antenna connector, including any installed filtering to show what the full system response is that is presented to the transceiver. This measurement includes all system losses.

This test helps us to characterize the band pass parameters of the antenna. The information is useful in determining how much the antenna element contributes to filtering out of band energy as well as whether or not the antenna is functioning correctly. The results from the VSWR testing indicated all antennas and associated components were functioning properly. The full data from this testing has been presented in Appendix A. Typical data recorded from the locomotive is presented in Table A below.

TABLE A VSWR Plots

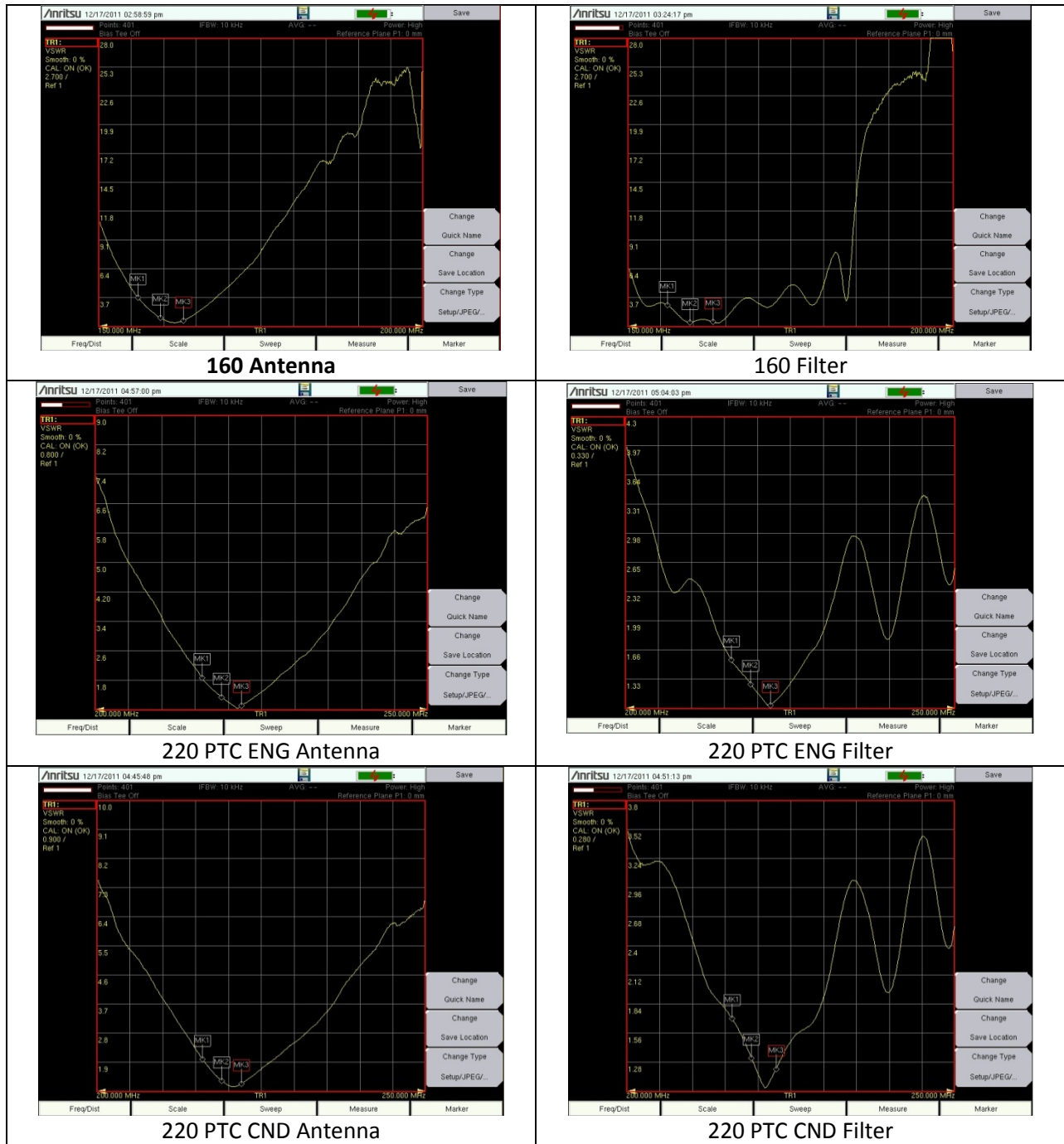


TABLE A VSWR Plots

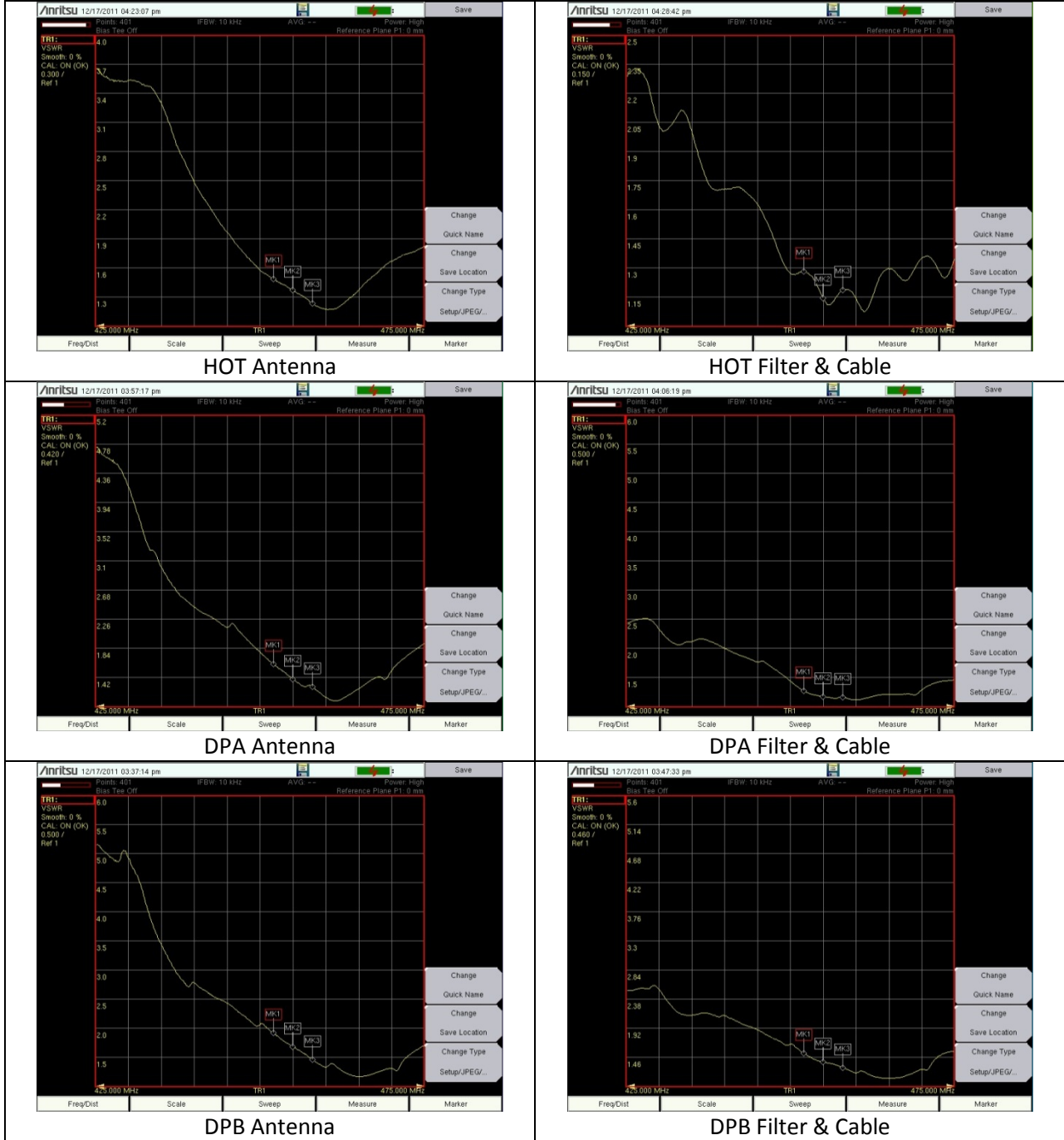


TABLE A VSWR Plots

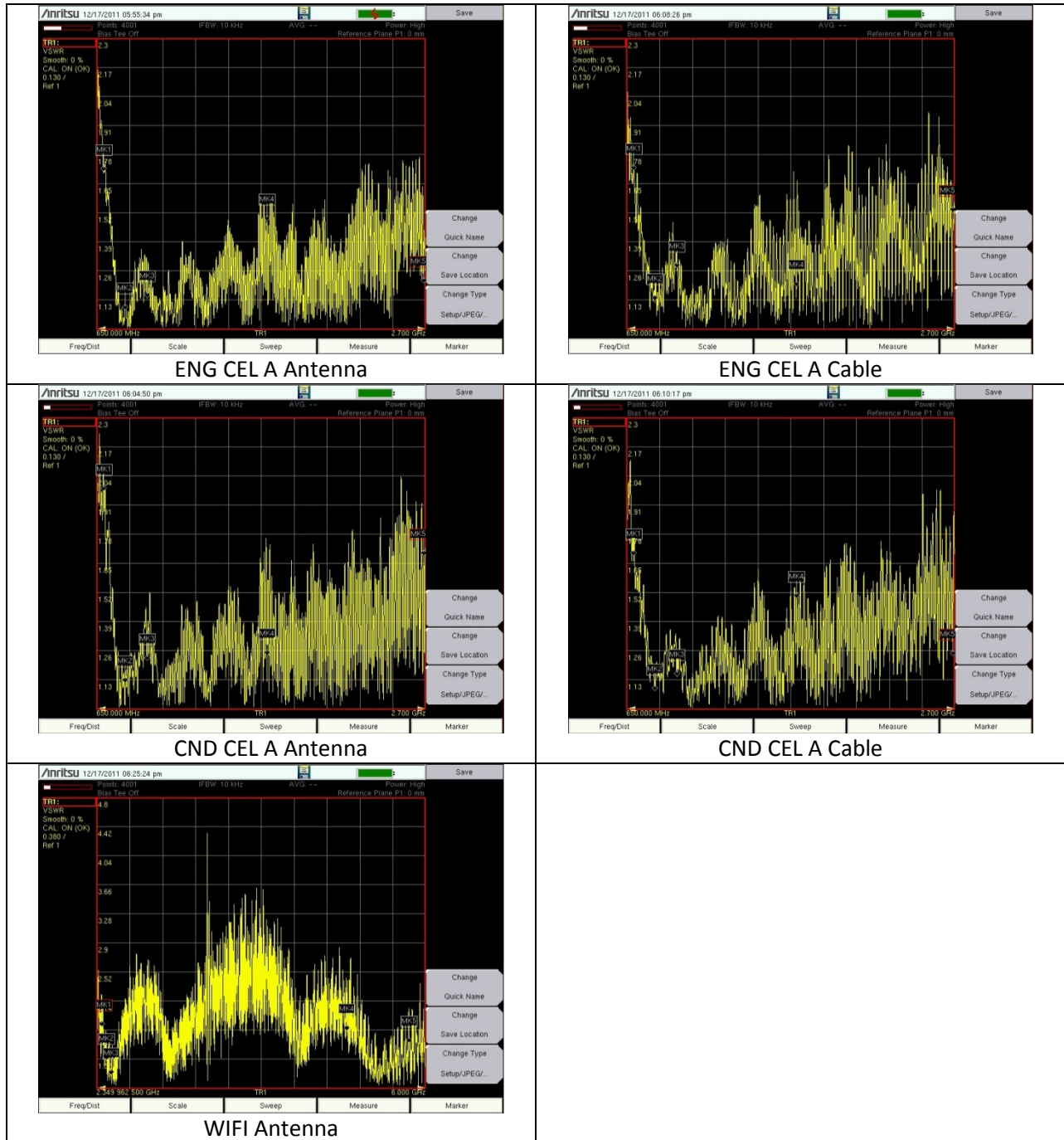
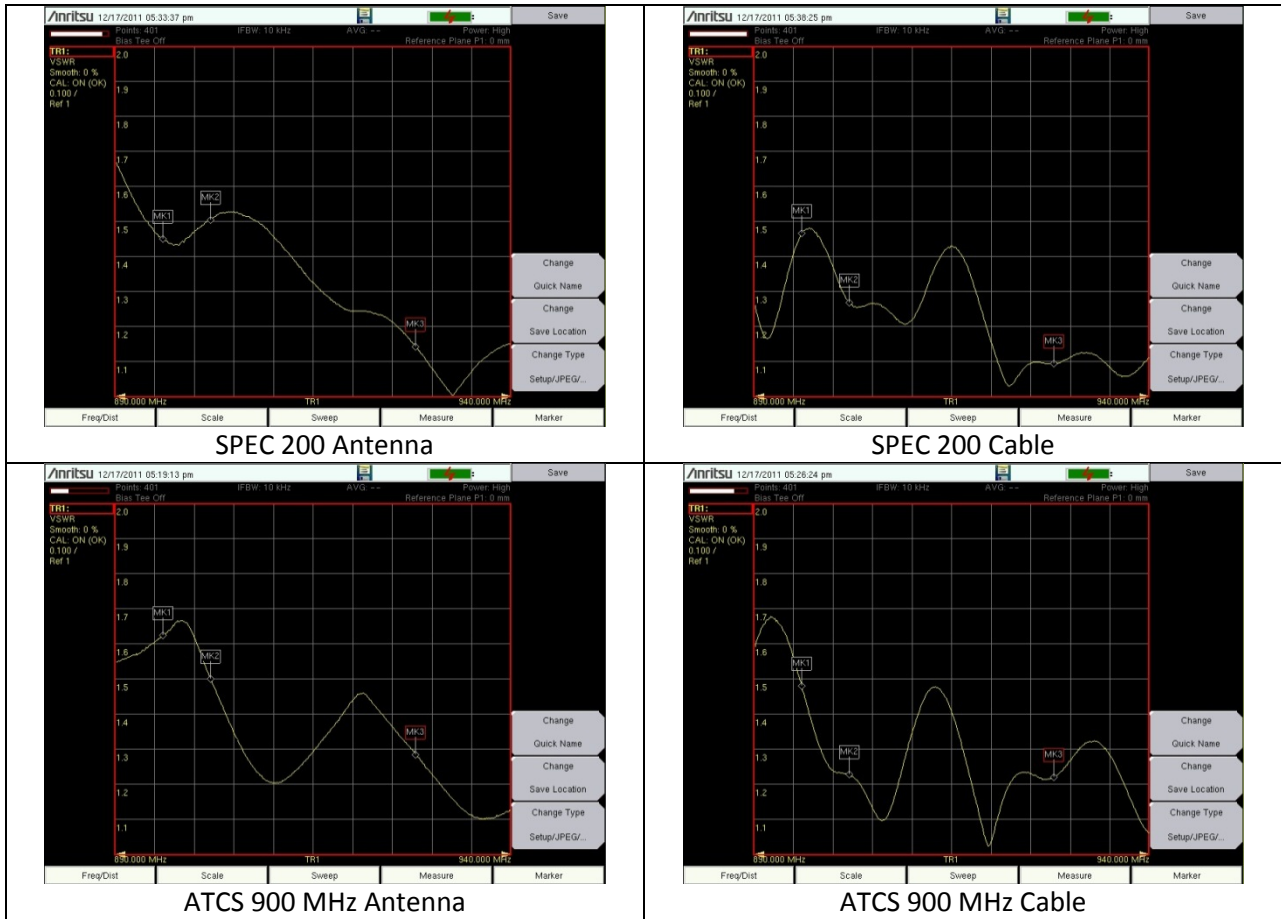


TABLE A VSWR Plots



### Insertion Loss

This test is designed to collect insertion loss data in several formats for use in locomotive noise and intermodulation reporting. The test involved collecting insertion loss data in the following formats; insertion loss in dB, S1P scatter parameters, comma separated values, and a portable network graphics. It is important to know how much loss is experienced in the system in order to determine the impact on transmitted power and intermodulation effects. The test was performed on the transmission lines by measuring the loss from the antenna connection port to the equipment port. The test is frequency specific and each cable was measured based on the appropriate frequency range.

This report is useful for evaluating cable integrity and is representative of any losses that are present in the system. At the completion of this testing it was found that all on-board elements were in compliance as compared to planned values. A full report has been included in Appendix B.

**TABLE B Insertion Loss Plots**

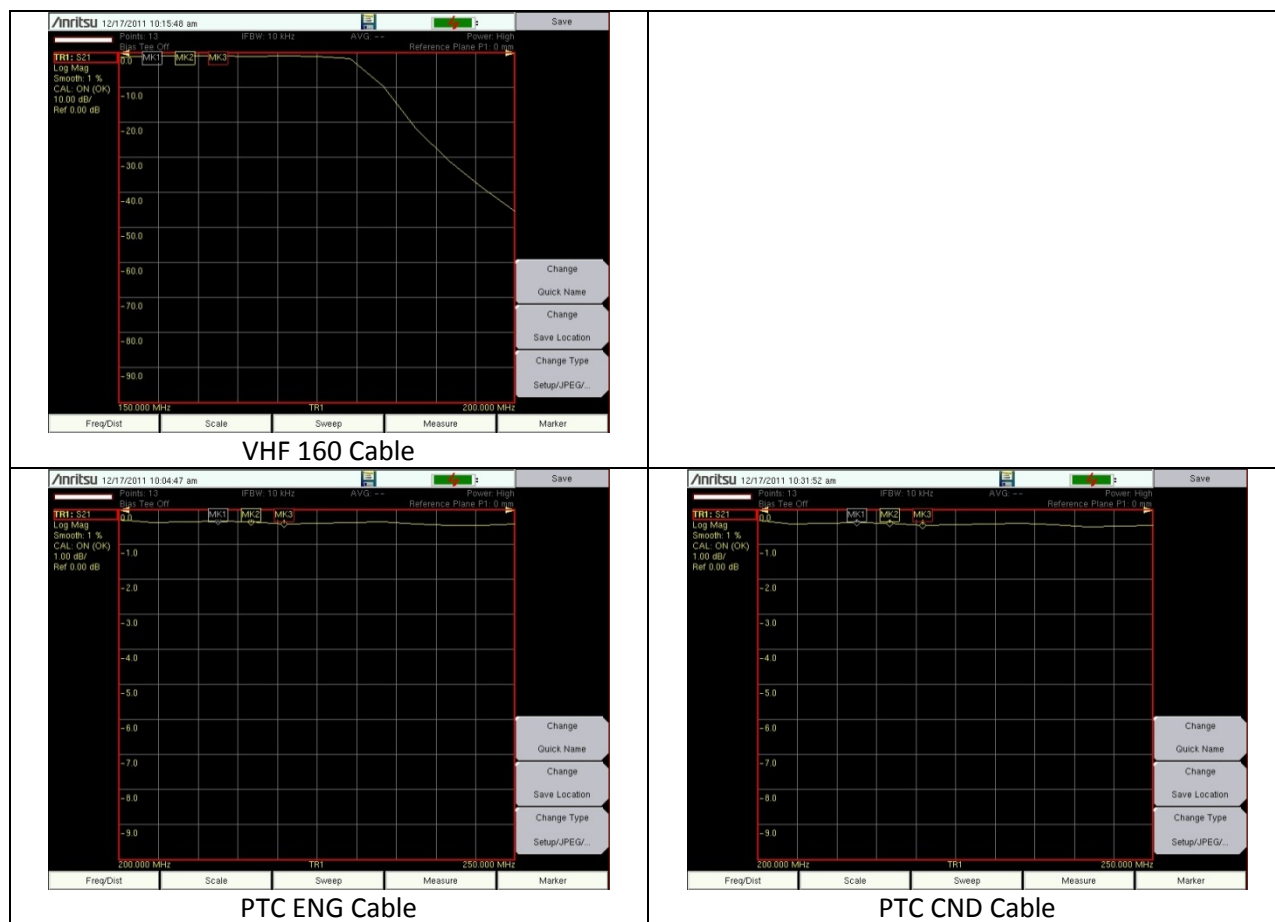
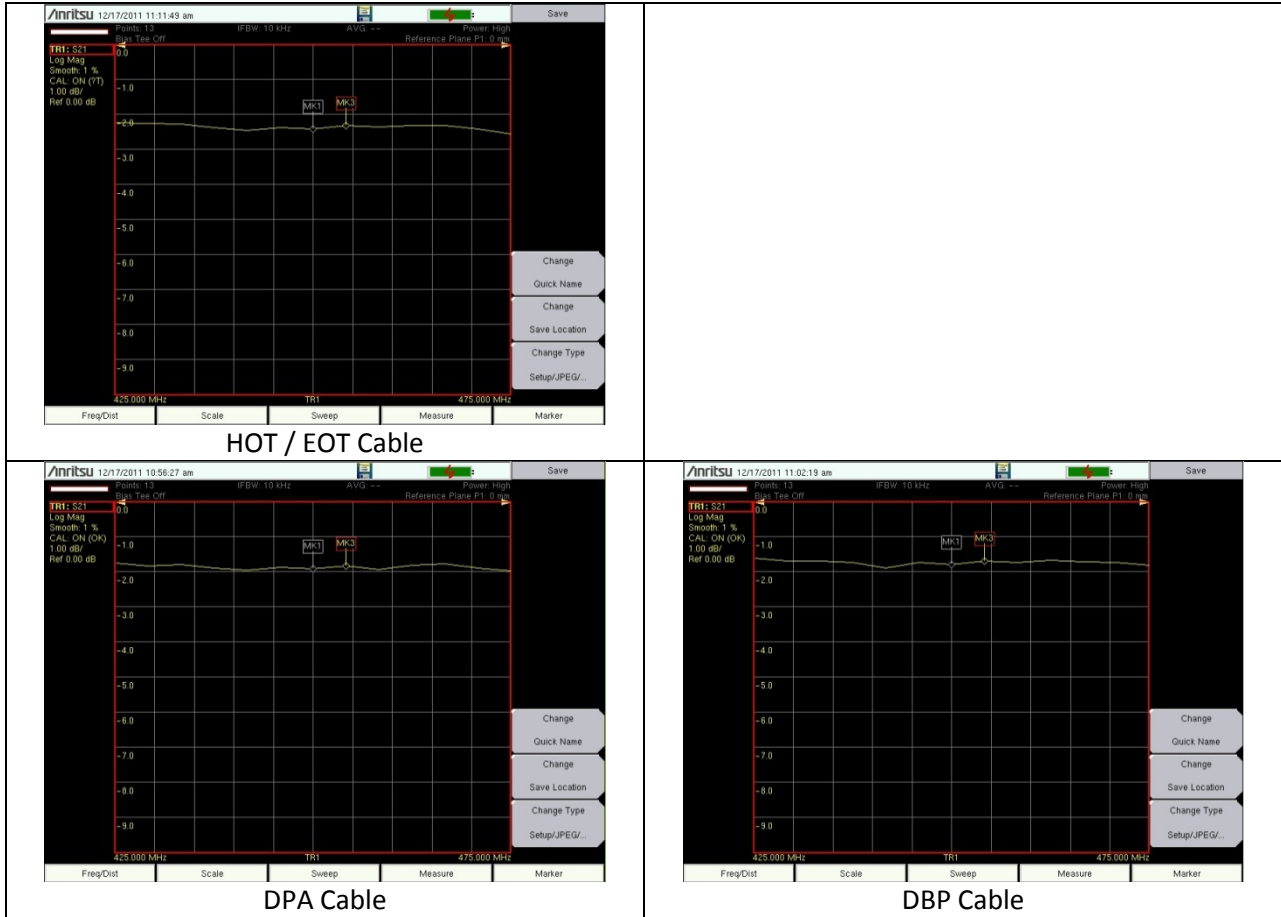


TABLE B Insertion Loss Plots

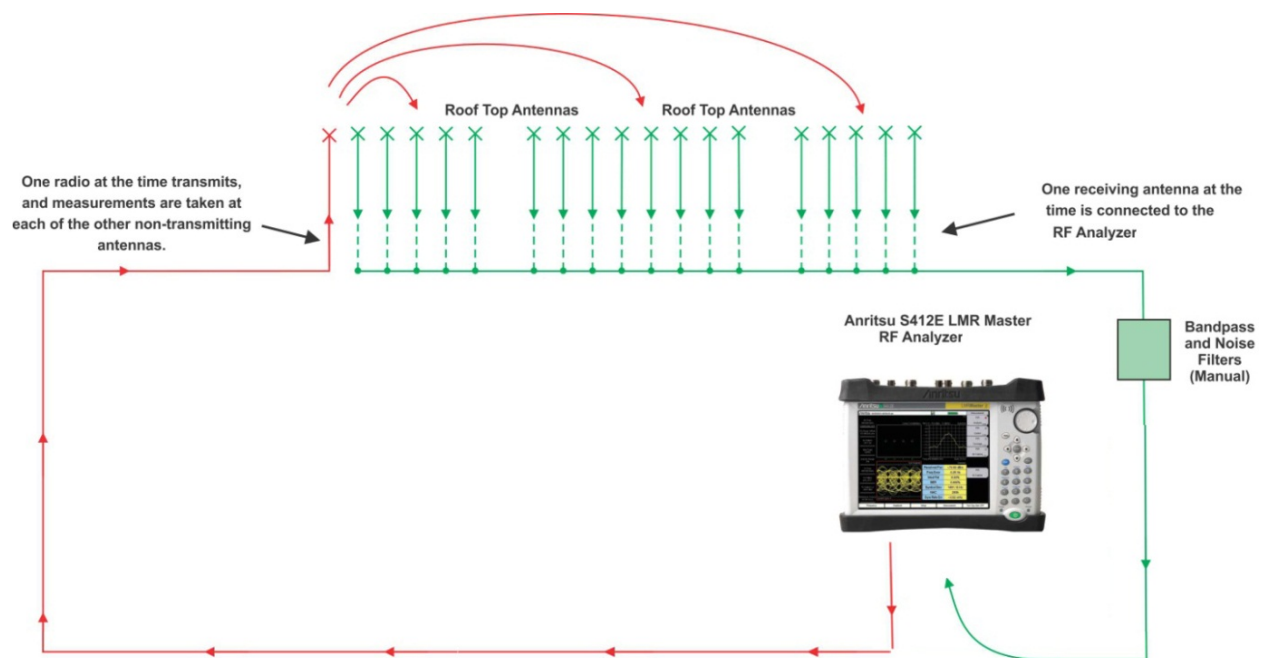


## Antenna Isolation Test

This test is designed to collect information on the amount of free space isolation between each antenna and each other antenna. This value is in decibels and is used to calculate the amount of power from each radio transmitter impacting each radio receiver front end during transmission. High signal levels impacting the receiver front end of a radio in receive mode will cause intermodulation products in proportion to the power received from the transmitting radio. The antenna isolation data is also used to determine the need for filtering in the system.

The test was performed by measuring the loss from the transmitting radio antenna to each other antenna, and the data was recorded in decibel format. The information gathered from this test correlates to the amount on intermodulation that is present in the roof environment, and possible prevention methods.

The test is executed without filters, and then executed with any filters under consideration by the Railroad.



Antenna Isolation Testing Configuration  
Figure 16



TABLE C Antenna Isolation Plots

AAR Voice Transmit Direct

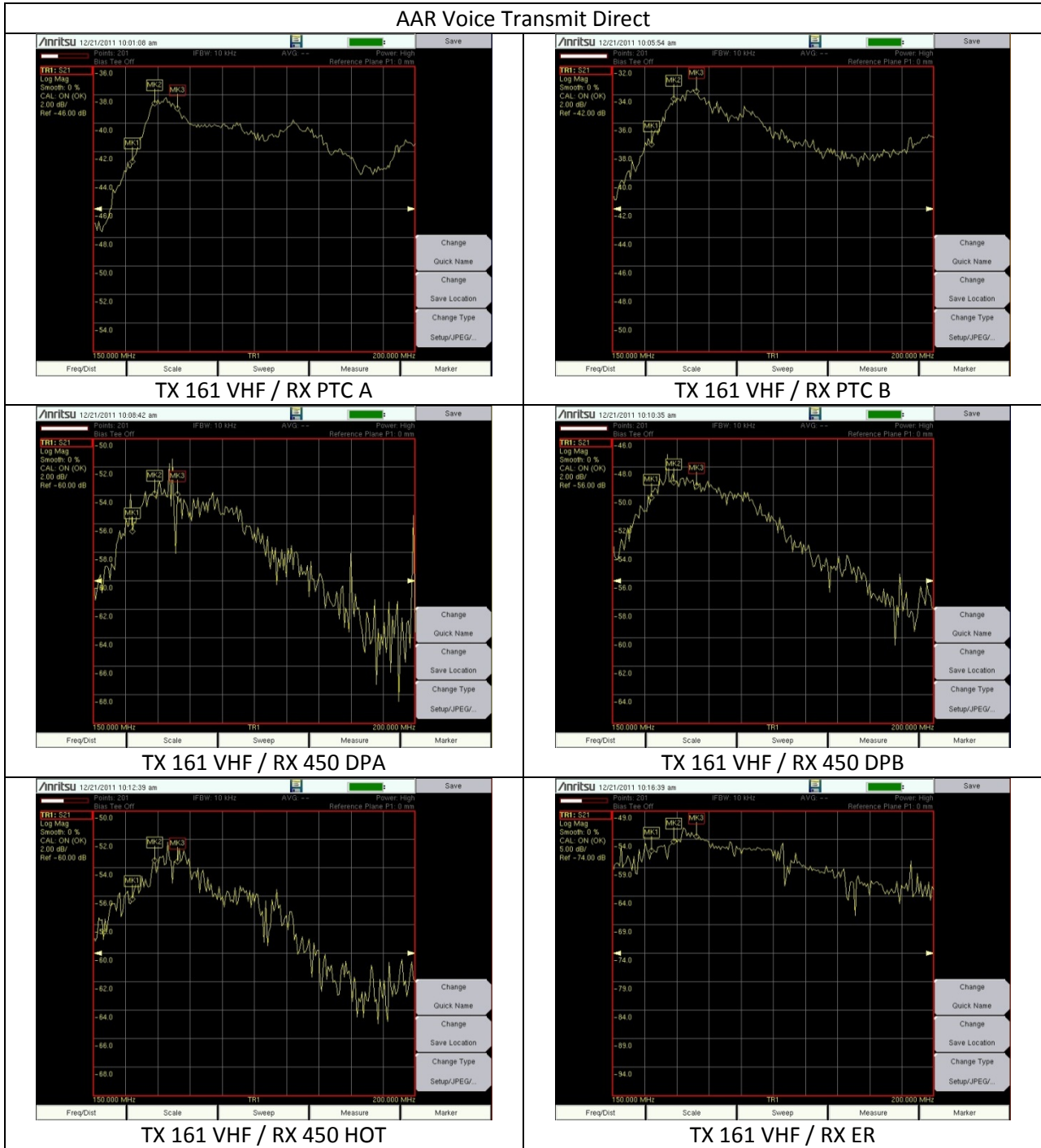


TABLE C Antenna Isolation Plots

AAR Voice Transmit Direct

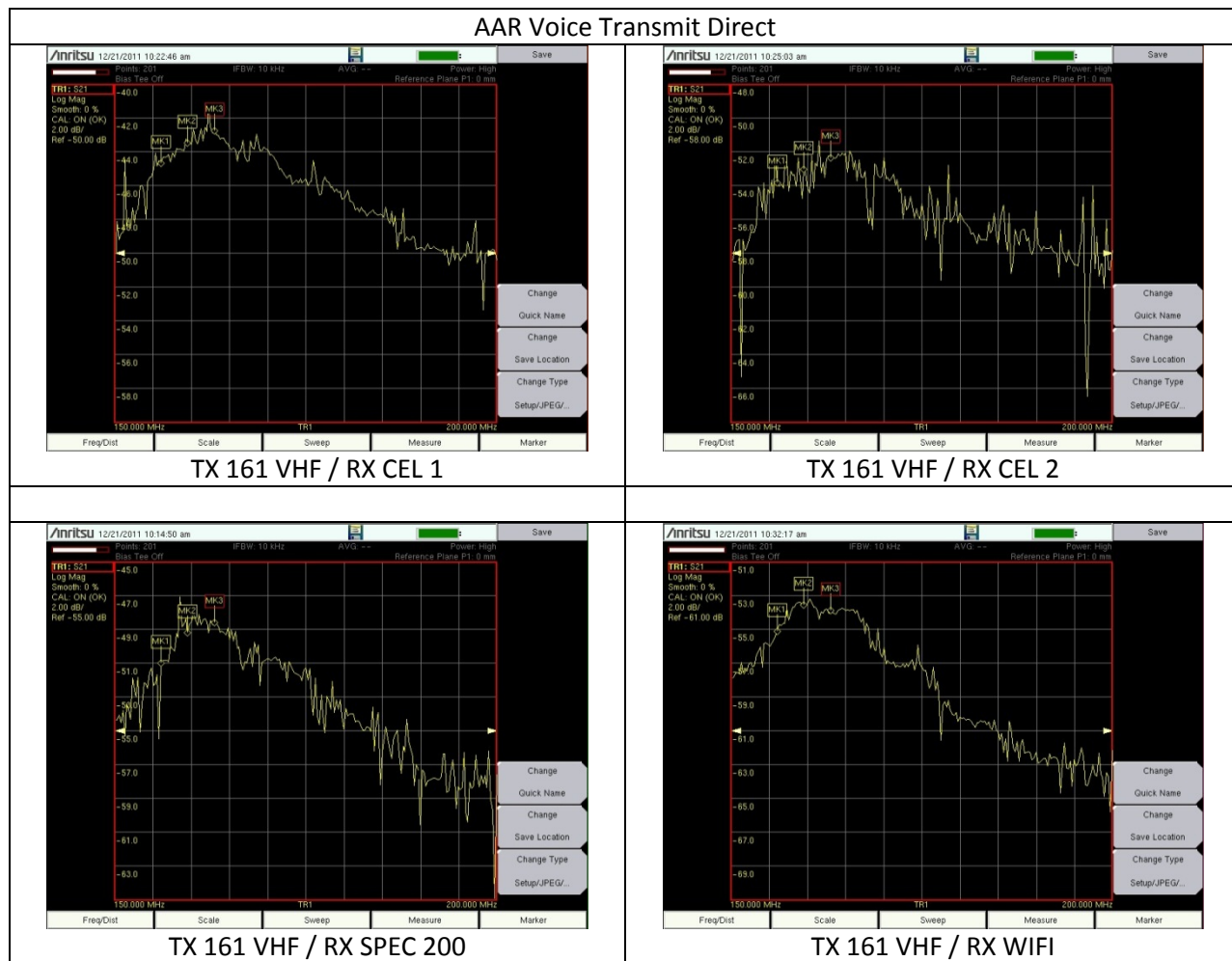


TABLE C Antenna Isolation Plots

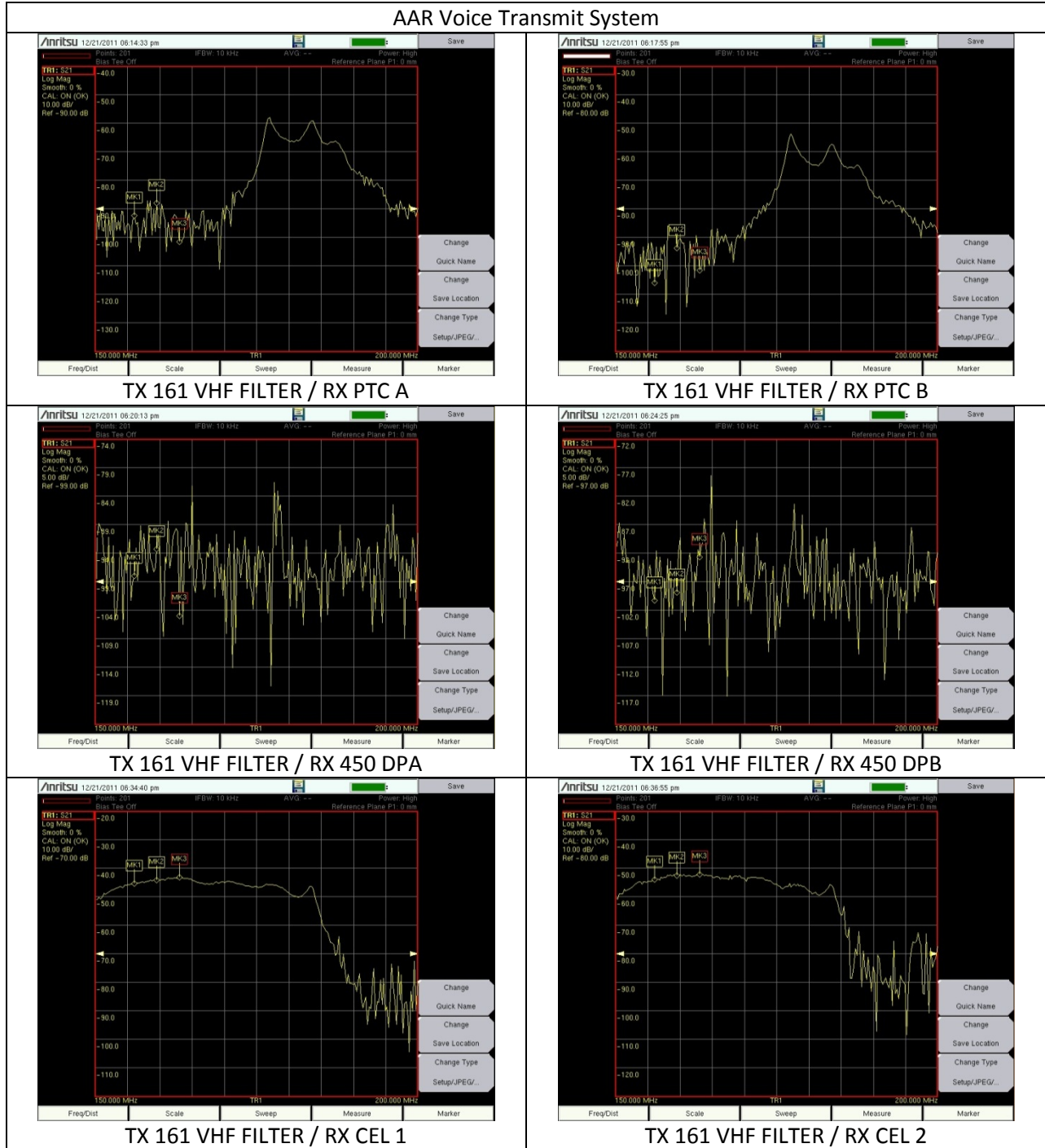


TABLE C Antenna Isolation Plots

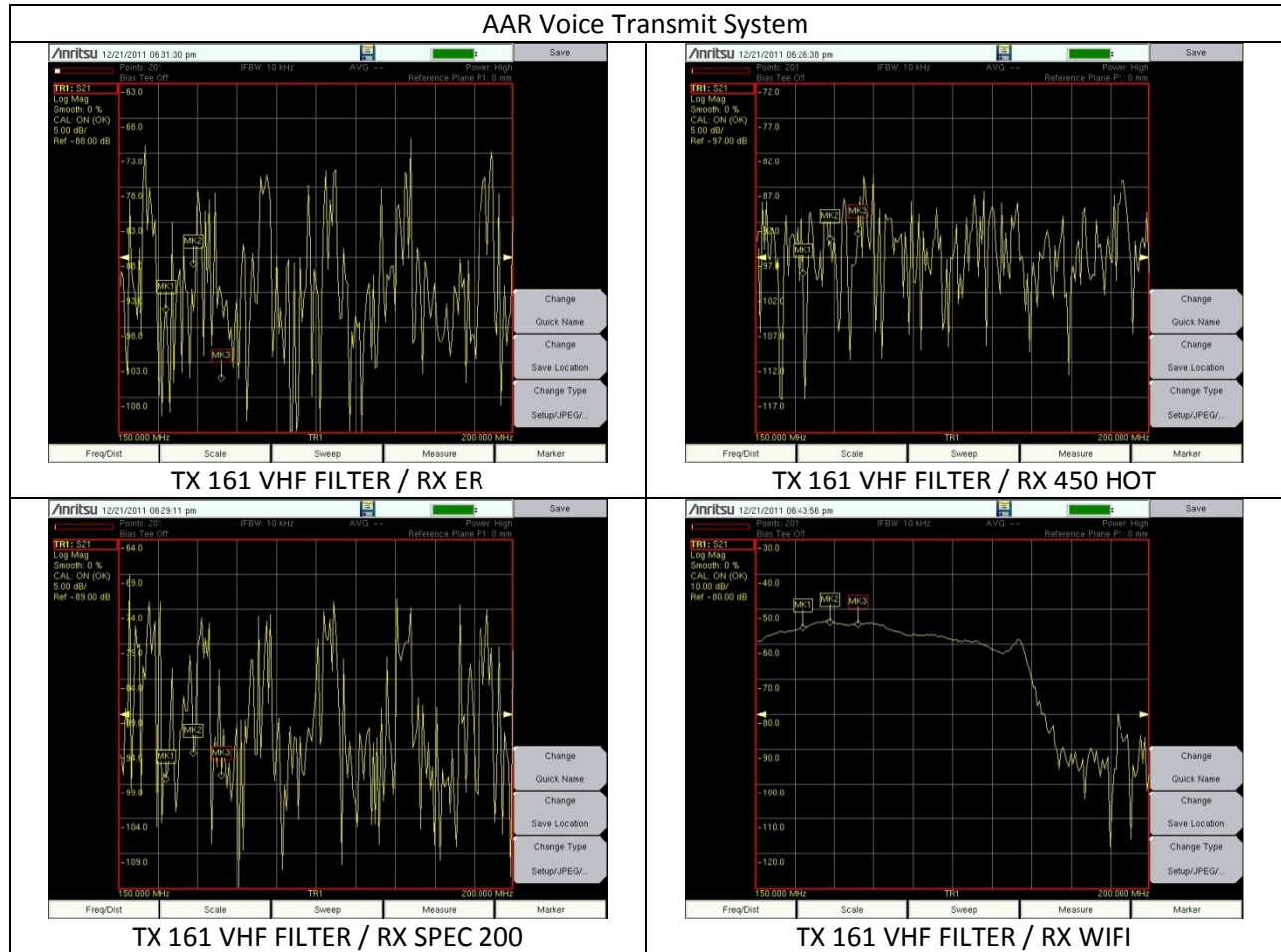


TABLE C Antenna Isolation Plots

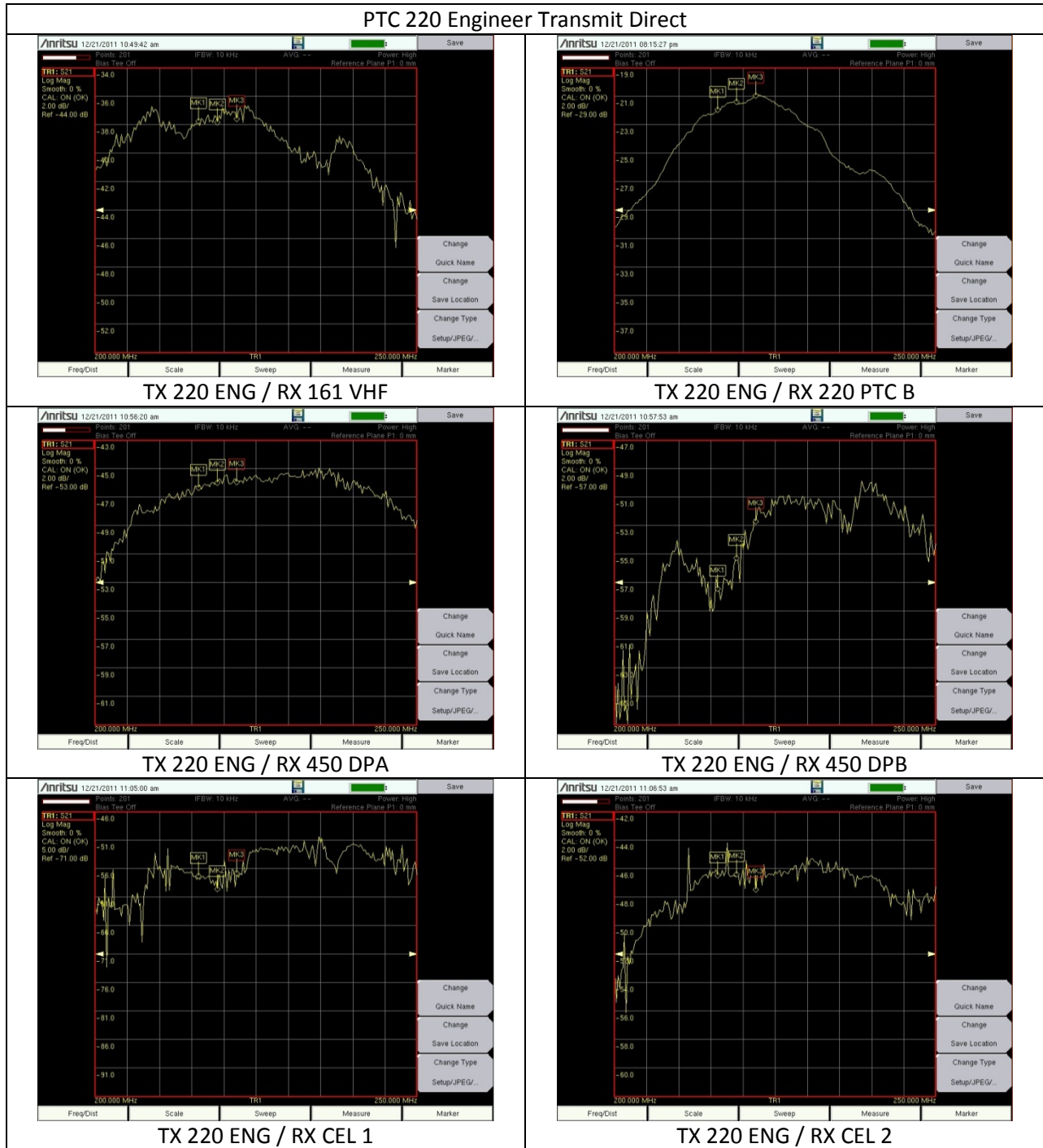


TABLE C Antenna Isolation Plots

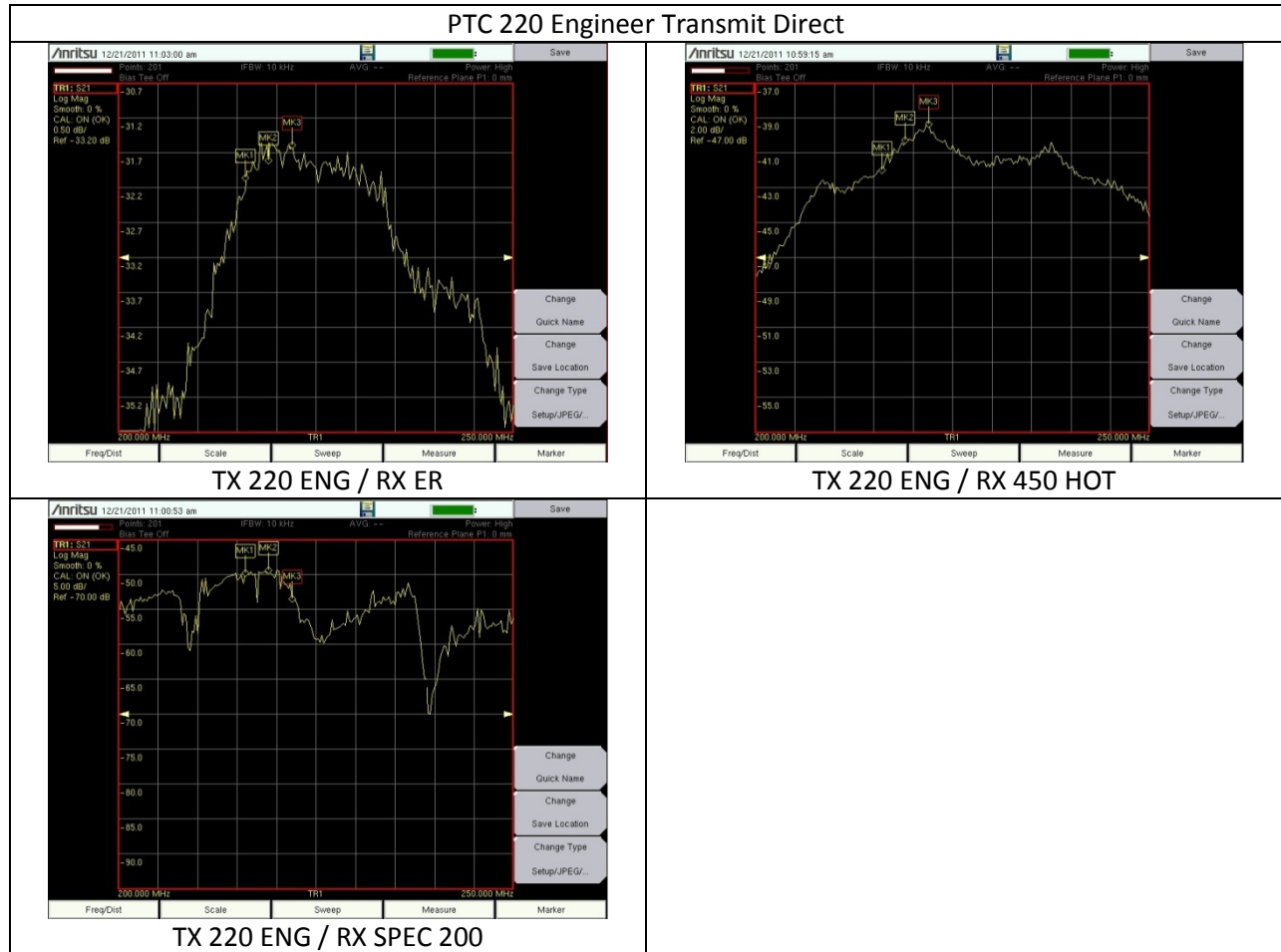


TABLE C Antenna Isolation Plots

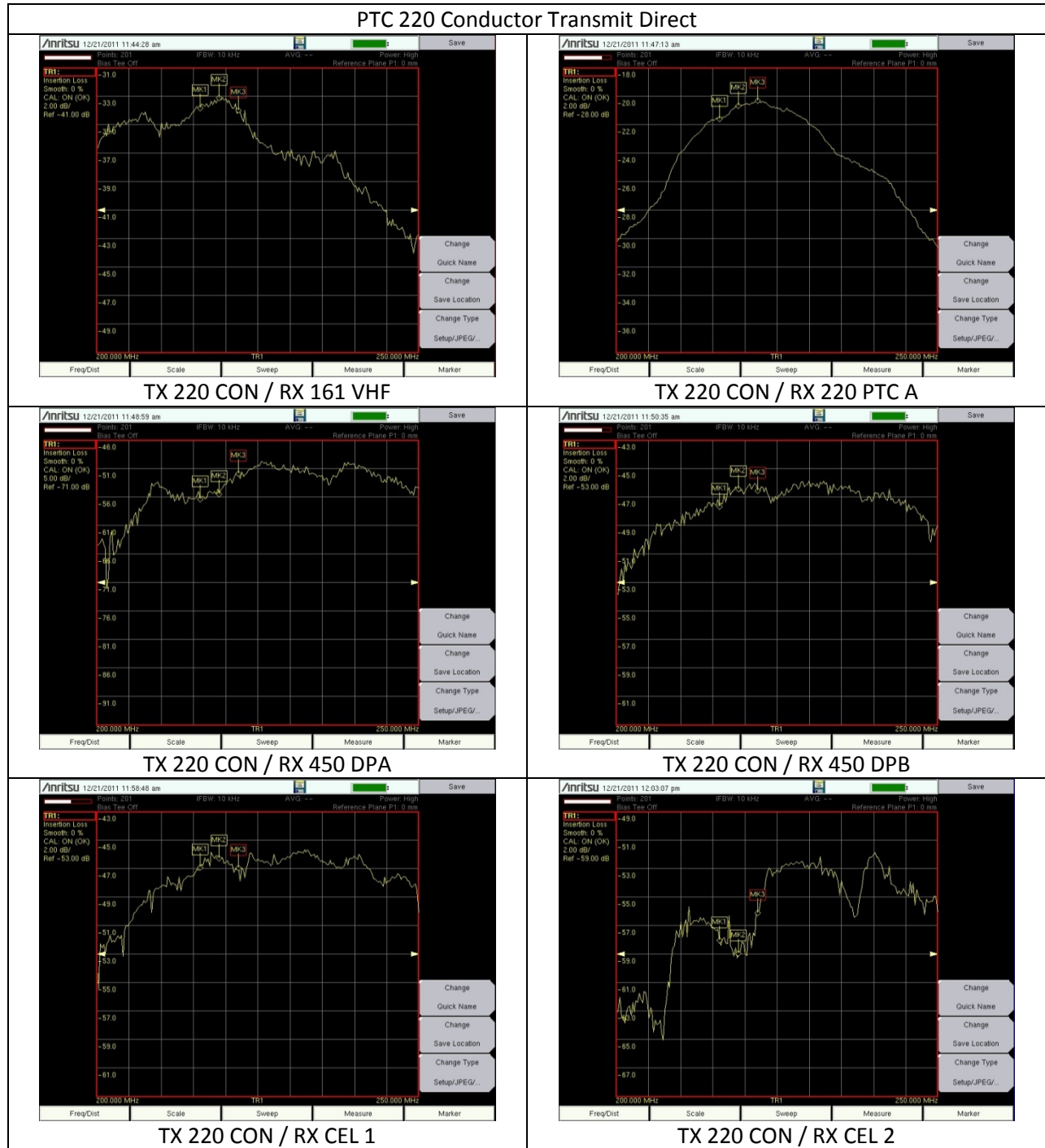


TABLE C Antenna Isolation Plots

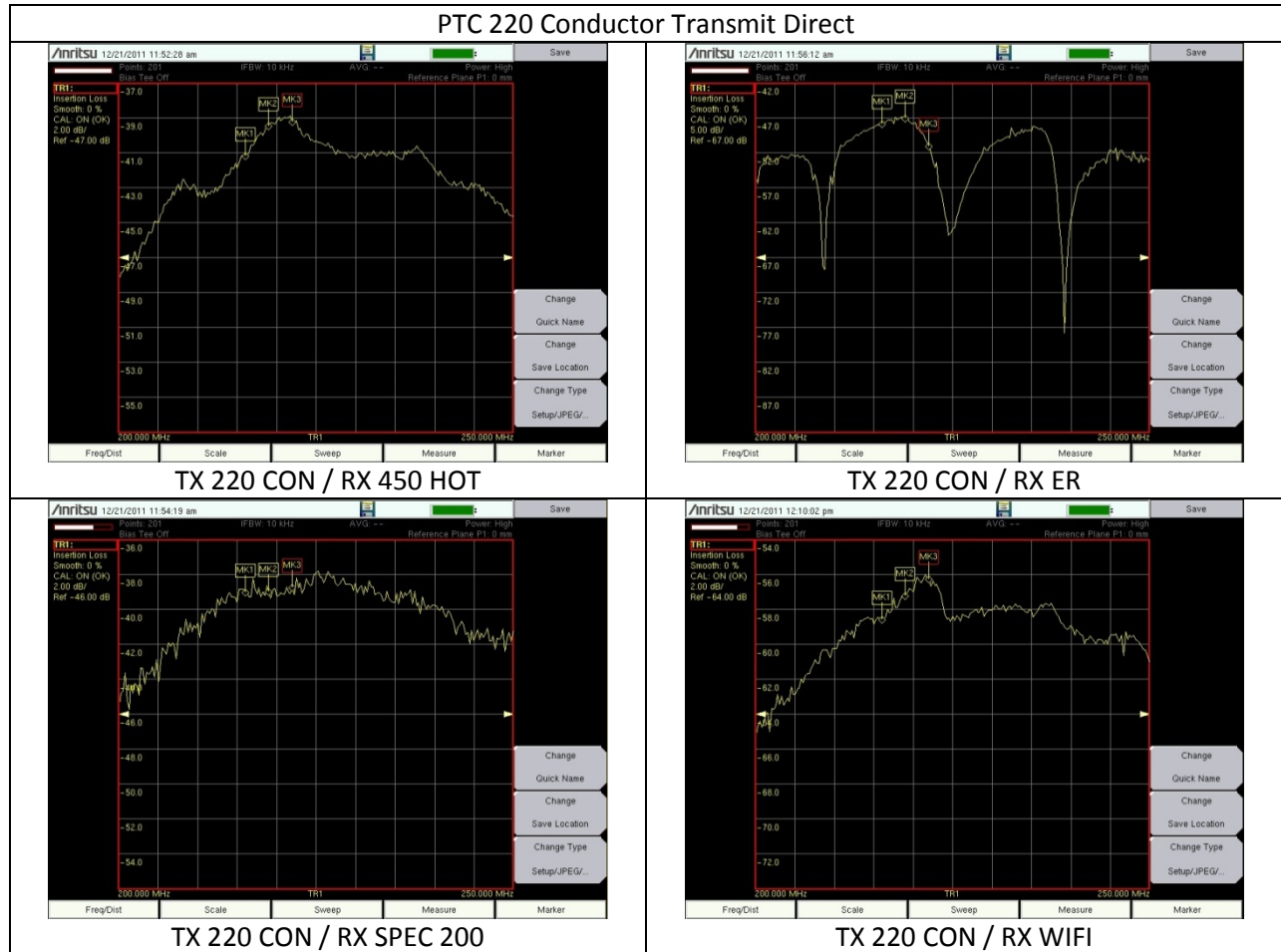




TABLE C Antenna Isolation Plots

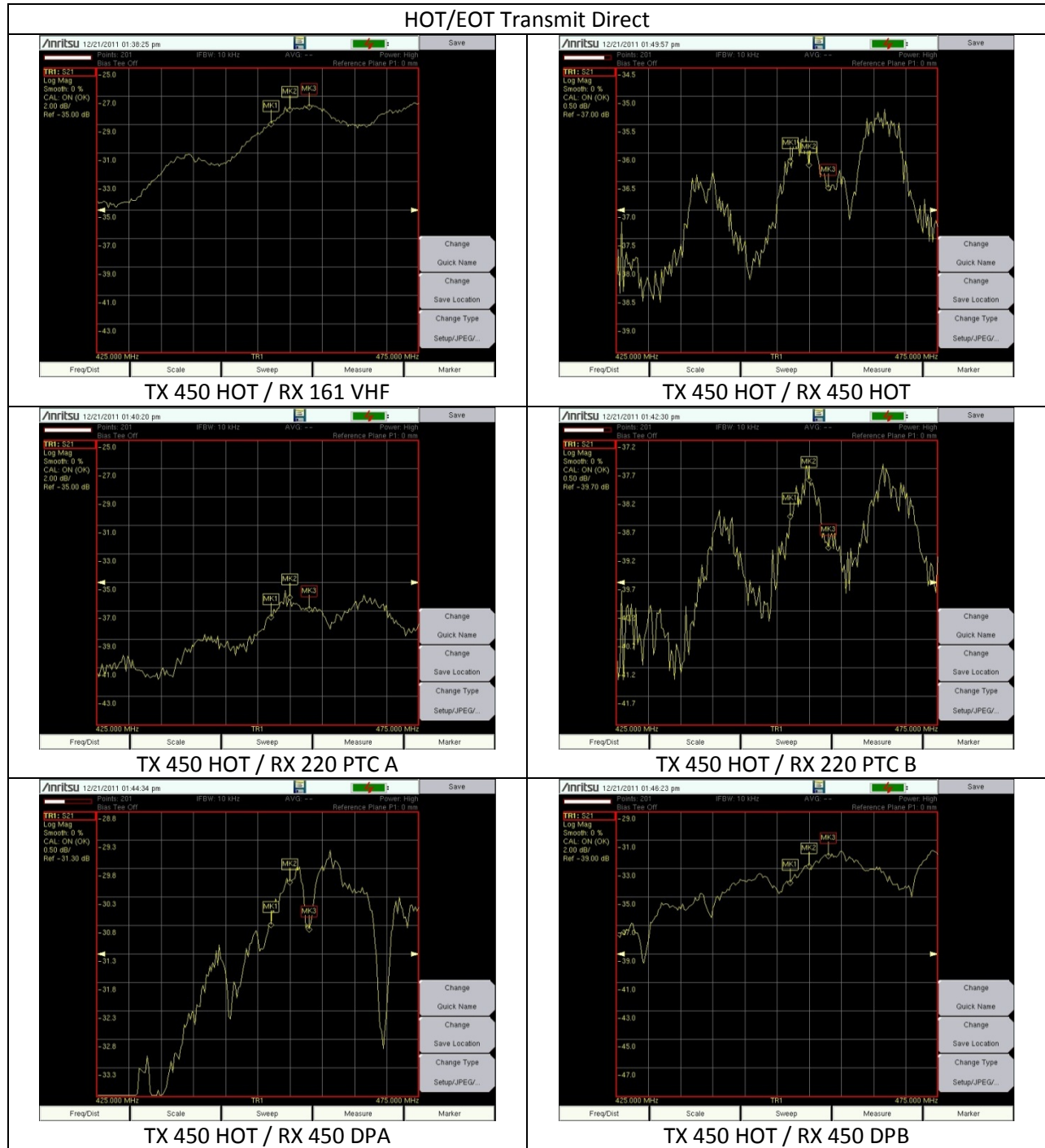


TABLE C Antenna Isolation Plots

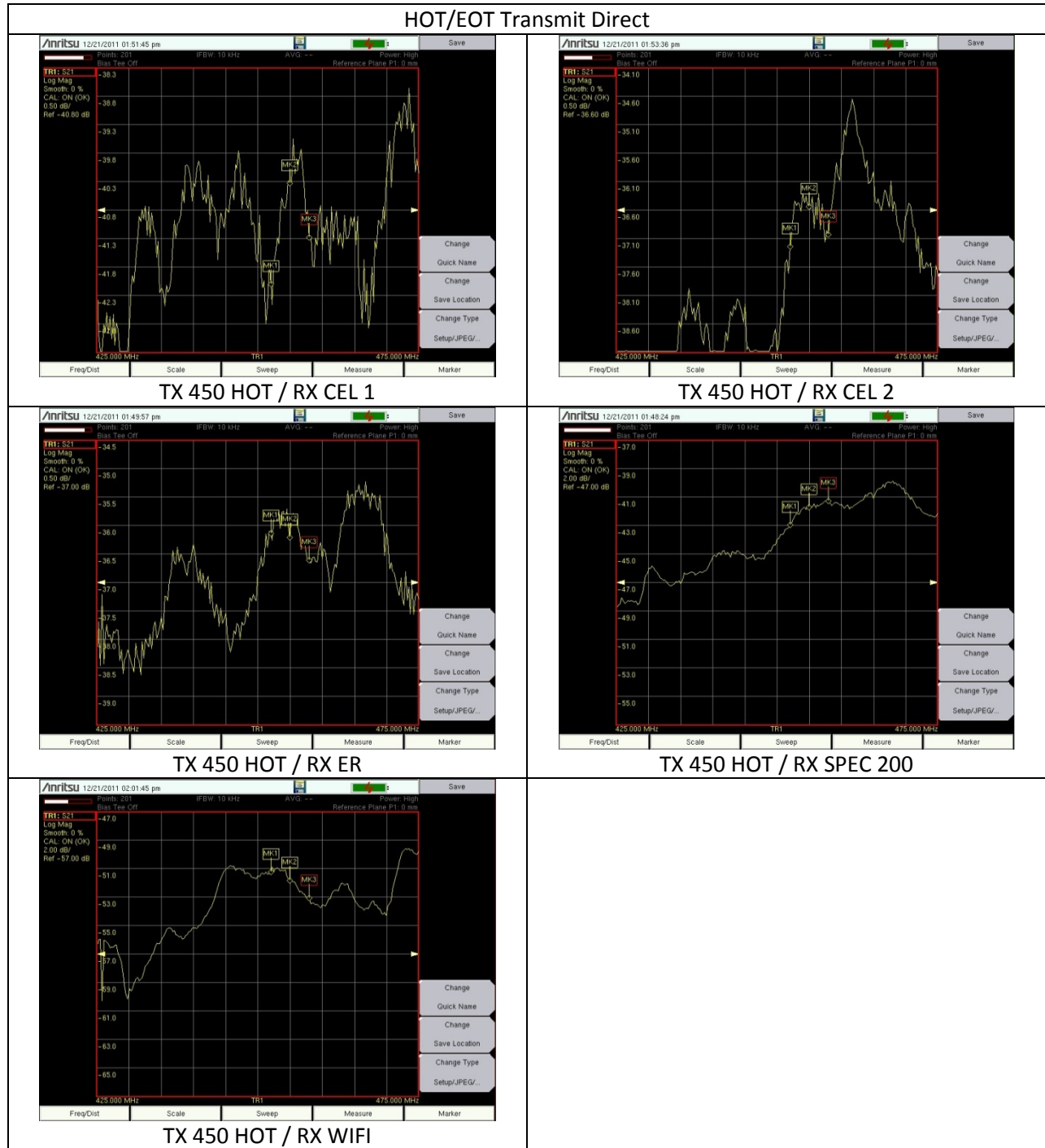


TABLE C Antenna Isolation Plots

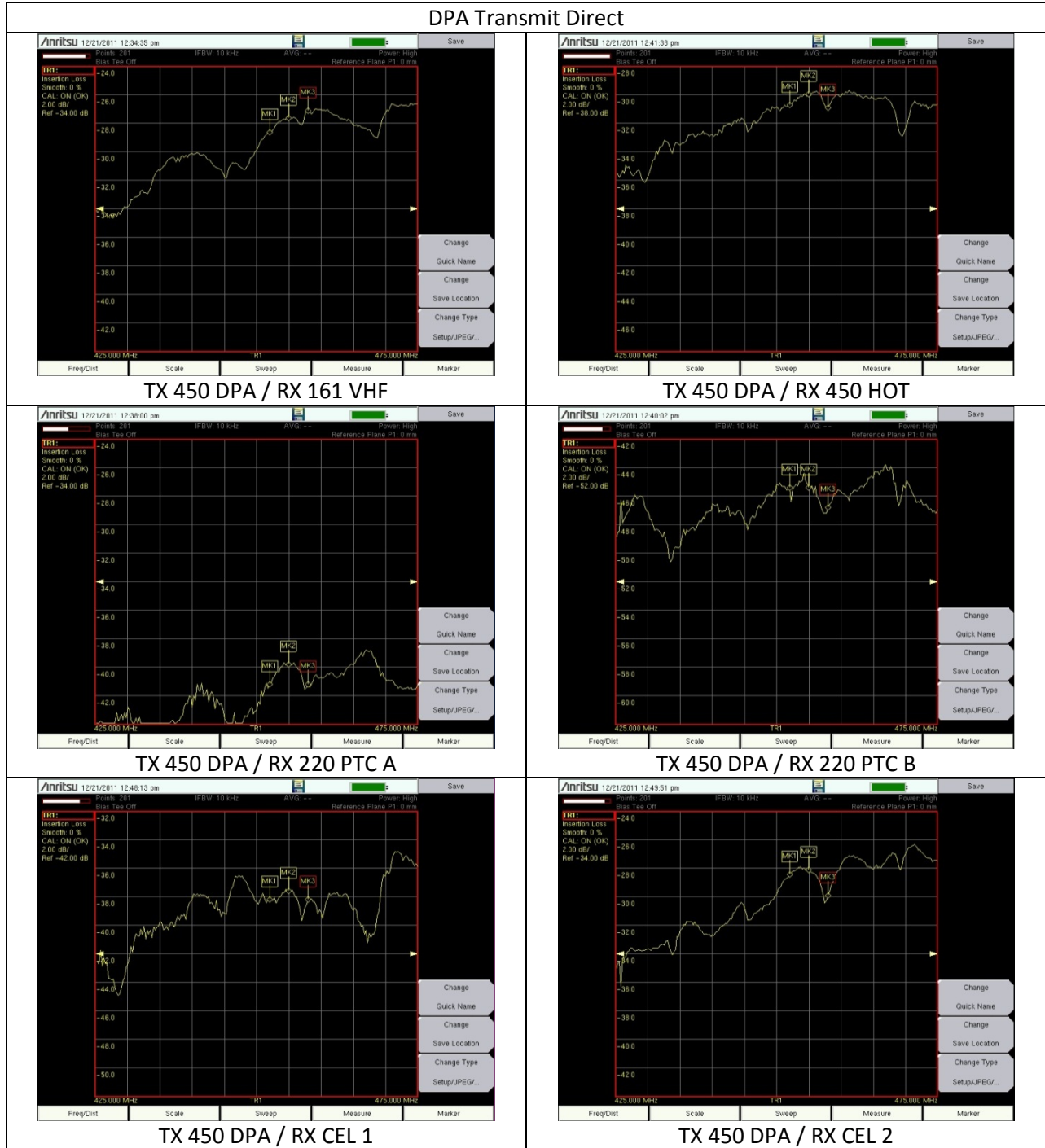


TABLE C Antenna Isolation Plots

DPA Transmit Direct

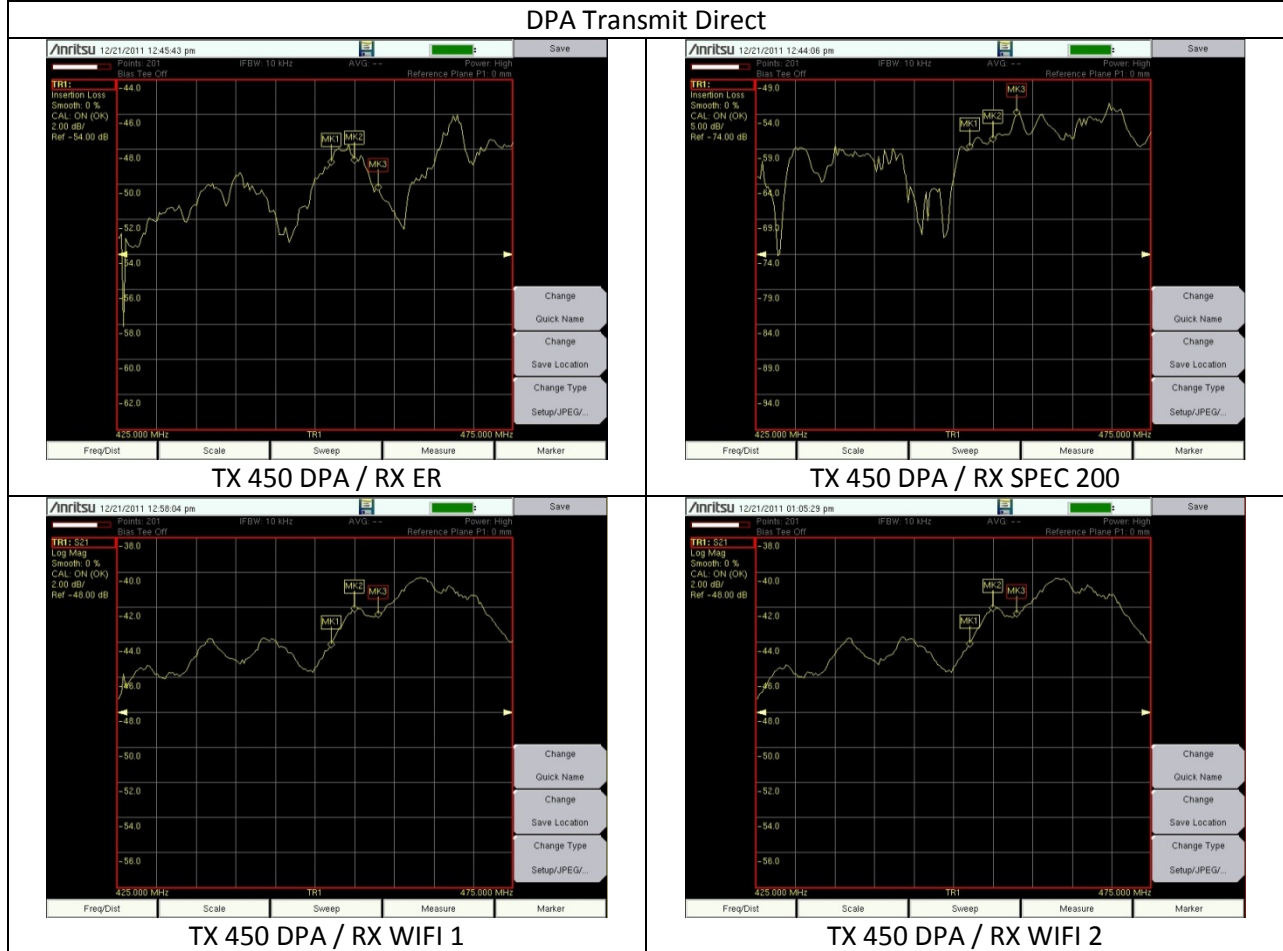


TABLE C Antenna Isolation Plots

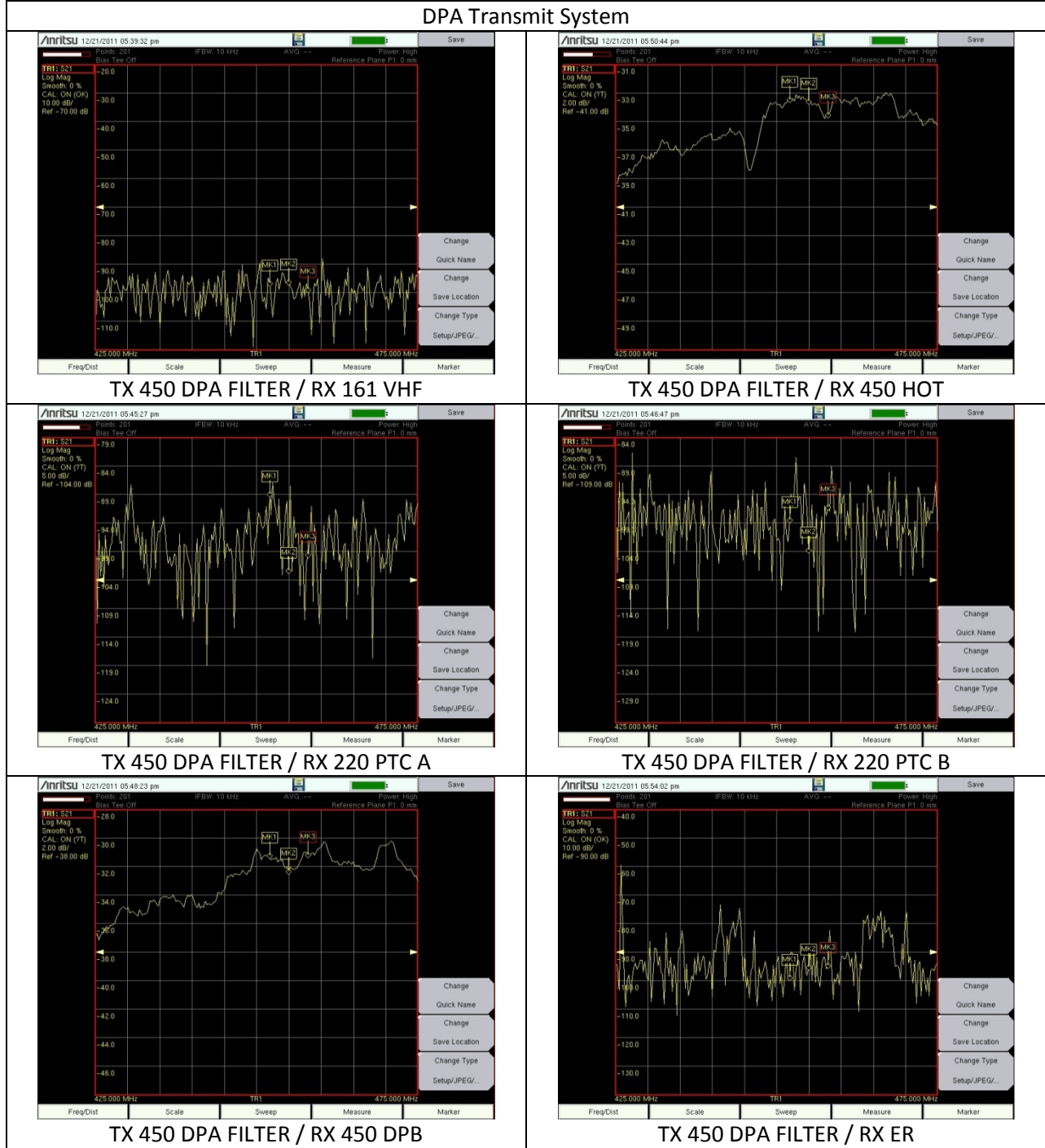


TABLE C Antenna Isolation Plots

DPA Transmit System

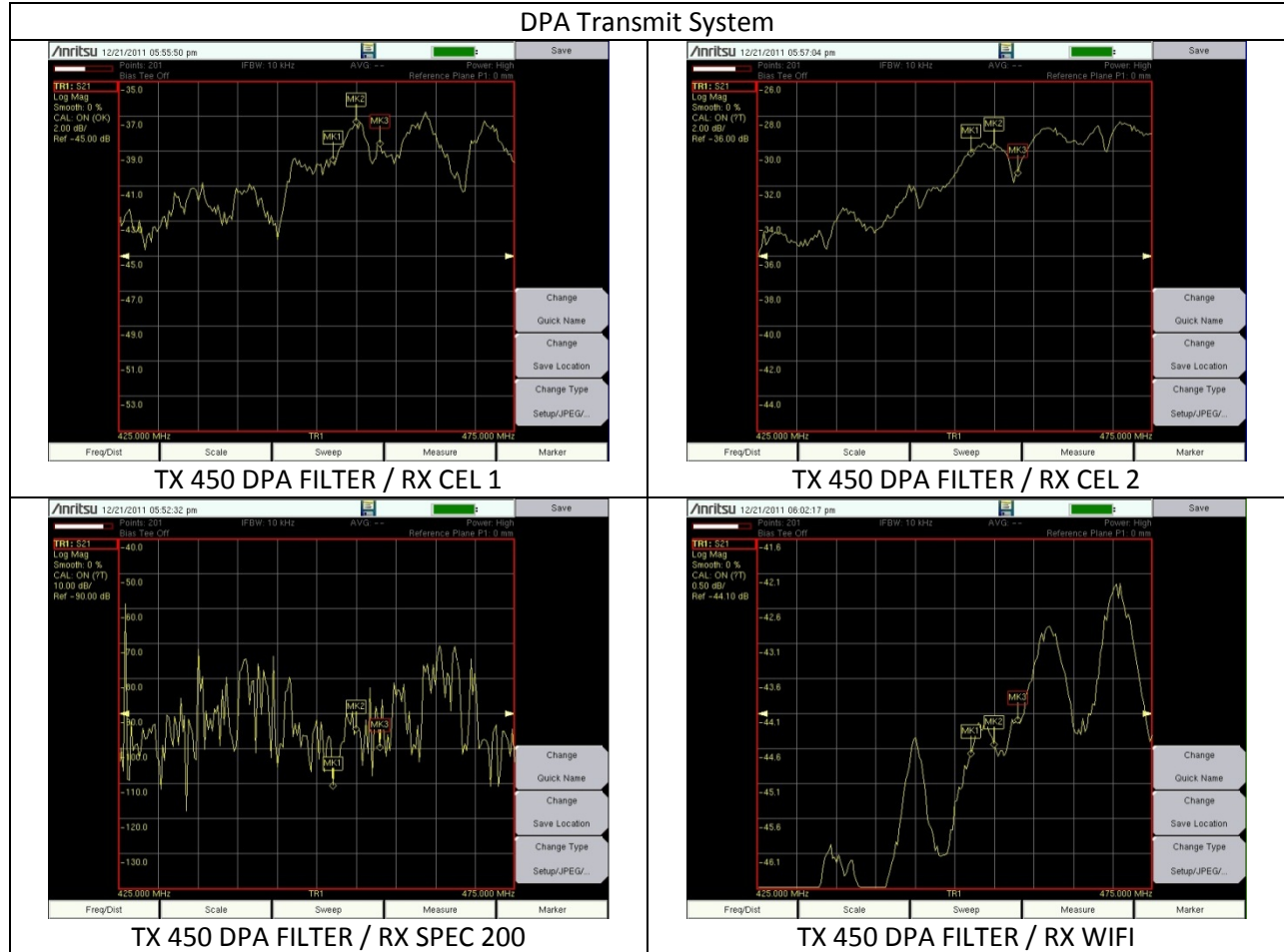


TABLE C Antenna Isolation Plots

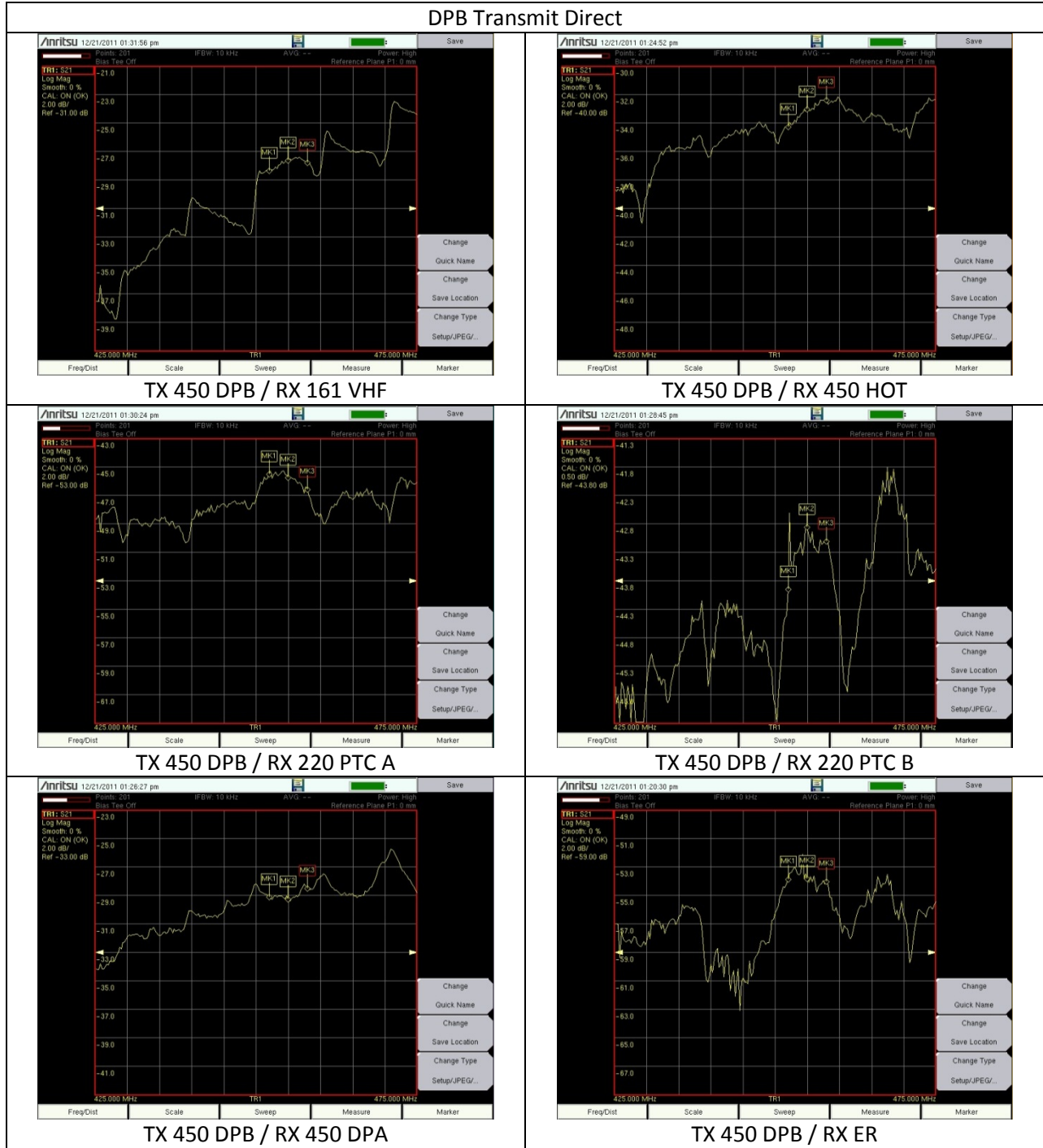


TABLE C Antenna Isolation Plots

DPB Transmit Direct

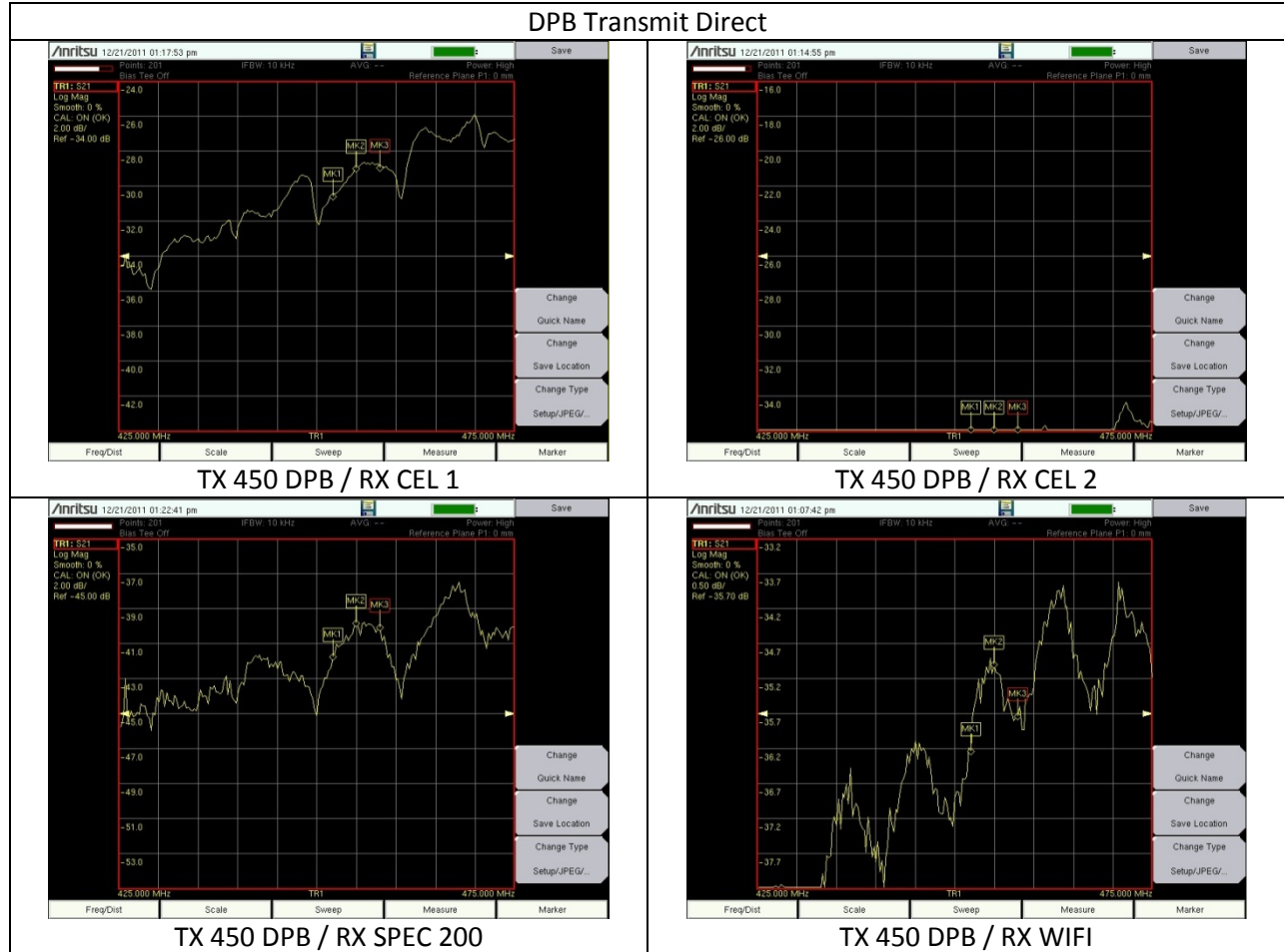




TABLE C Antenna Isolation Plots

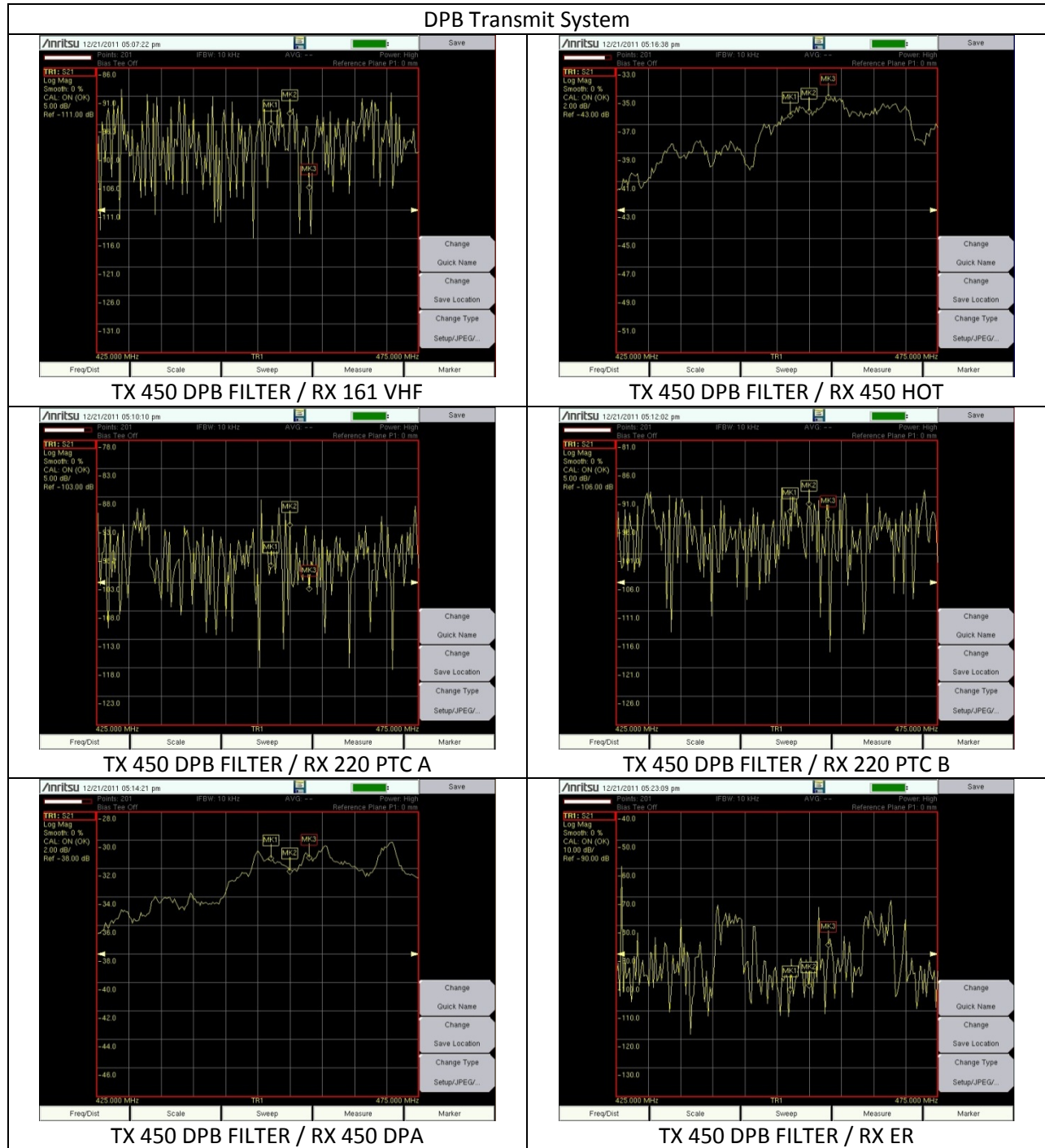


TABLE C Antenna Isolation Plots

DPB Transmit System

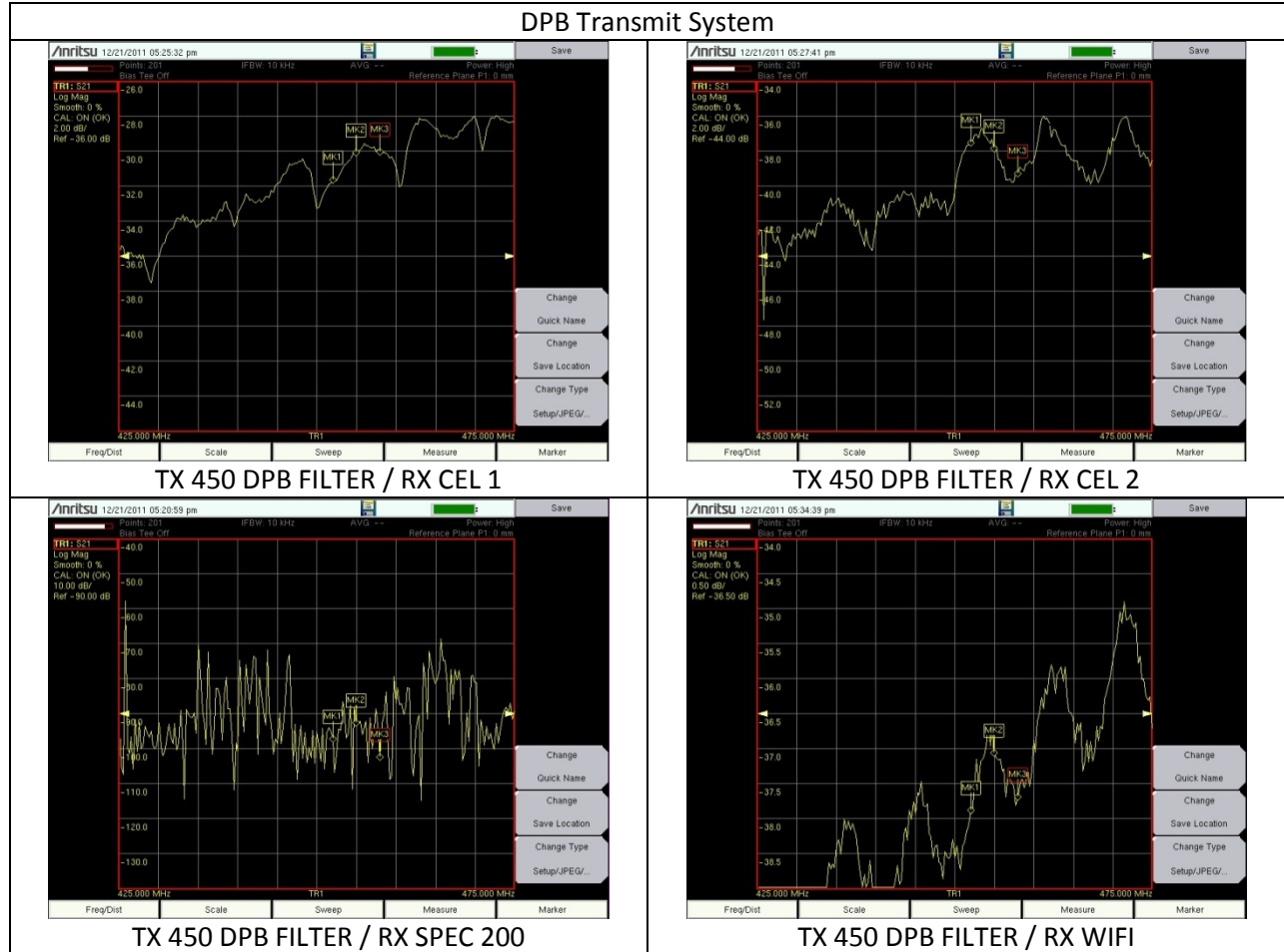


TABLE C Antenna Isolation Plots

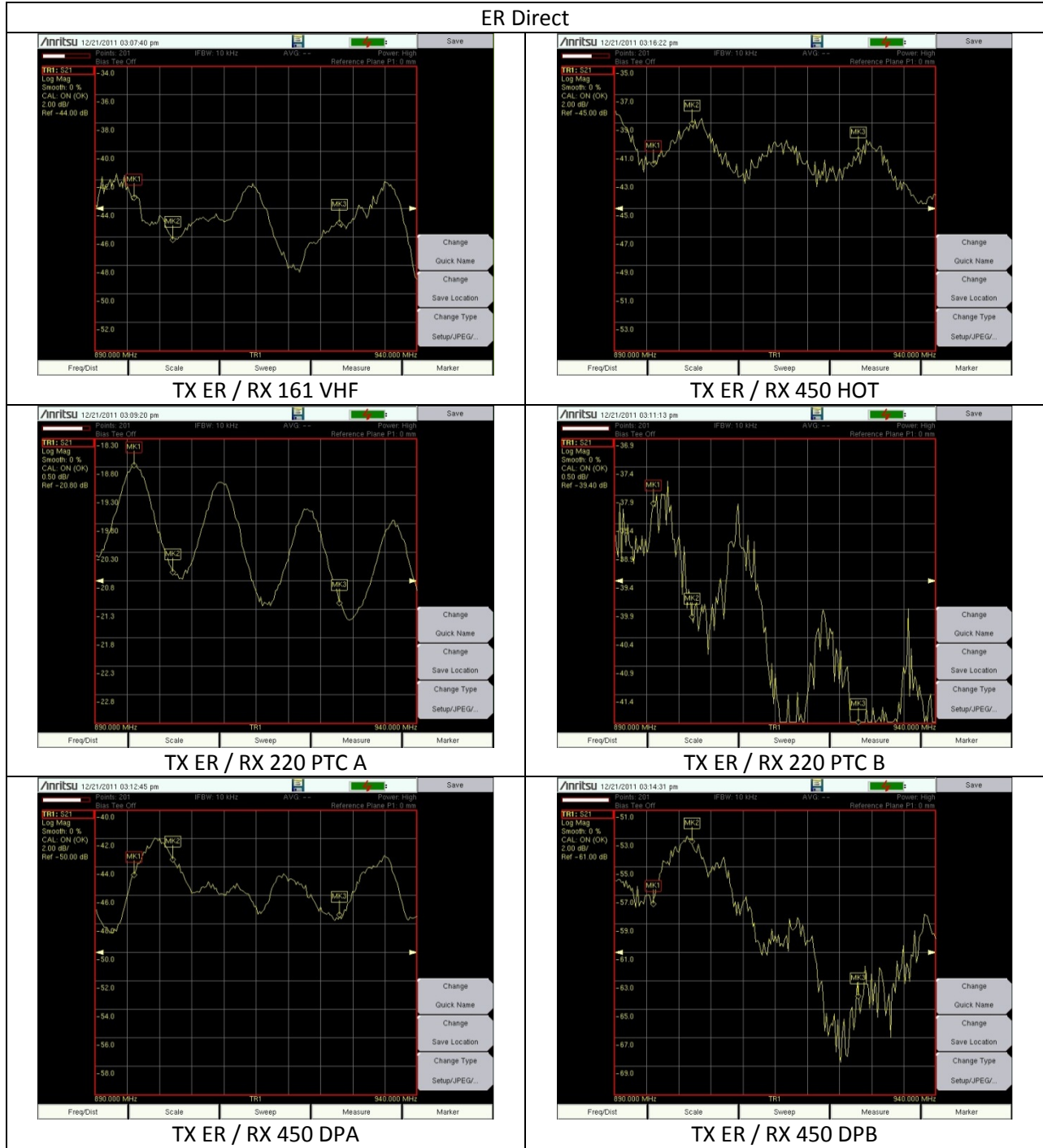


TABLE C Antenna Isolation Plots

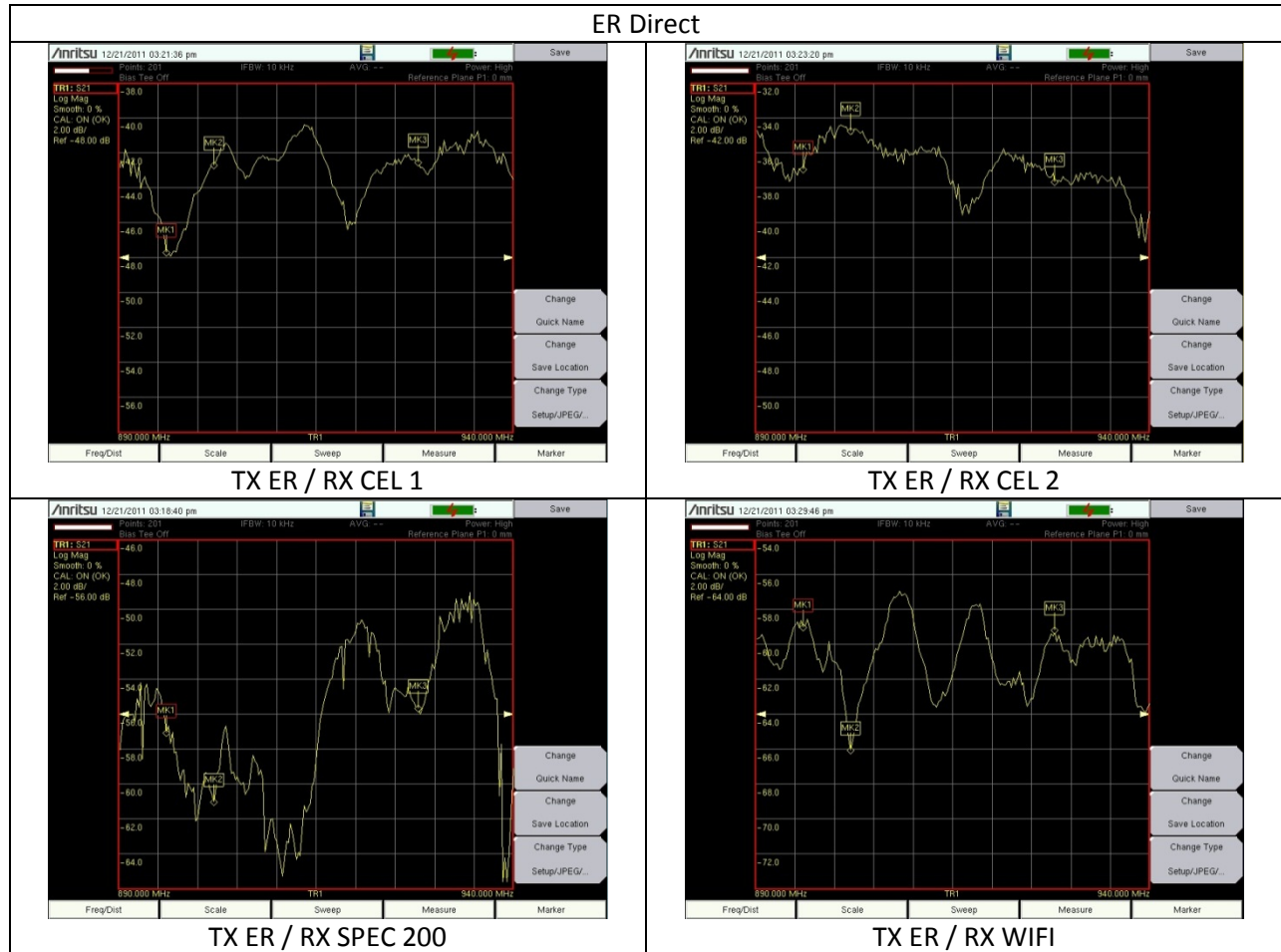


TABLE C Antenna Isolation Plots

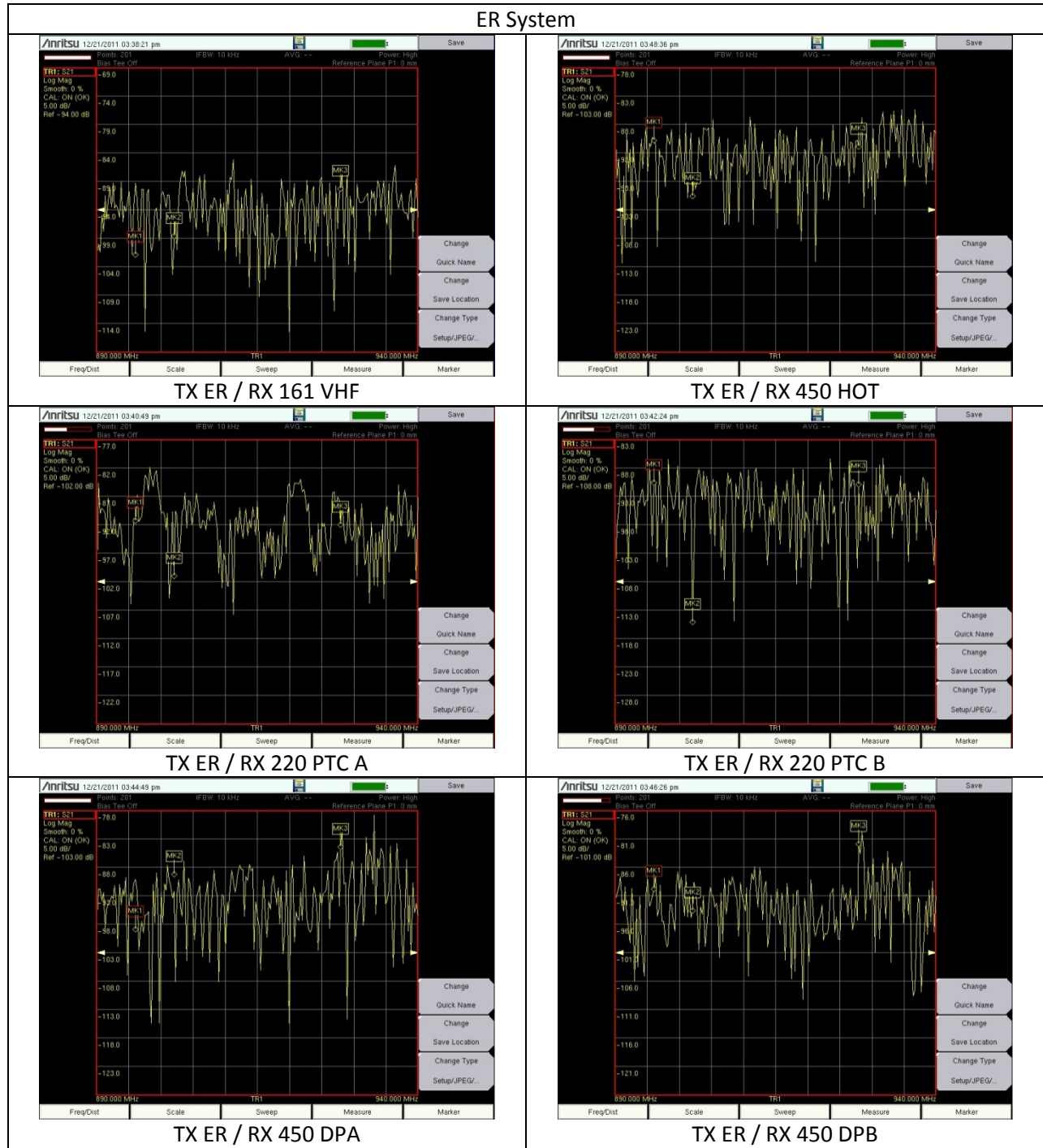


TABLE C Antenna Isolation Plots

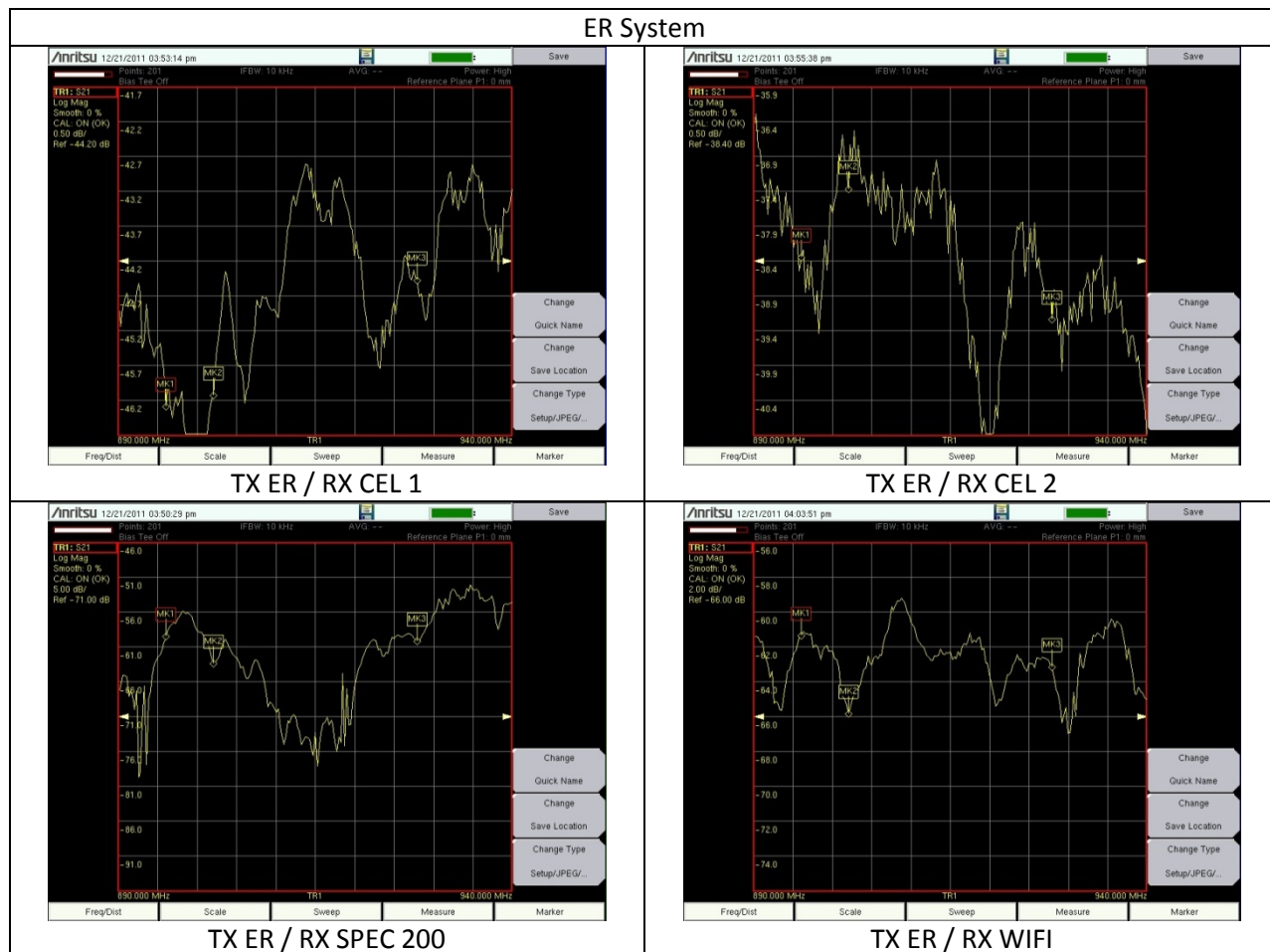


TABLE C Antenna Isolation Plots

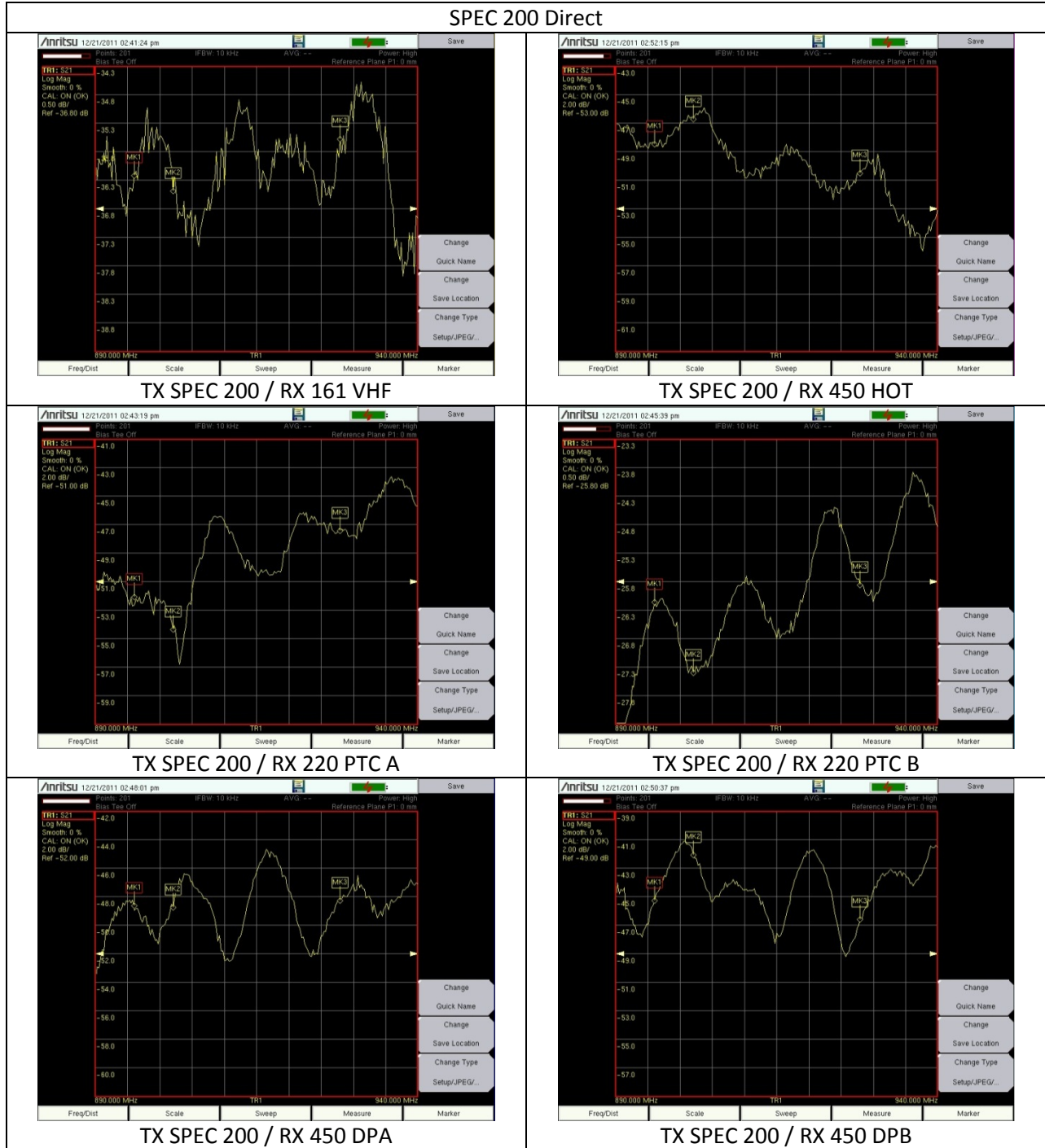


TABLE C Antenna Isolation Plots

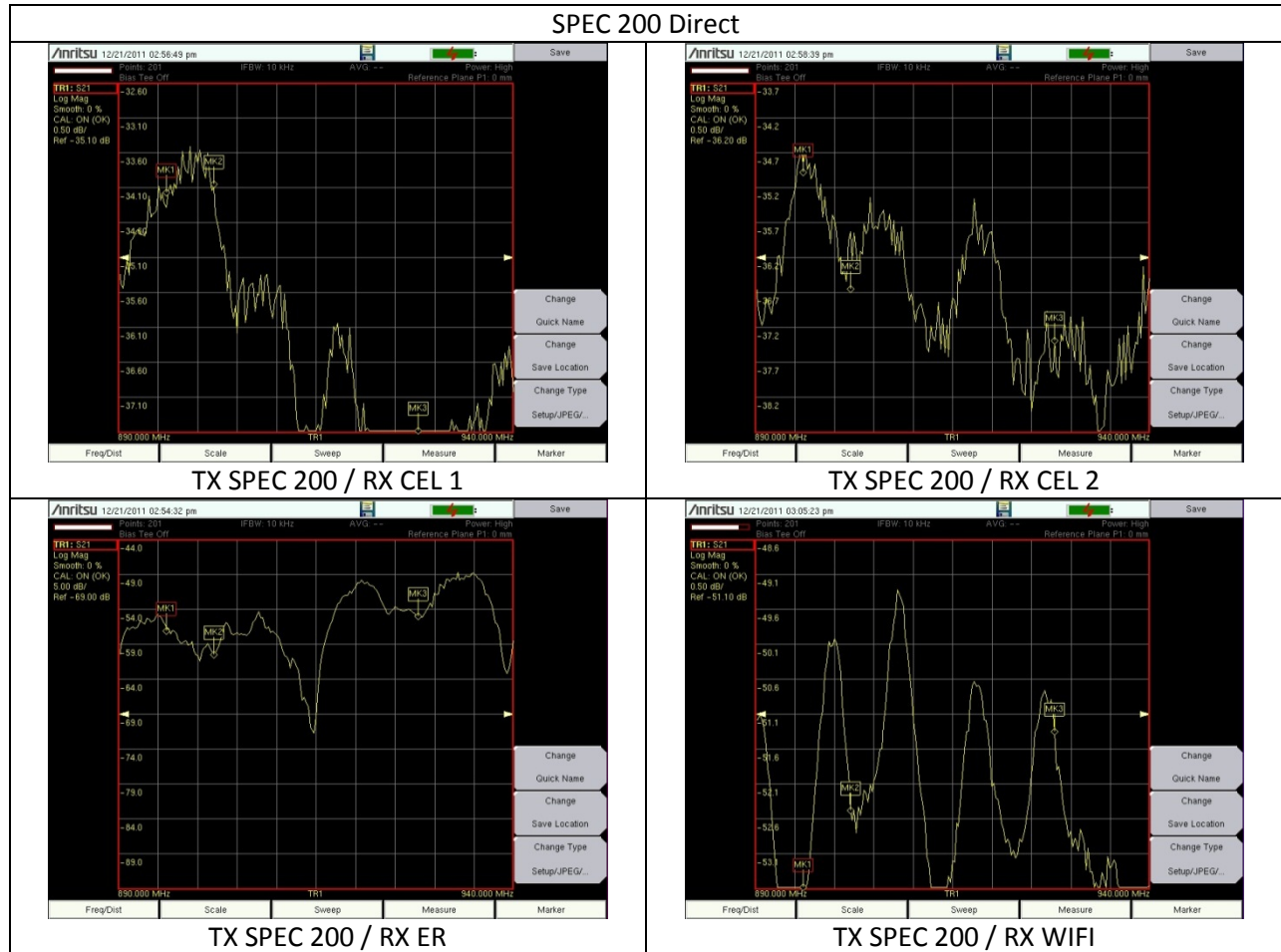




TABLE D Antenna Isolation Chart

## Antenna Isolation Report Form

Receive Band	VHF 161	220 ENG PTC B	220 CON PTC A	HOT 450	Dist. PWR A	Dist. PWR B	SPEC 2000 900	Event Record 900	CON CEL A	CON CELA DIV	ENG CEL B	ENG CEL B DIV	ACC WIFI	
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	
VHF 161	TB	-34.4	-38.8	-53.8	-54.0	-49.2	-48.8	-54.6	-43.45	-46.7	-53.42	-43.7	-53.6	
220 ENG PTC B	-33.2	TB	-20.8	-39.6	-55.7	-46.5	-39.2	-47.0	-46.3	-49.8	-58.7	-59.9	-57.2	
220 CON PTC A	-37.5	-20.4	TB	-40.4	-45.9	-55.7	-49.8	-31.8	-59.1	-58.9	-46.2	-48.5	-	
HOT 450	-28.0	-37.8	-36.6	TB	-29.9	-32.9	-41.7	-35.5	-40.7	-45.4	-37.6	-40.2	-51.9	
Dist. Power A	-27.7	-45.2	-40.0	-30.1	TB	-29.0	-57.7	-48.5	-37.7	-34.9	-28.3	-21.0	-42.1	
Dist. Power B	-27.6	-42.8	-45.8	-33.3	-29.3	TB	-40.2	-53.5	-29.0	-19.5	-37.6	-36.8	-35.1	
SPEC 2000 (900)	-36.6	-27.3	-54.0	-46.4	-48.4	-42.1	TB	-61.0	-34.3	-34.4	-36.4	-36.6	-	
Event Record (900)	-46.4	-39.7	-20.7	-39.1	-43.6	-54.2	-61.1	TB	-42.8	-47.4	-35.0	-35.0	-64.8	
Receive Band	VHF 161 Filter	220 ENG Filter	220 CON Filter	HOT 450 Filter	Dist. PWR A Filter	Dist. PWR B Filter	SPEC 2000 900	Event Record 900	CON CEL A	CON CELA DIV	ENG CEL B	ENG CEL B DIV	ACC WIFI	
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	
VHF 161 Filter	TB	-98.4	-93.6	-93.6	-90.4	-110.7	-88.5	-103.7	-44.5	-47.2	-52.9	-54.4	-53.7	
220 ENG Filter	NF	TB	-25.0	NF	NF	NF	NF	-	-	-	-	-	-	
220 CON Filter	NF	-24.9	TB	NF	NF	NF	NF	-	-	-	-	-	-	
HOT 450 Filter	NF	NF	NF	TB	NF	NF	NF	-	-	-	-	-	-	
Dist. Power A Filter	-99.4	-115.0	-98.7	-33.8	TB	-32.2	-101.5	-102.0	-37.3	-36.9	-29.9	-22.4	-44.6	
Dist. Power B Filter	-98.7	-98.8	-97.8	-36.0	-32.1	TB	-92.2	-101.4	-30.1	-20.1	-37.6	-37.1	-37.0	

Antenna Isolation Table

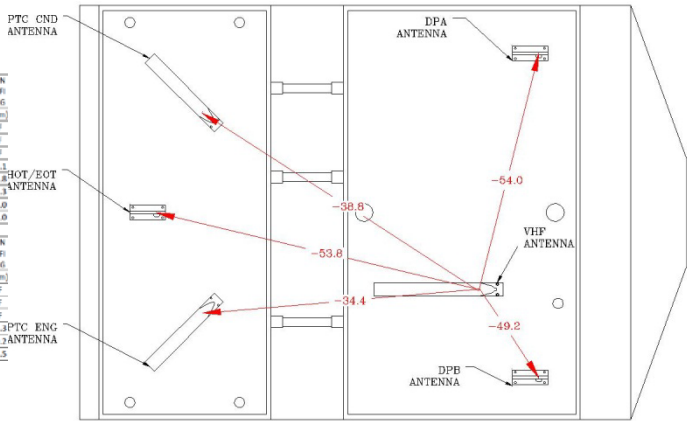
The data recorded from the locomotive included both non-filtered and filtered information if the locomotive was equipped, or if future versions were to be equipped with band specific filters.

In the set of diagrams below, the data from the chart is represented graphically. The arrows indicate where the transmission source originates. The "A" diagram shows the isolation data with no filtering and indicates the relationship between antenna spacing and free space path loss with the single element as the transmission source. The "B" diagram shows how the addition of the filters provides the increased isolation required by such a small ground plane area. The "C" diagrams indicate what energy is seen by the primary element from different frequency bands un-filtered, and again the "D" diagrams show the effect of filtering.

In addition to spatial separation, there are other factors to be considered such as the antenna element type and frequency response and filter performance which will contribute to out of band rejection characteristics, and these have been accounted for in the measurements in this section. In the cases where there is diversity or redundant antennas spaced across the locomotive, there is symmetry in the isolation numbers which tracks with the layout of the antenna elements. The data shows the improvements in isolation that can be achieved by adding filtering to the antenna system. The results here will correlate to the intermodulation data collected in later testing.

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A BLUE	ENG CEL B GRAY	ENG WFI ORG	CON CEL A BLUE	CON CEL B GRAY	CON WFI ORG
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
220 ENG	-29.7	TB	-24.3	-35.1	-35.4	-36.4	-29.7	-29.8	-37.1	-39.6	NF	-37.0	-34.6	NF
220 CON	-39.0	-34.4	TB	-35.3	-31.1	-30.8	-48.0	-41.2	-45.0	-50.0	NF	-31.3	-32.9	NF
HOT 450	-23.0	-32.1	-38.1	TB	-19.9	-20.1	-28.9	-29.2	-25.5	-34.2	-52.4	-25.5	-31.1	-40.1
Dist. Power A	-22.7	-31.1	-41.6	-19.6	TB	-19.0	-24.8	-34.2	-21.2	-21.8	-41.5	-33.0	-31.7	-54.8
Dist. Power B	-23.7	-39.8	-29.2	-20.1	-18.9	TB	-24.7	-24.9	-34.7	-34.3	-53.0	-23.9	-29.8	-44.3
ATCS 900	-34.0	-32.1	-32.5	-30.0	-34.0	-32.5	TB	-17.9	-28.0	-30.0	-33.0	-26.8	-26.9	-32.0
YARD 900	-34.6	-32.0	-31.0	-31.1	-35.0	-31.7	-17.4	TB	-28.3	-29.4	-31.1	-25.6	-25.6	-31.0

Receive Band	VHF 161 Filter	220 ENG Filter	220 CON Filter	HOT 450 Filter	Dist. PWR A Filter	Dist. PWR B Filter	ATCS 900	YARD 900	ENG CEL A BLUE	ENG CEL B GRAY	ENG WFI ORG	CON CEL A BLUE	CON CEL B GRAY	CON WFI ORG
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
VHF 161 Filter	TB	NF	NF	NF	NF	NF	-	-	31.2	39.0	-40.5	NF	39.0	40.2
220 ENG Filter	NF	TB	NF	NF	NF	NF	-	-	-49.0	-35.7	-38.7	NF	-48.1	-45.5
220 CON Filter	NF	-29.3	TB	NF	NF	NF	-	-	-44.6	-47.1	-55.0	NF	-34.7	-38.1
HOT 450 Filter	NF	NF	NF	TB	-24.1	-23.6	-	-	-32.4	-32.5	-36.5	-52.6	-27.8	-30.5
Dist. Power A Filter	NF	NF	NF	TB	-24.1	-23.5	-	-	-40.9	-26.2	-26.3	-44.1	-35.7	-42.0
Dist. Power B Filter	NF	NF	NF	TB	-23.7	-23.5	TB	-	-28.0	-35.0	-36.2	-53.7	-27.6	-35.1

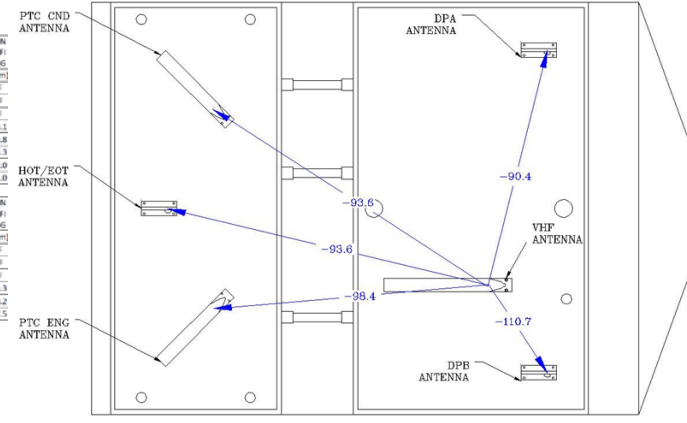


Transmit Energy is Single Frequency Band  
Un-filtered

Transmit from single source  
Unfiltered

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A BLUE	ENG CEL B GRAY	ENG WFI ORG	CON CEL A BLUE	CON CEL B GRAY	CON WFI ORG
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
VHF 161	TB	-33.0	-35.0	-28.0	-31.8	-31.5	-29.7	-29.8	-37.1	-39.6	NF	-37.0	-34.6	NF
220 ENG	-39.7	TB	-24.3	-35.1	-35.6	-36.6	-47.5	-45.3	-32.0	-36.0	NF	-45.7	-41.7	NF
220 CON	-39.0	-34.4	TB	-35.3	-31.1	-30.8	-48.0	-41.2	-45.0	-50.0	NF	-31.3	-32.9	NF
HOT 450	-23.0	-32.1	-38.1	TB	-19.9	-20.1	-28.9	-29.2	-25.5	-34.2	-52.4	-25.5	-31.1	-40.1
Dist. Power A	-22.7	-31.1	-41.6	-19.6	TB	-19.0	-24.8	-34.2	-21.2	-21.8	-41.5	-33.0	-31.7	-54.8
Dist. Power B	-23.7	-39.8	-29.2	-20.1	-18.9	TB	-24.7	-24.9	-34.7	-34.3	-53.0	-23.9	-29.8	-44.3
ATCS 900	-34.0	-32.1	-32.5	-30.0	-34.0	-32.5	TB	-17.9	-28.0	-30.0	-33.0	-26.8	-26.9	-32.0
YARD 900	-34.6	-32.0	-31.0	-31.1	-35.0	-31.7	-17.4	TB	-28.3	-29.4	-31.1	-25.6	-25.6	-31.0

Receive Band	VHF 161 Filter	220 ENG Filter	220 CON Filter	HOT 450 Filter	Dist. PWR A Filter	Dist. PWR B Filter	ATCS 900	YARD 900	ENG CEL A BLUE	ENG CEL B GRAY	ENG WFI ORG	CON CEL A BLUE	CON CEL B GRAY	CON WFI ORG
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
VHF 161 Filter	TB	NF	NF	NF	NF	NF	-	-	31.2	39.0	-40.5	NF	39.0	40.2
220 ENG Filter	NF	TB	-29.1	NF	NF	NF	-	-	-49.0	-35.7	-38.7	NF	-48.1	-45.5
220 CON Filter	NF	-29.3	TB	NF	NF	NF	-	-	-44.6	-47.1	-55.0	NF	-34.7	-38.1
HOT 450 Filter	NF	NF	NF	TB	-24.1	-23.6	-	-	-32.4	-32.5	-36.5	-52.6	-27.8	-30.5
Dist. Power A Filter	NF	NF	NF	TB	-24.1	-23.5	-	-	-40.9	-26.2	-26.3	-44.1	-35.7	-42.0
Dist. Power B Filter	NF	NF	NF	TB	-23.7	-23.5	TB	-	-28.0	-35.0	-36.2	-53.7	-27.6	-35.1



Transmit Energy is Single Frequency Band  
Filtered

Transmit from single source  
Filtered

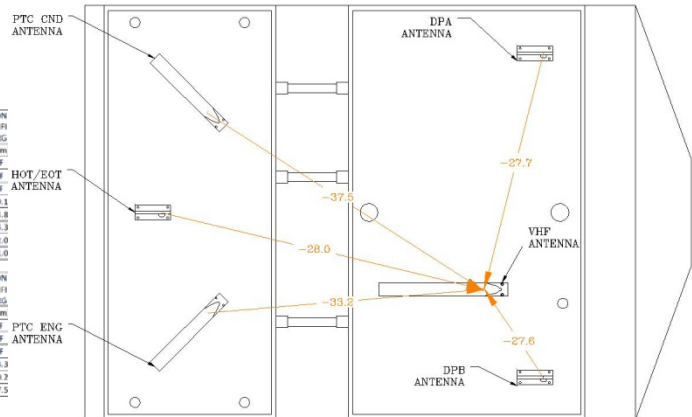
# UP 5802 (AC44CWCTE-GE) Locomotive Noise Test Battery Report

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A	ENG CEL B	ENG WFI	CON CEL A	CON CEL B	CON WFI	
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	
VHF 161	TB	-33.0	-35.0	-28.0	-31.8	-31.5	-29.7	-29.8	-37.1	-39.6	NF	-37.0	-38.6	NF	
220 ENG	TB	-39.7	TB	-24.3	-35.1	-35.6	-36.4	-47.5	-46.3	-32.0	-36.0	NF	-45.7	-41.7	NF
220 CON	TB	-37.6	-34.4	TB	-35.3	-31.1	-30.8	-48.0	-43.2	-45.0	-50.0	NF	-31.3	-32.9	NF
HOT 450	TB	-23.0	-32.1	-38.1	TB	-19.9	-20.1	-28.9	-25.5	-34.2	-32.4	-25.5	-31.1	-49.1	
Dist. Power A	TB	-22.2	-31.1	-41.6	-19.9	TB	-19.0	-24.8	-34.2	-23.2	-21.8	-41.5	-33.0	-35.7	-54.8
Dist. Power B	TB	-22.7	-35.8	-29.2	-20.1	-18.0	TB	-24.7	-24.9	-34.7	-34.1	-53.0	-23.9	-29.8	-44.3
ATCS 900	TB	-34.0	-32.1	-32.5	-30.0	-34.0	-32.5	TB	-17.6	-28.0	-30.0	-31.0	-26.8	-26.0	-32.0
YARD 900	TB	-34.6	-32.9	-31.0	-31.1	-35.0	-31.7	TB	-28.3	-29.4	-31.3	-26.6	-26.6	-33.0	

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A	ENG CEL B	ENG WFI	CON CEL A	CON CEL B	CON WFI
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
VHF 161 Filter	TB	NF	NF	NF	NF	NF	-	-31.2	-39.0	-40.5	NF	-39.0	-40.2	NF
220 ENG Filter	NF	TB	-29.1	NF	NF	NF	-	-49.0	-35.7	-38.7	NF	-48.1	-45.5	NF
220 CON Filter	NF	-29.1	TB	NF	NF	NF	-	-44.6	-47.1	-55.0	NF	-34.7	-36.1	NF
HOT 450 Filter	NF	NF	NF	TB	-24.1	-23.6	-	-32.4	-32.5	-36.3	-32.6	-27.8	-26.5	-33.3
Dist. Power A Filter	NF	NF	NF	TB	-24.1	-23.5	-	-40.9	-36.2	-36.3	-44.1	-35.7	-43.0	-40.2
Dist. Power B Filter	NF	NF	NF	-23.7	-23.5	TB	-	-28.0	-35.0	-36.2	-33.7	-27.6	-36.1	-47.5

Receive Energy is Multiple Frequency Bands  
Unfiltered



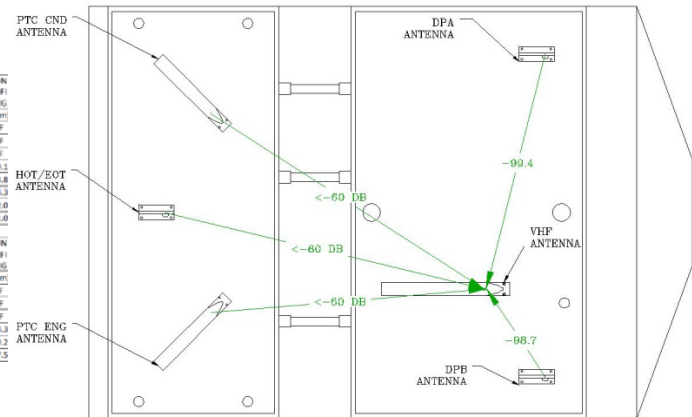
Receive from multiple sources  
Unfiltered

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A	ENG CEL B	ENG WFI	CON CEL A	CON CEL B	CON WFI	
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	
VHF 161	TB	-33.0	-35.0	-28.0	-31.8	-31.5	-29.7	-29.8	-37.1	-39.6	NF	-37.0	-38.6	NF	
220 ENG	TB	-39.7	TB	-24.3	-35.1	-35.6	-36.4	-47.5	-46.3	-32.0	-36.0	NF	-45.7	-41.7	NF
220 CON	TB	-37.6	-34.4	TB	-35.3	-31.1	-30.8	-48.0	-43.2	-45.0	-50.0	NF	-31.3	-32.9	NF
HOT 450	TB	-23.0	-32.1	-38.1	TB	-19.9	-20.1	-28.9	-25.5	-34.2	-32.4	-25.5	-31.1	-49.1	
Dist. Power A	TB	-22.2	-31.1	-41.6	-19.9	TB	-19.0	-24.8	-34.2	-23.2	-21.8	-41.5	-33.0	-35.7	-54.8
Dist. Power B	TB	-22.7	-35.8	-29.2	-20.1	-18.0	TB	-24.7	-24.9	-34.7	-34.1	-53.0	-23.9	-29.8	-44.3
ATCS 900	TB	-34.0	-32.1	-32.5	-30.0	-34.0	-32.5	TB	-17.6	-28.0	-30.0	-31.0	-26.8	-26.0	-32.0
YARD 900	TB	-34.6	-32.9	-31.0	-31.1	-35.0	-31.7	TB	-28.3	-29.4	-31.3	-26.6	-26.6	-33.0	

Receive Band	VHF 161	220 ENG	220 CON	HOT 450	Dist. PWR A	Dist. PWR B	ATCS 900	YARD 900	ENG CEL A	ENG CEL B	ENG WFI	CON CEL A	CON CEL B	CON WFI
Transmit Band	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)	(dBm)
VHF 161 Filter	TB	NF	NF	NF	NF	NF	-	-31.2	-39.0	-40.5	NF	-39.0	-40.2	NF
220 ENG Filter	NF	TB	-29.1	NF	NF	NF	-	-49.0	-35.7	-38.7	NF	-48.1	-45.5	NF
220 CON Filter	NF	-29.1	TB	NF	NF	NF	-	-44.6	-47.1	-55.0	NF	-34.7	-36.1	NF
HOT 450 Filter	NF	NF	NF	TB	-24.1	-23.6	-	-32.4	-32.5	-36.3	-32.6	-27.8	-26.5	-33.3
Dist. Power A Filter	NF	NF	NF	TB	-24.1	-23.5	-	-40.9	-36.2	-36.3	-44.1	-35.7	-43.0	-40.2
Dist. Power B Filter	NF	NF	NF	-23.7	-23.5	TB	-	-28.0	-35.0	-36.2	-33.7	-27.6	-36.1	-47.5

Receive Energy is Multiple Frequency Bands  
Filtered



Receive from multiple sources  
Filtered

UP 5802 Antenna Isolation  
VHF XMIT Mapping

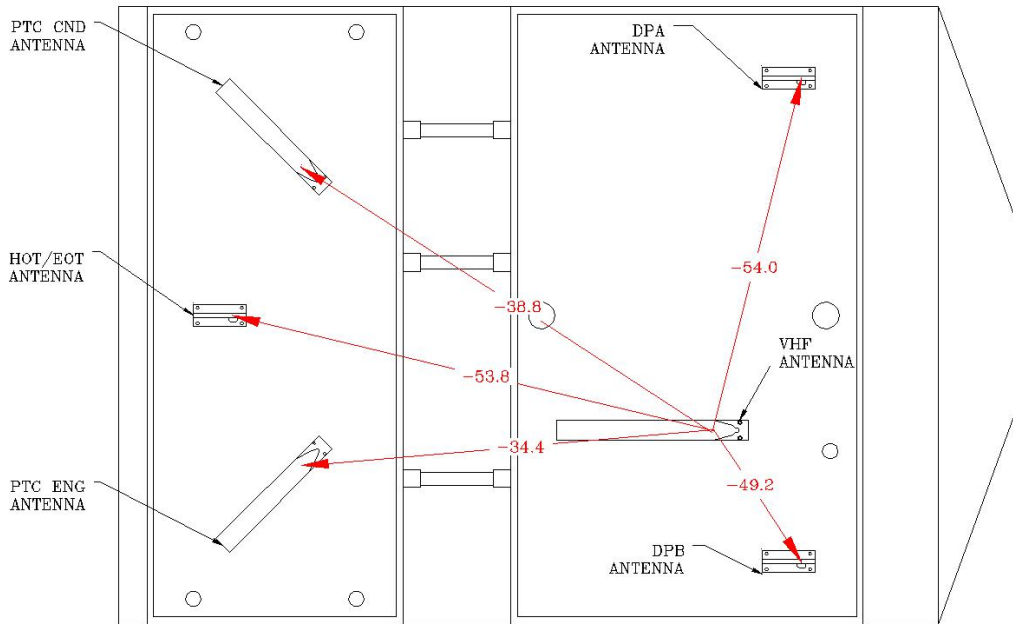


Figure 17 A  
Non-Filtered

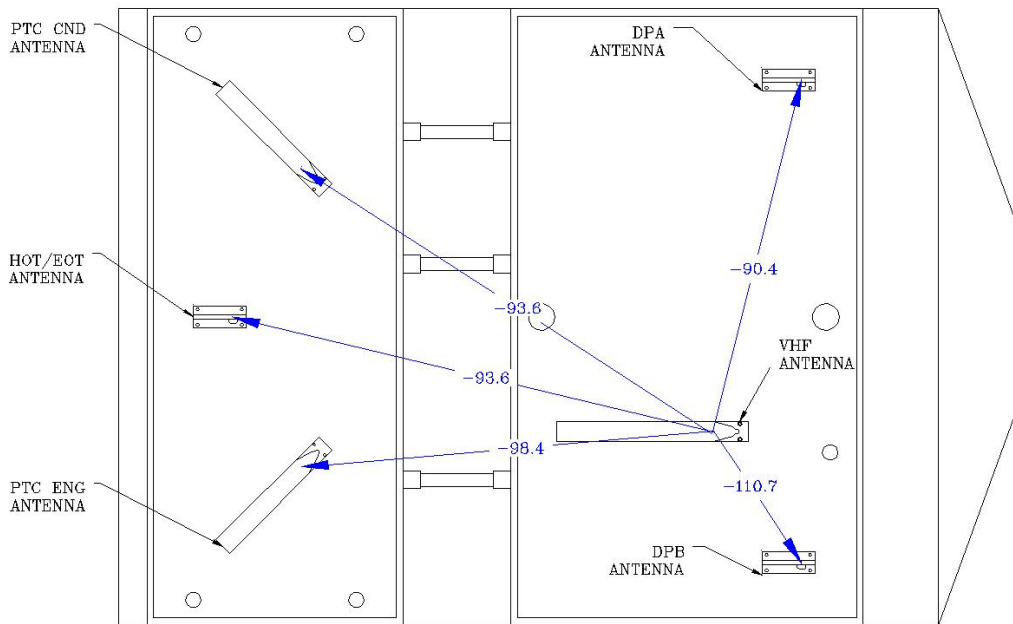


Figure 17 B  
Filtered

UP 5802 Antenna Isolation  
VHF RCV Mapping

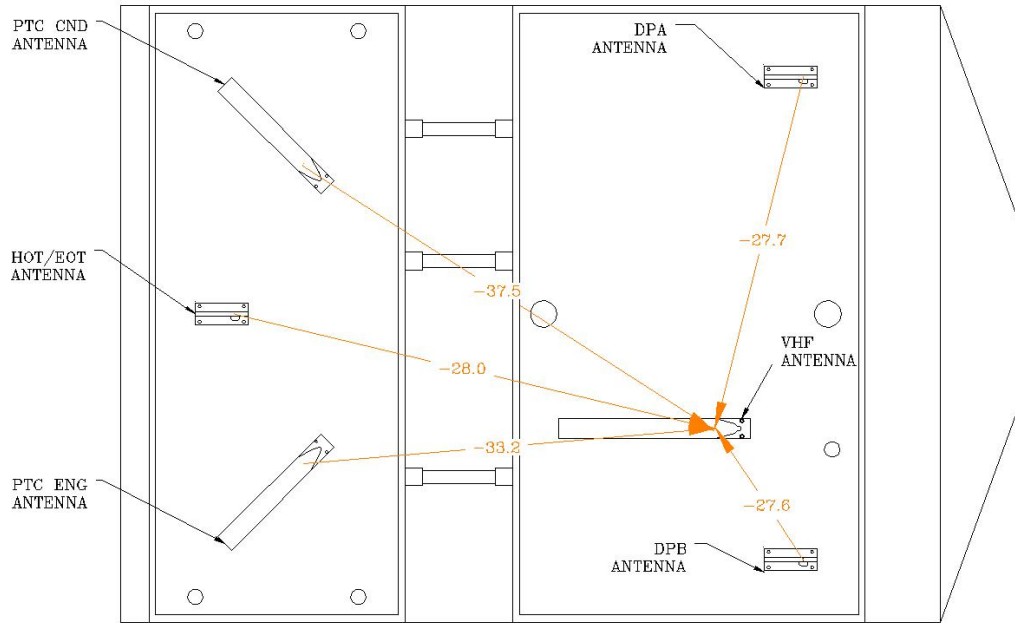


Figure 17 C  
Non-Filtered

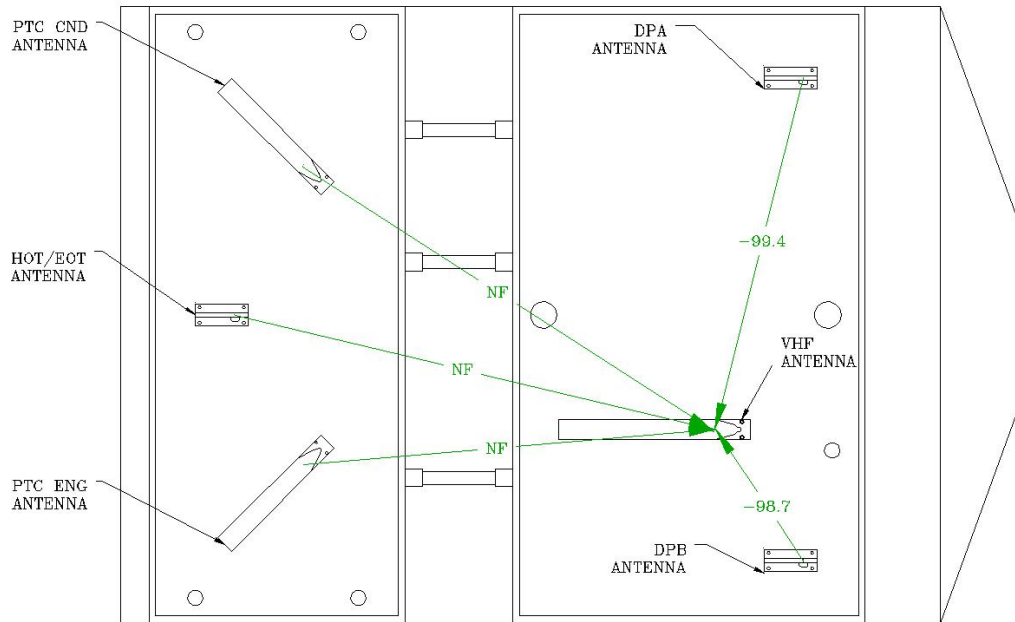


Figure 17 D  
Filtered

UP 5802 Antenna Isolation  
PTC ENG XMIT Mapping

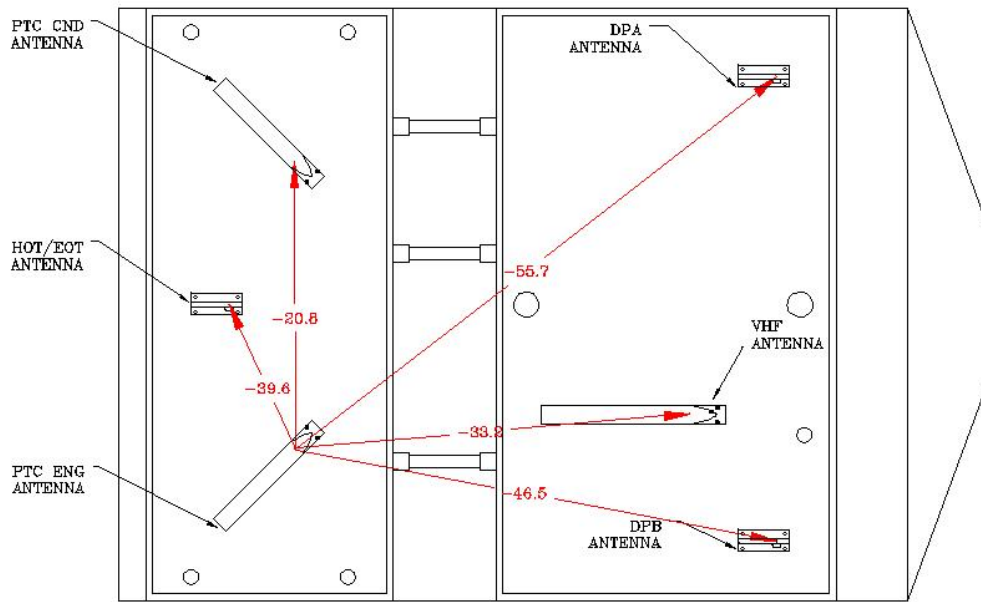


Figure 18 A  
Non-Filtered

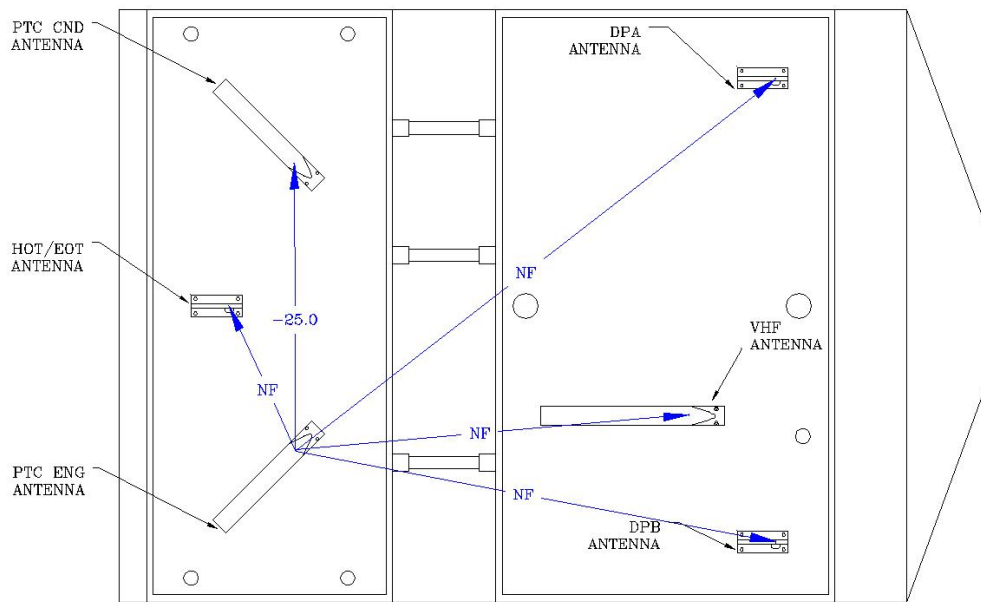


Figure 18 B  
Filtered

UP 5802 Antenna Isolation  
PTC ENG RCV Mapping

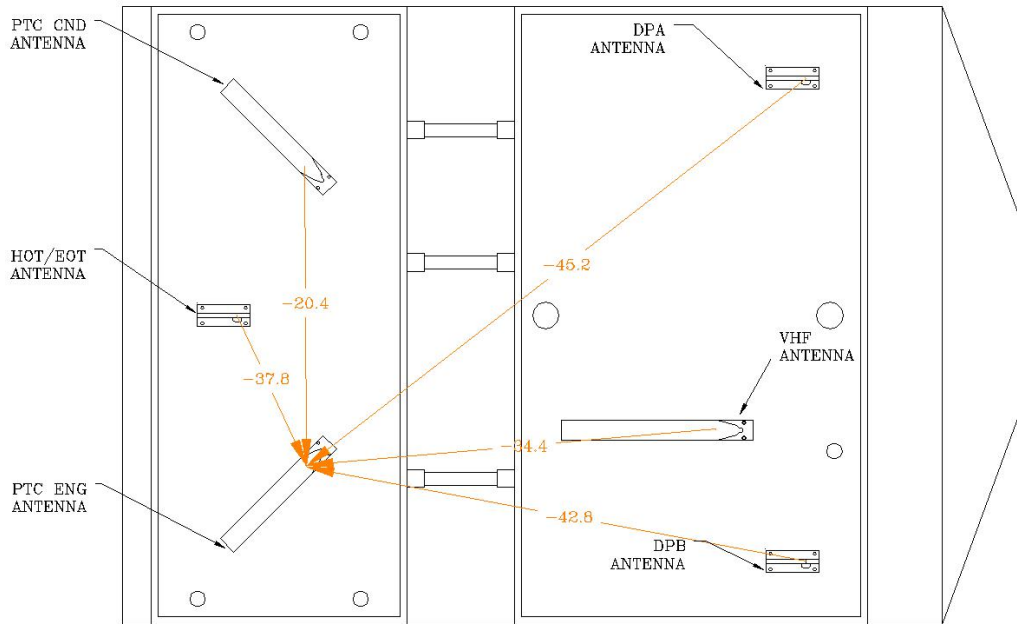


Figure 18 C  
Non-Filtered

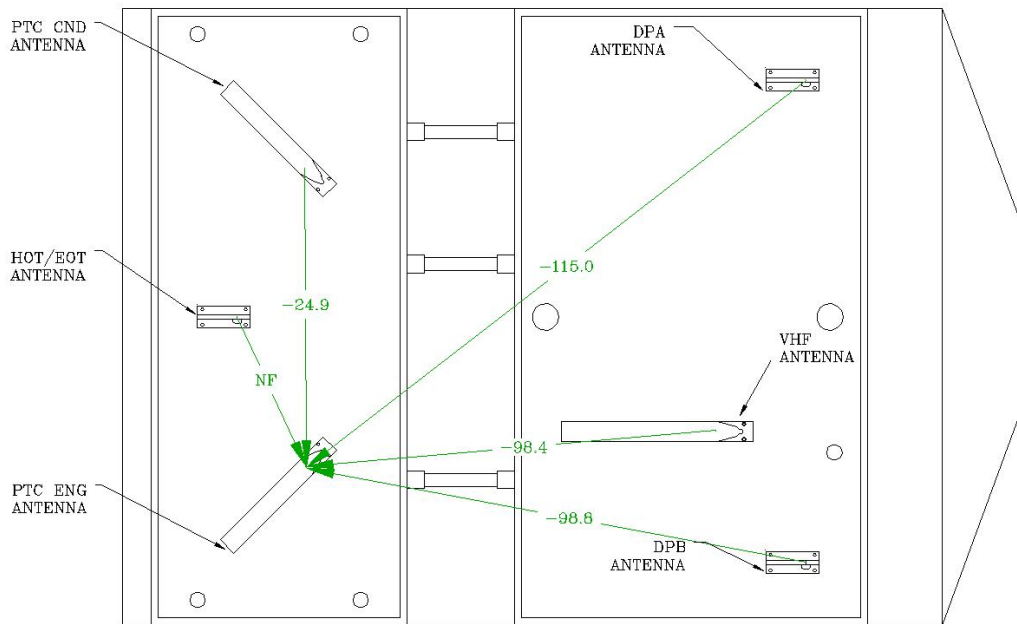


Figure 18 D  
Filtered



UP 5802 Antenna Isolation  
PTC CND XMIT Mapping

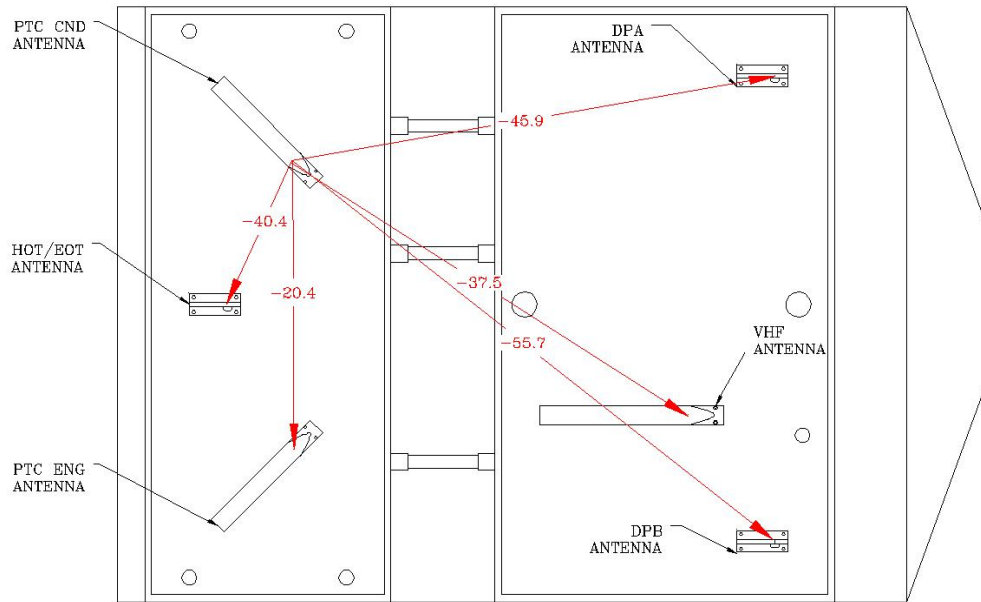


Figure 19 A  
Non-Filtered

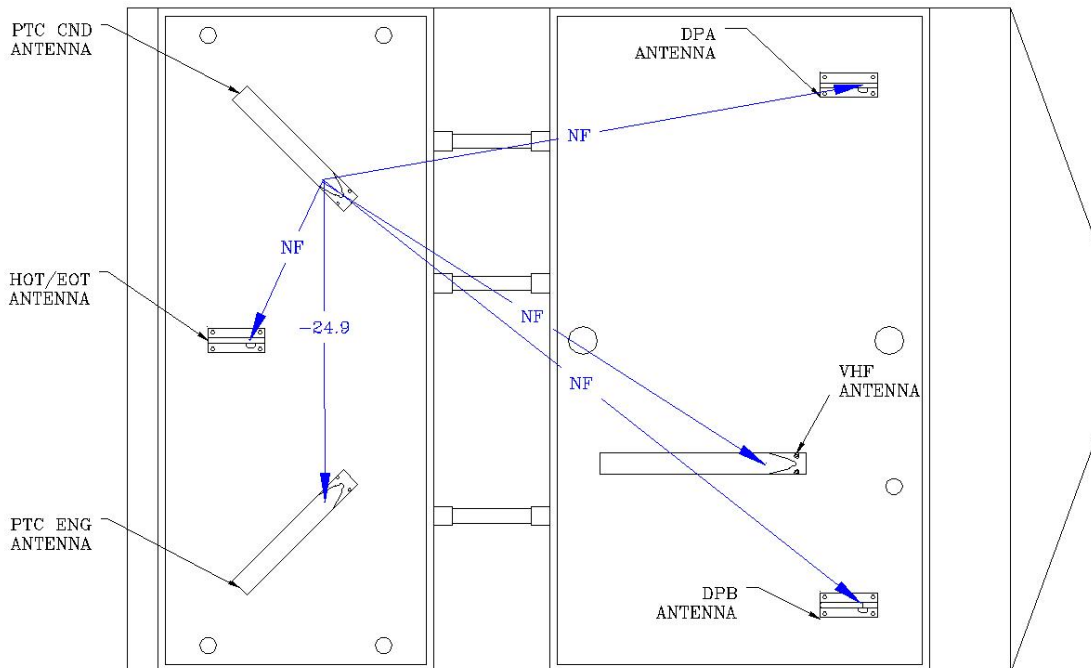


Figure 19 B  
Filtered

UP 5802 Antenna Isolation  
PTC CND RCV Mapping

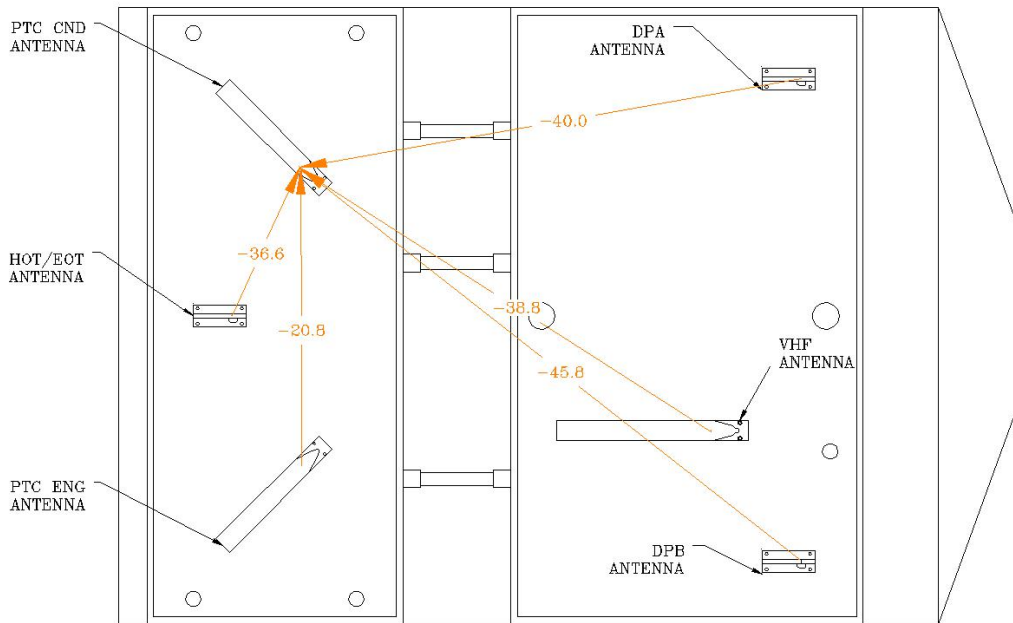


Figure 19 C  
Non-Filtered

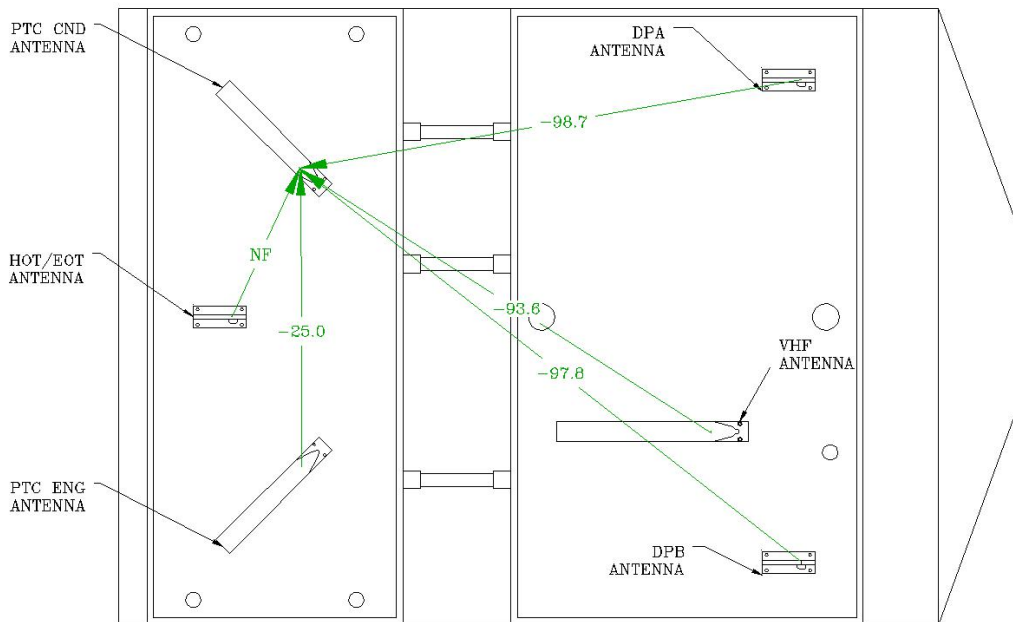


Figure 19 D  
Filtered

UP 5802 Antenna Isolation  
HOT XMIT Mapping

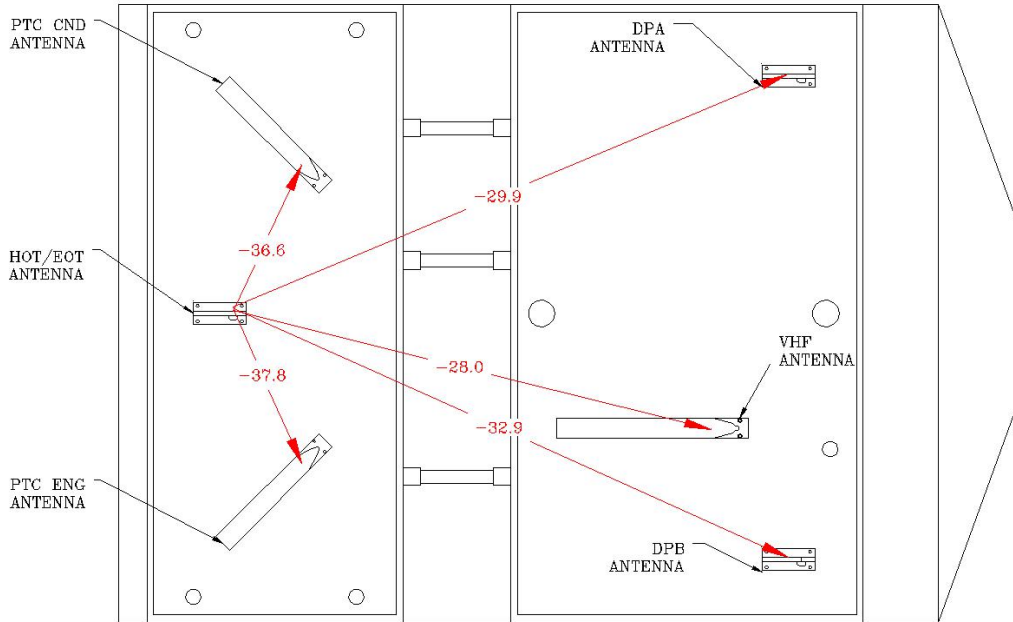


Figure 20 A  
Non-Filtered

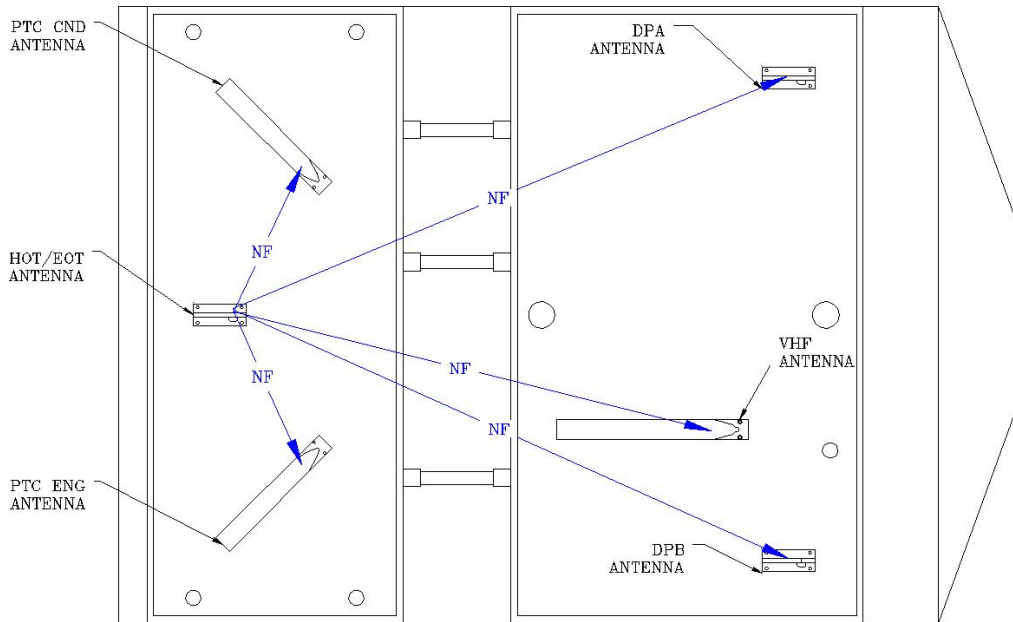


Figure 20 B  
Filtered

UP 5802 Antenna Isolation  
HOT RCV Mapping

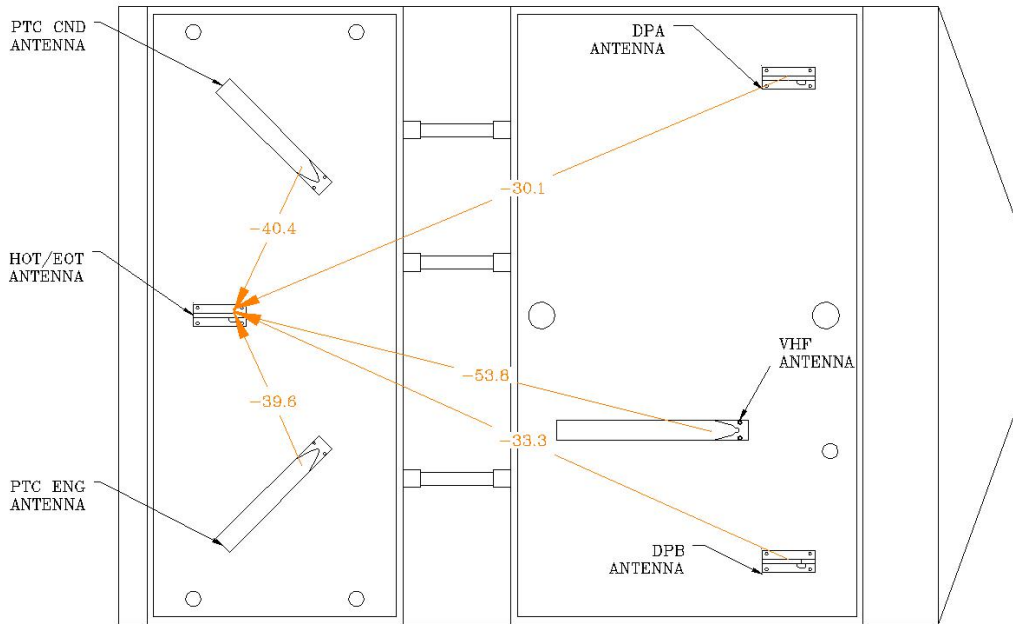


Figure 20 C  
Non-Filtered

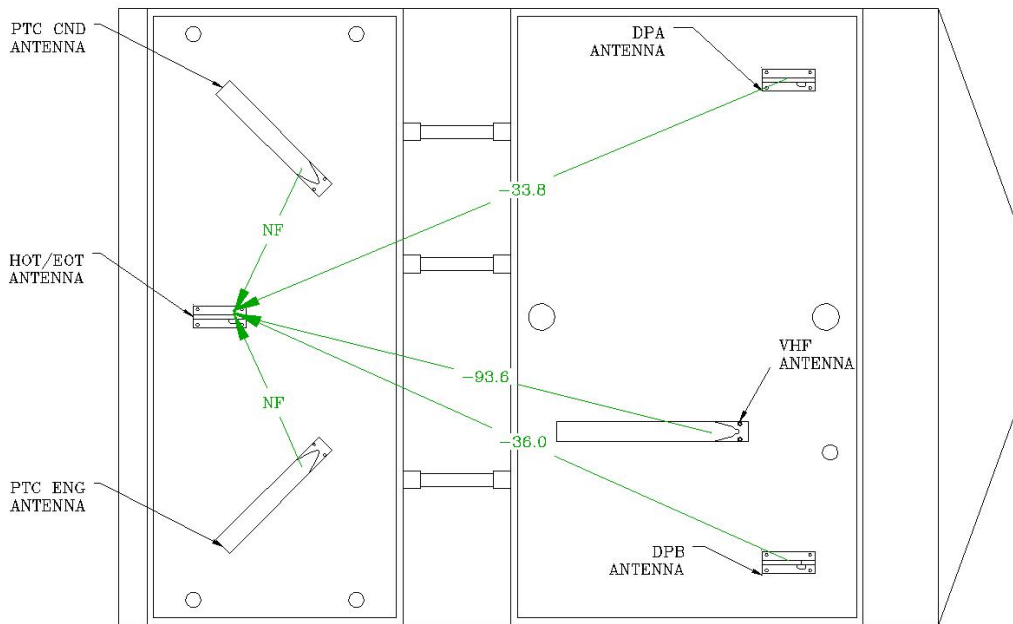


Figure 20 D  
Filtered

UP 5802 Antenna Isolation  
DPA XMIT Mapping

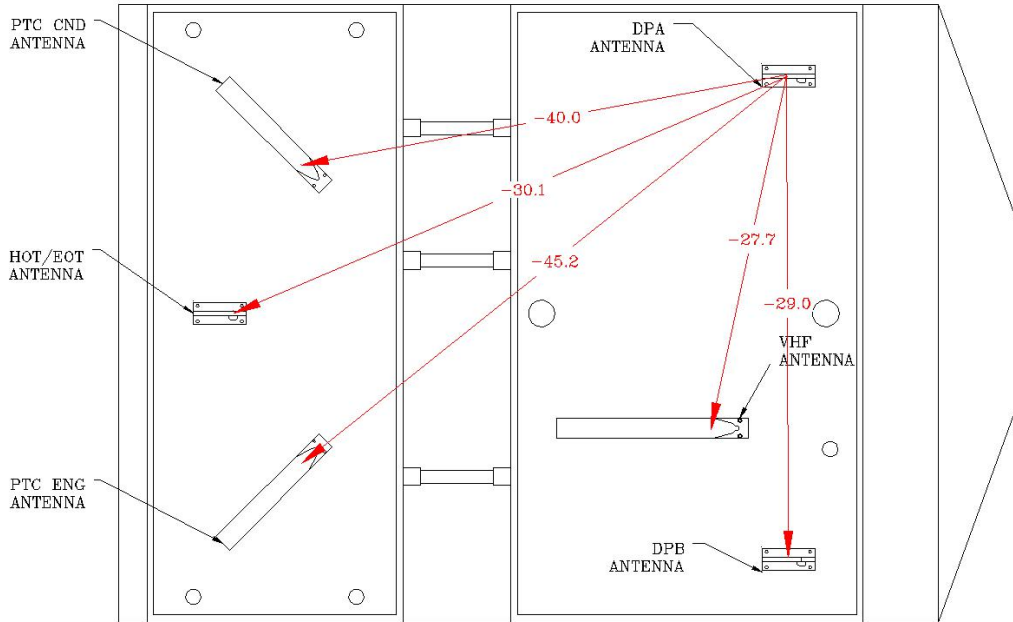


Figure 21 A  
Non-Filtered

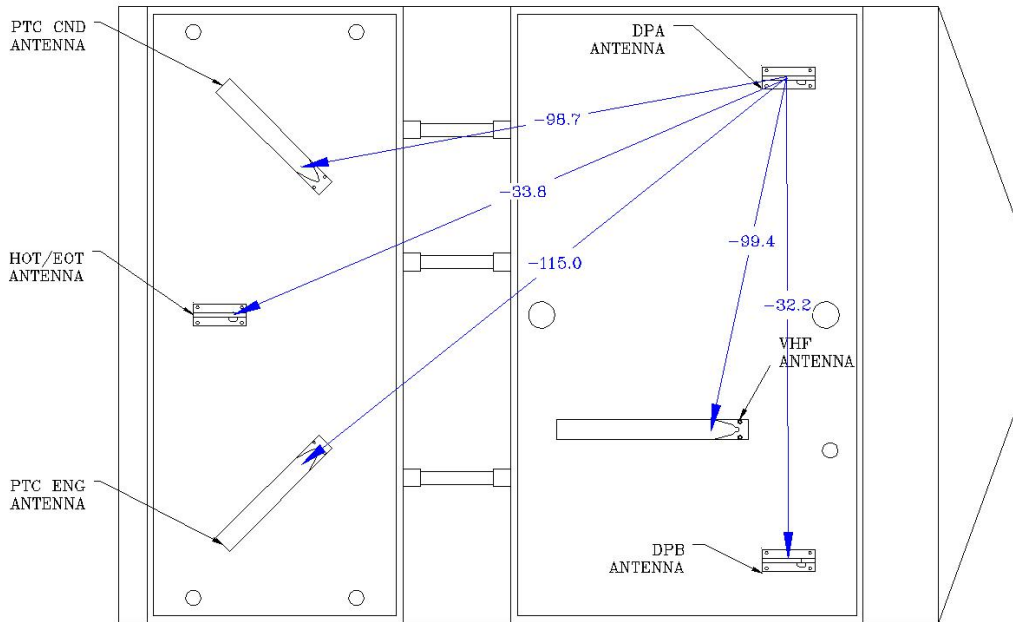


Figure 21 B  
Filtered

UP 5802 Antenna Isolation  
DPA RCV Mapping

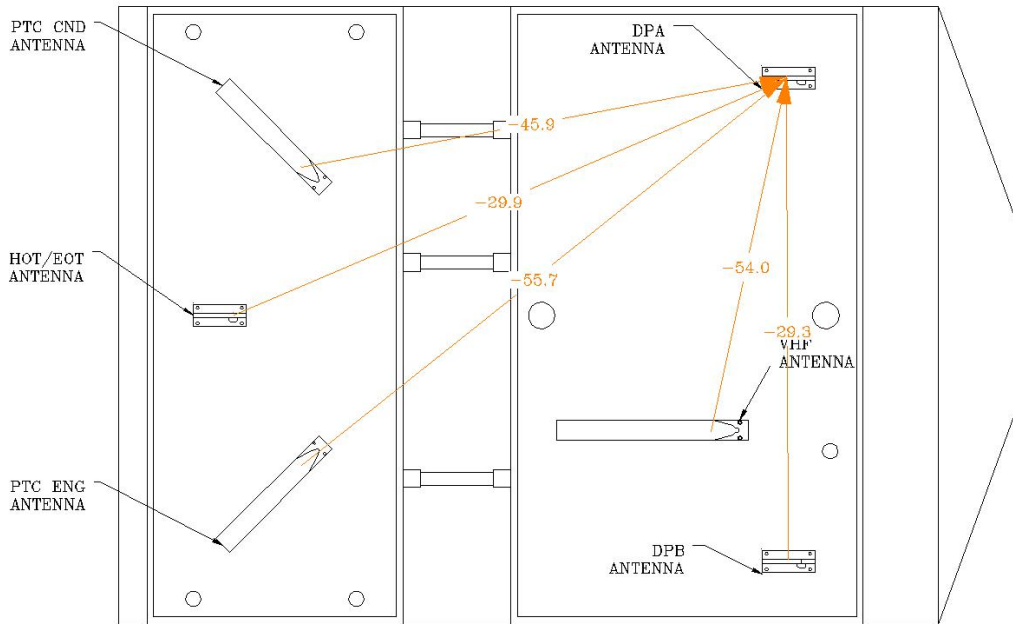


Figure 21 C  
Non-Filtered

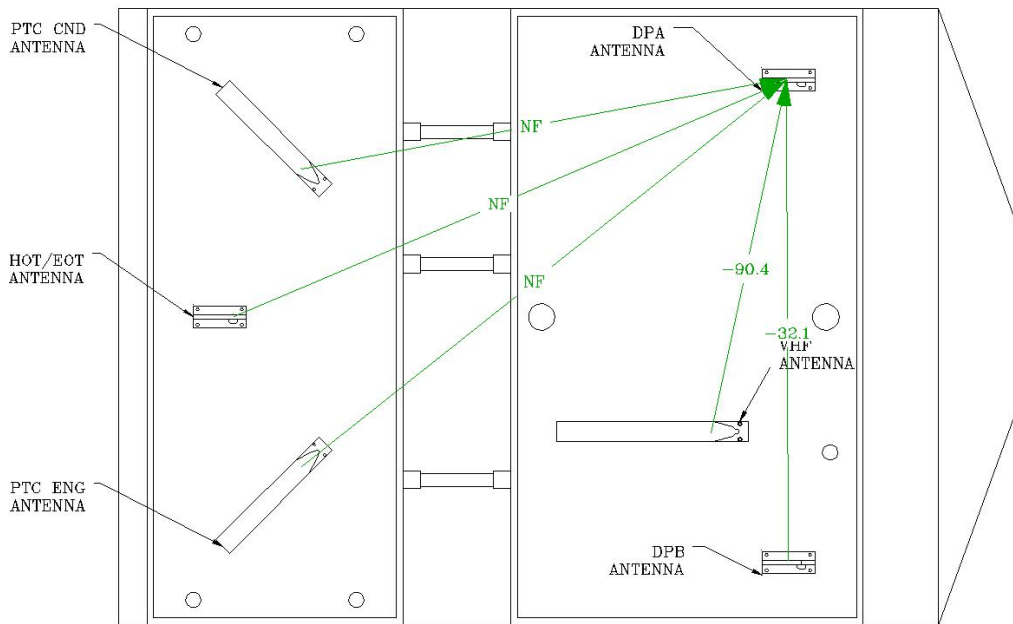


Figure 21 D  
Filtered

UP 5802 Antenna Isolation  
DPB XMIT Mapping

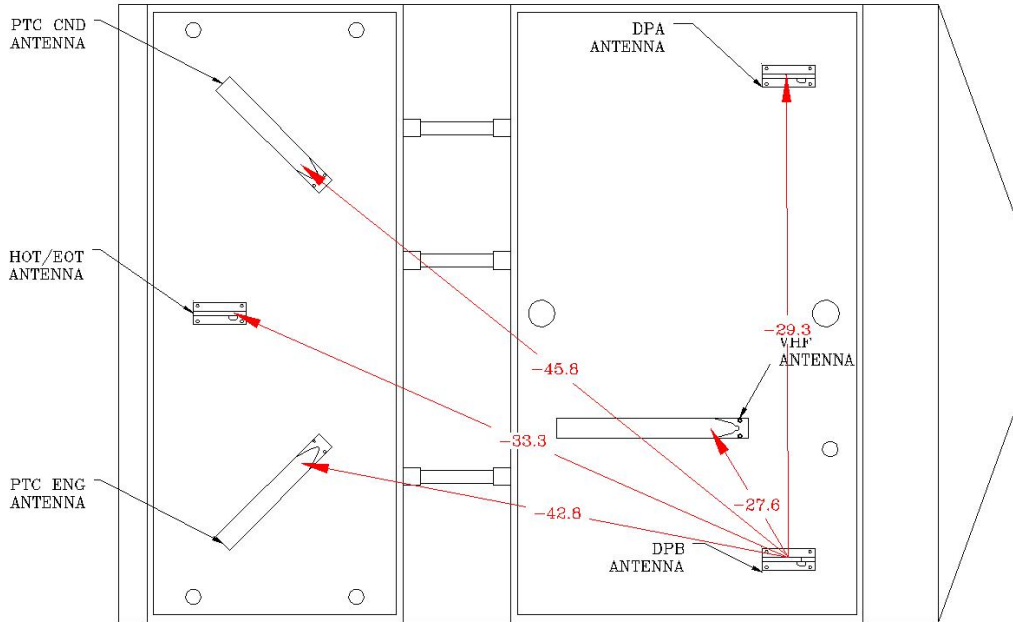


Figure 22 A  
Non-Filtered

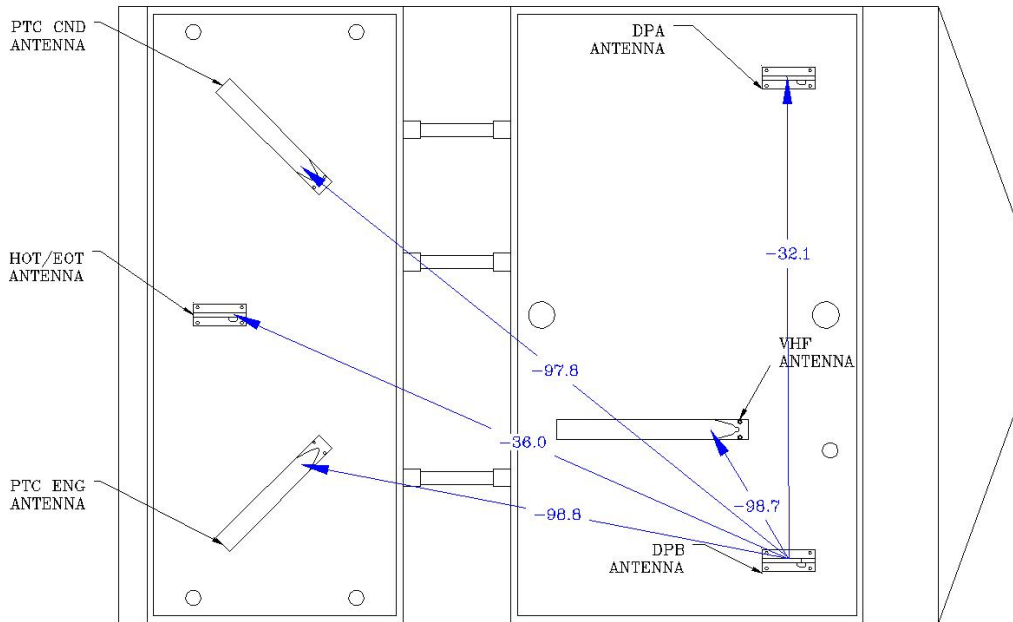


Figure 22 B  
Filtered

UP 5802 Antenna Isolation  
DPB XMIT Mapping

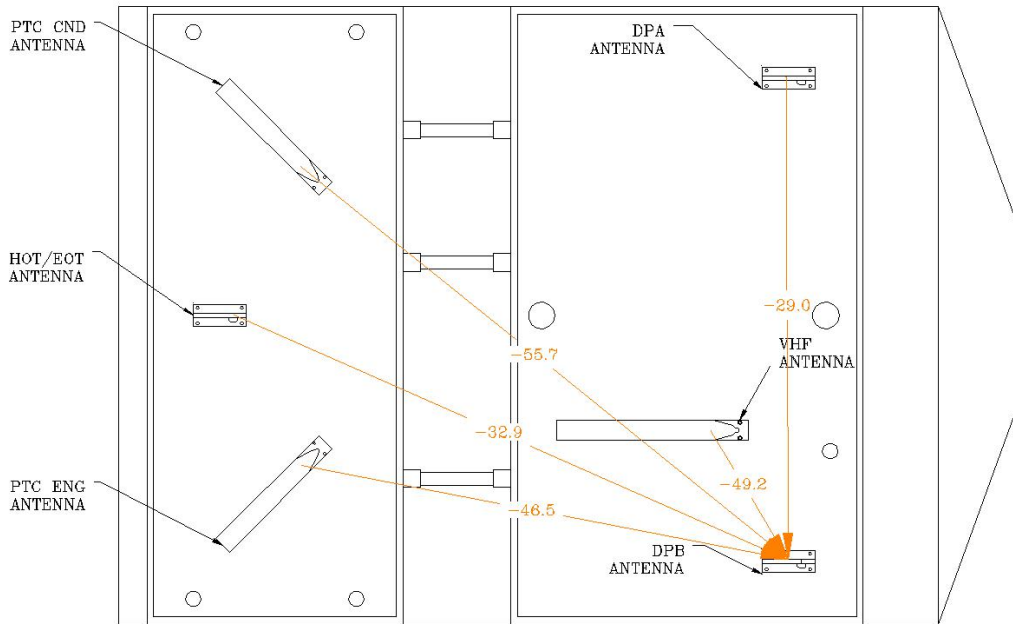


Figure 22 C  
Non-Filtered

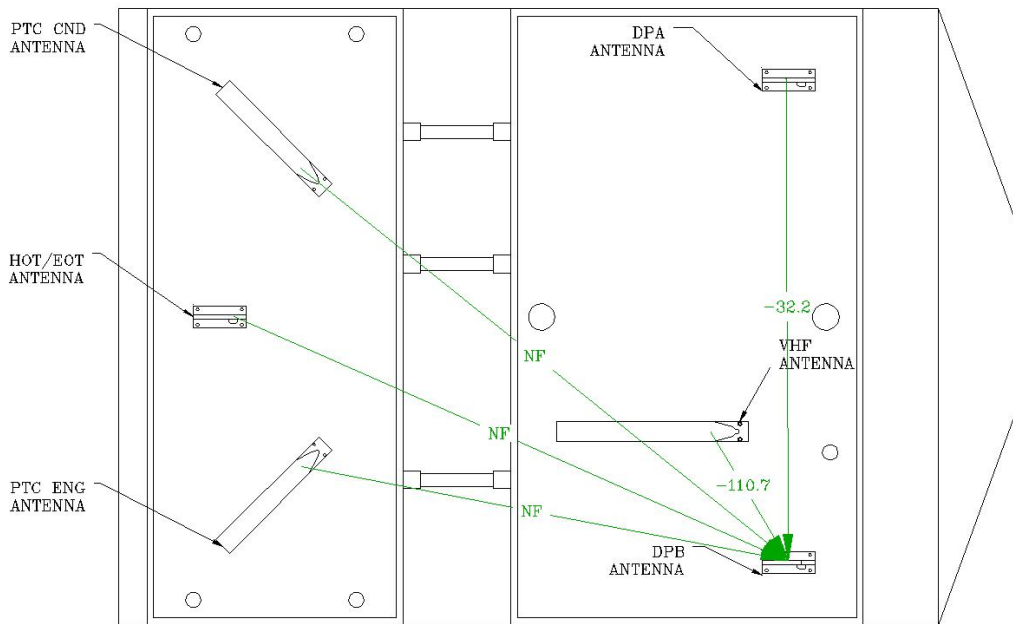


Figure 22 D  
Filtered



## Receive Intermodulation Test

This test provides information on intermodulation products generated at the front end of each radio receiver when it is impacted by high power signals from the transmitting radio.

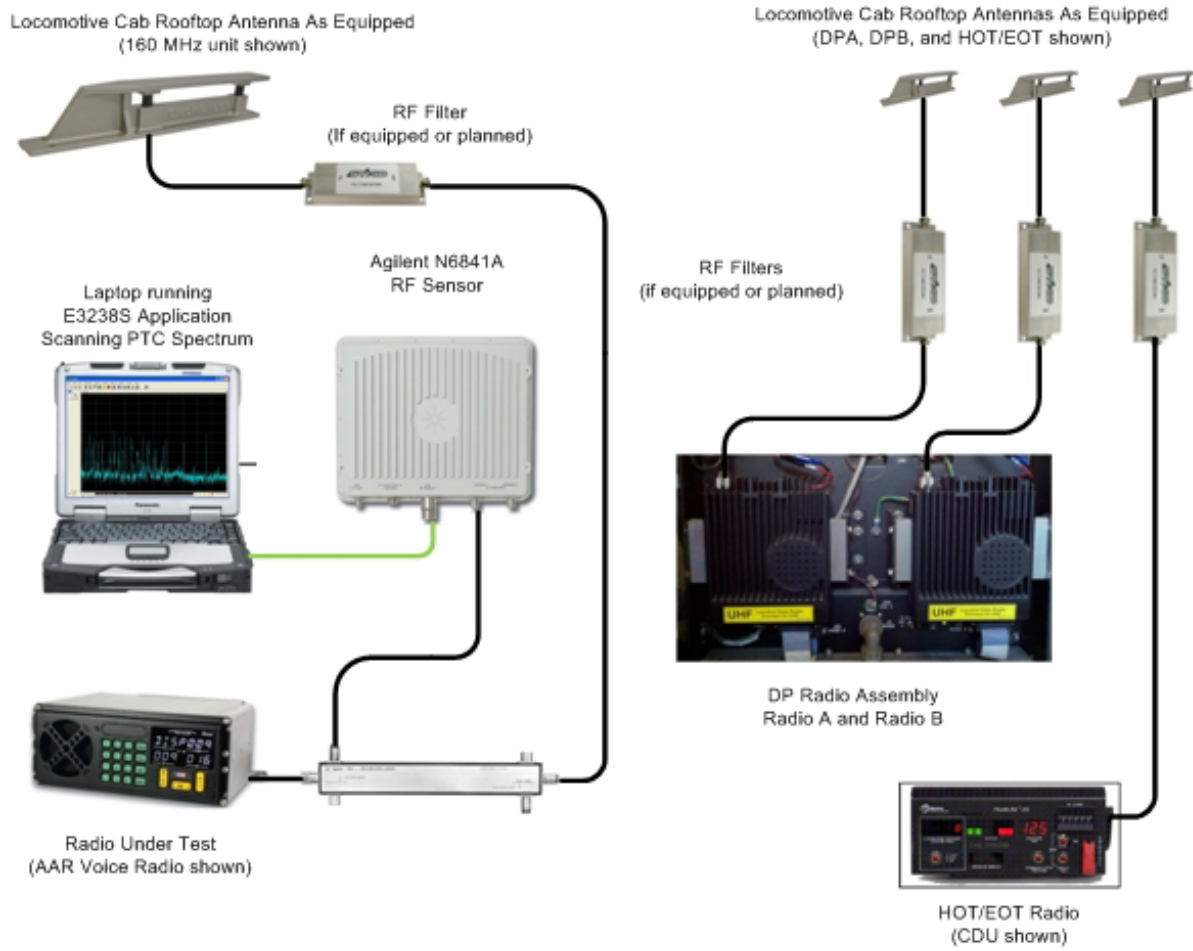
Each of the on board radios transmits at nominal power, and using a dual directional coupler the radio under test is measured for the amount of intermodulation products generated at the front end of the radio receiver and re-radiated back through the same antenna. Note that the radio under test is not transmitting.

A Dual Directional Coupler rated for a maximum power handling of 500 Watts was used to separately measure signals coming from the antenna to the radio receiver front end, and from the receiver front end travelling to the antenna and being transmitted as intermodulation products.

This Dual Directional Coupler has six ports, one for Antenna, one for Radio, two for 50 ohms loads, one to measure signals coming from the antenna to the radio transceiver, and one port to measure signals from the radio transceiver to the antenna.

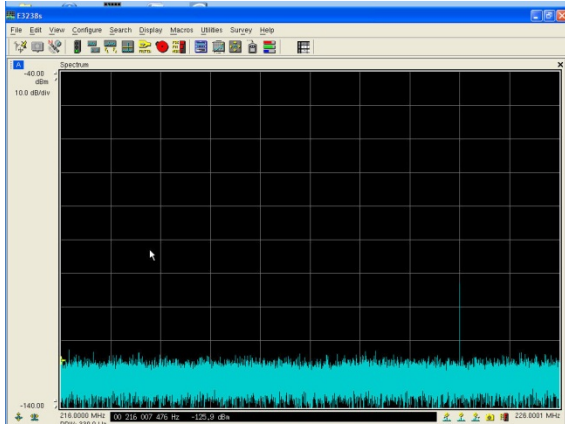
In the IMD Test Apparatus diagram, the initial radio under test shown is the AAR Voice Radio, operating at ~ 160 MHz. Its Receiver is coupled directly to its existing transmission path, including Antenna (and Filter, if equipped or planned). The RF Sensor is coupled 20 dB down to the Receiver in the Radio under Test. The other radios of interest on the Locomotive (DPA, DPB, and HOT/EOT) are then keyed and RF energy from those radios pass through their respective existing transmission paths, including Antennas (and Filters, if equipped or planned). The RF energy then propagates into the Antenna of the Radio under Test, and then into the Receiver under test. Any IMD products in the 220 MHz spectrum generated in the Receiver that would be propagated via the Antenna system are measured by the RF Sensor.

A permutation of the IMD Test Apparatus is configured for each of the other radios of interest (DPA, DPB, and HOT/EOT), so that each of them is connected as a Radio under Test, and the process is repeated.

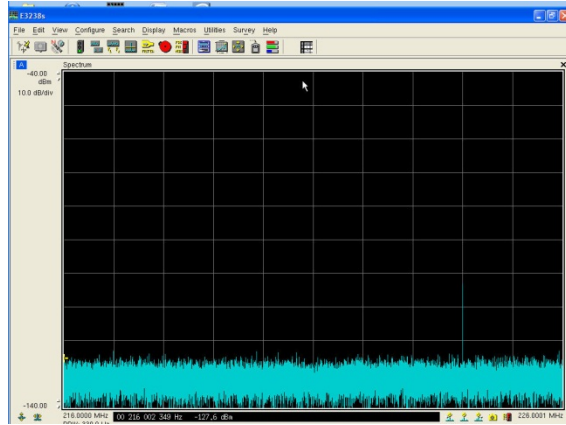


Receive Intermodulation Testing Configuration  
Figure 23

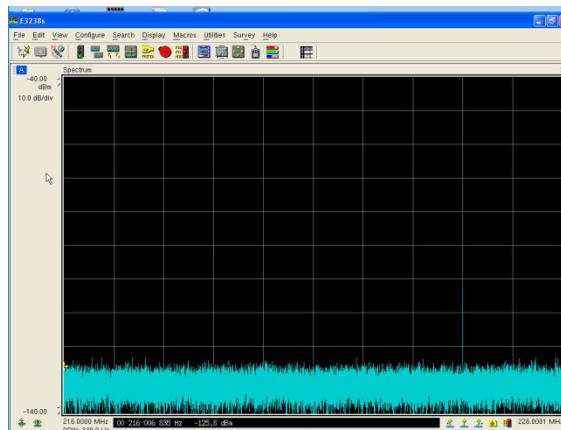
VHF RECEIVE



DPA Transmit Filtered

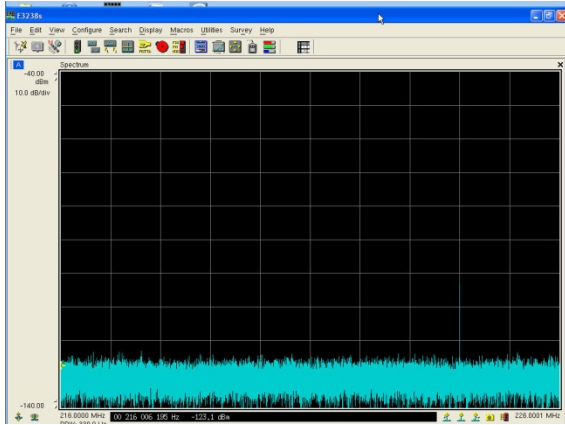


DBP Transmit Filtered

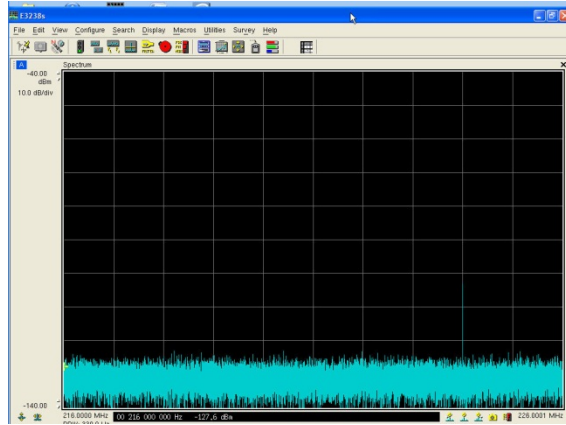


HOT Transmit Filtered

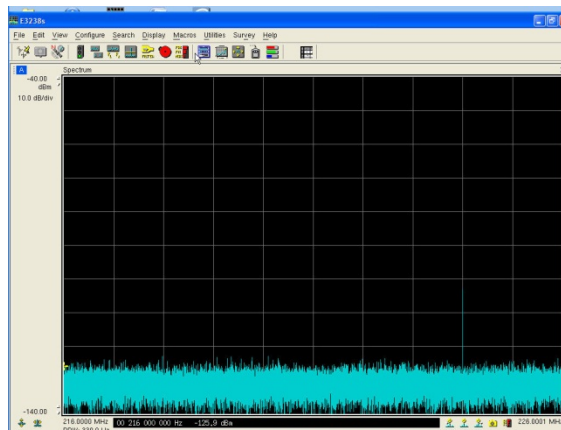
**HOT RECEIVE**



DPA Transmit Filtered

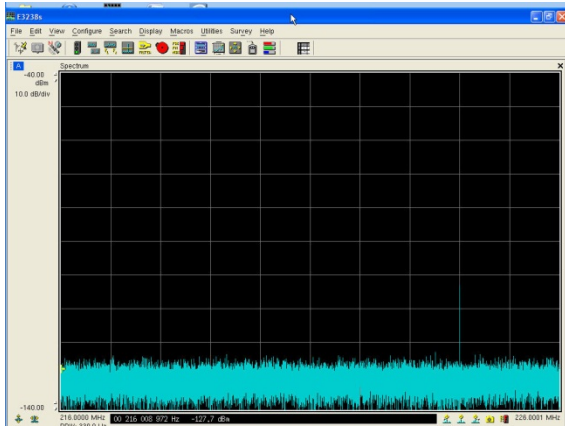


DBP Transmit Filtered

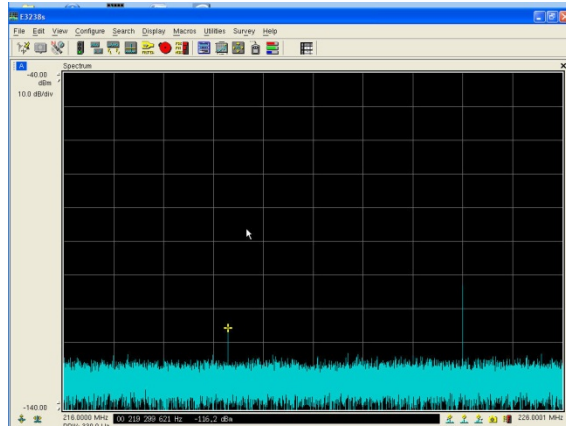


VHF Transmit Filtered

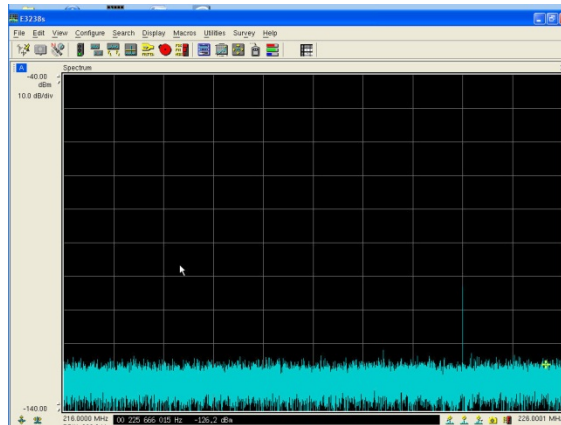
DPA RECEIVE



VHF Transmit Filtered

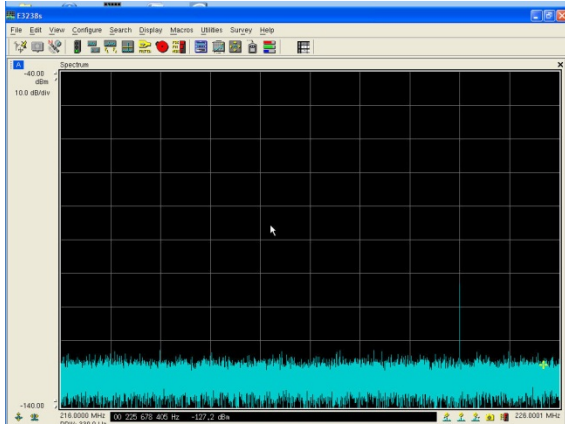


DBP Transmit Filtered

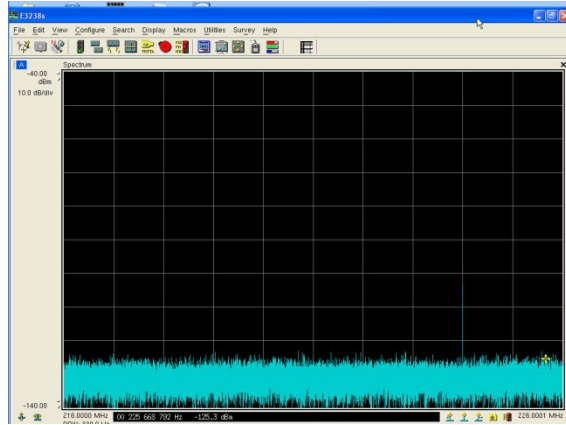


HOT Transmit Filtered

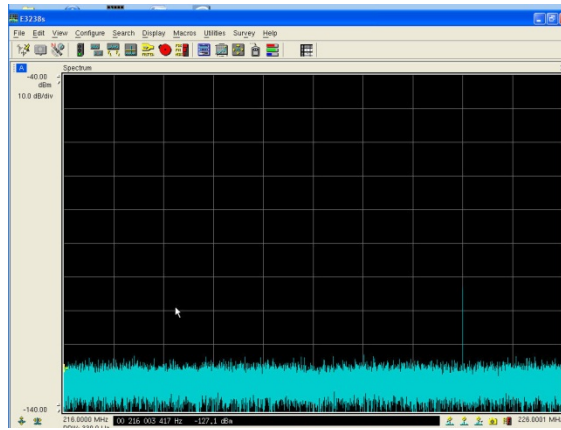
**DPB RECEIVE**



DPA Transmit Filtered

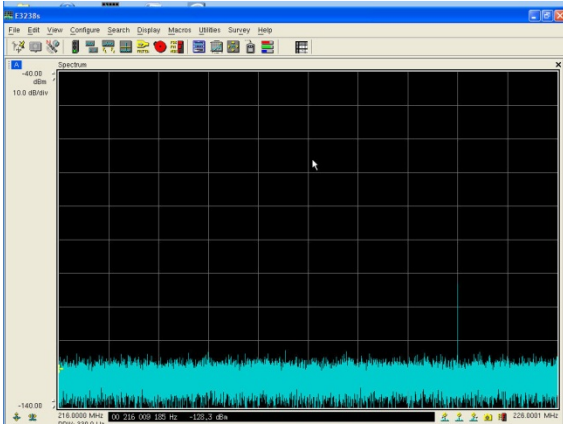


DBP Transmit Filtered

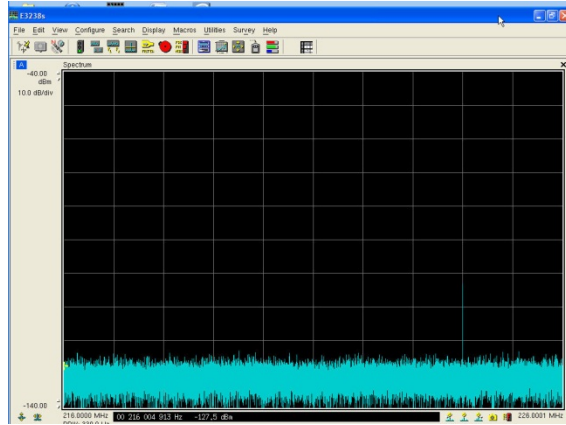


HOT Transmit Filtered

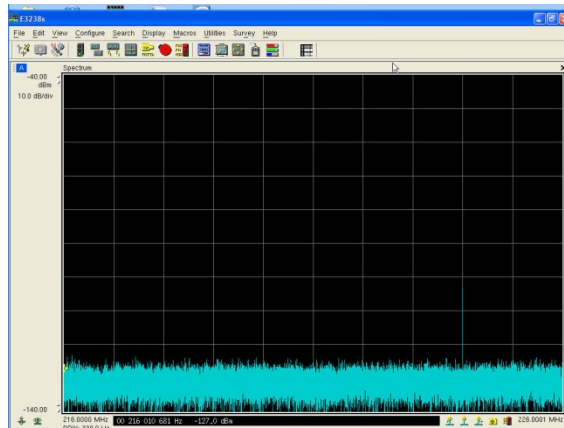
ER RECEIVE



DPA Transmit Filtered

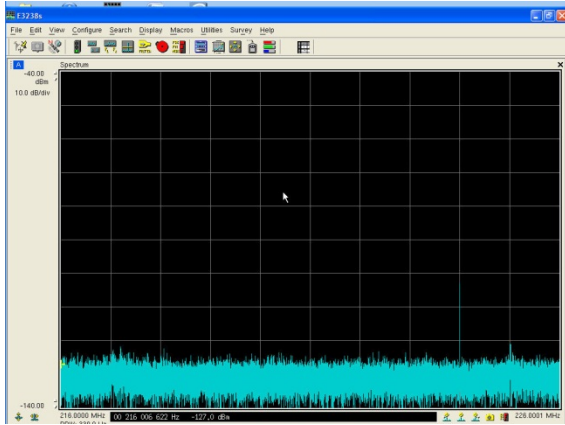


DBP Transmit Filtered

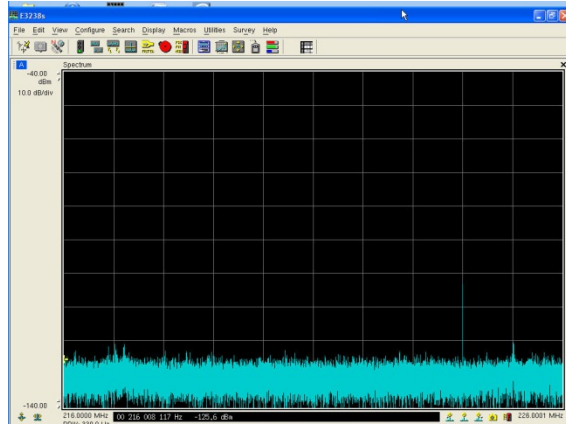


VHF Transmit Filtered

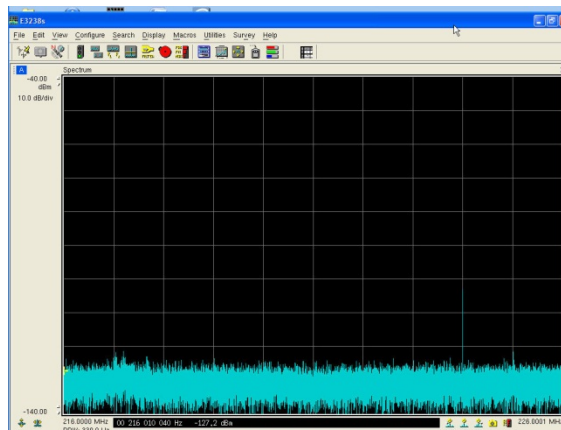
**SPEC 200 RECEIVE**



DPA Transmit Filtered



DBP Transmit Filtered



VHF Transmit Filtered



## Transmit Intermodulation Test

This test provides information on intermodulation products produced by multiple radio transmissions at the same time. Several radios on a locomotive, such as Voice 161 MHz, PTC 220 MHz, DP A UHF or DP B UHF, HOT UHF and SPEC 200 900 MHz, may transmit simultaneously. These simultaneous transmissions may occur on two, three or more radios at the same time.

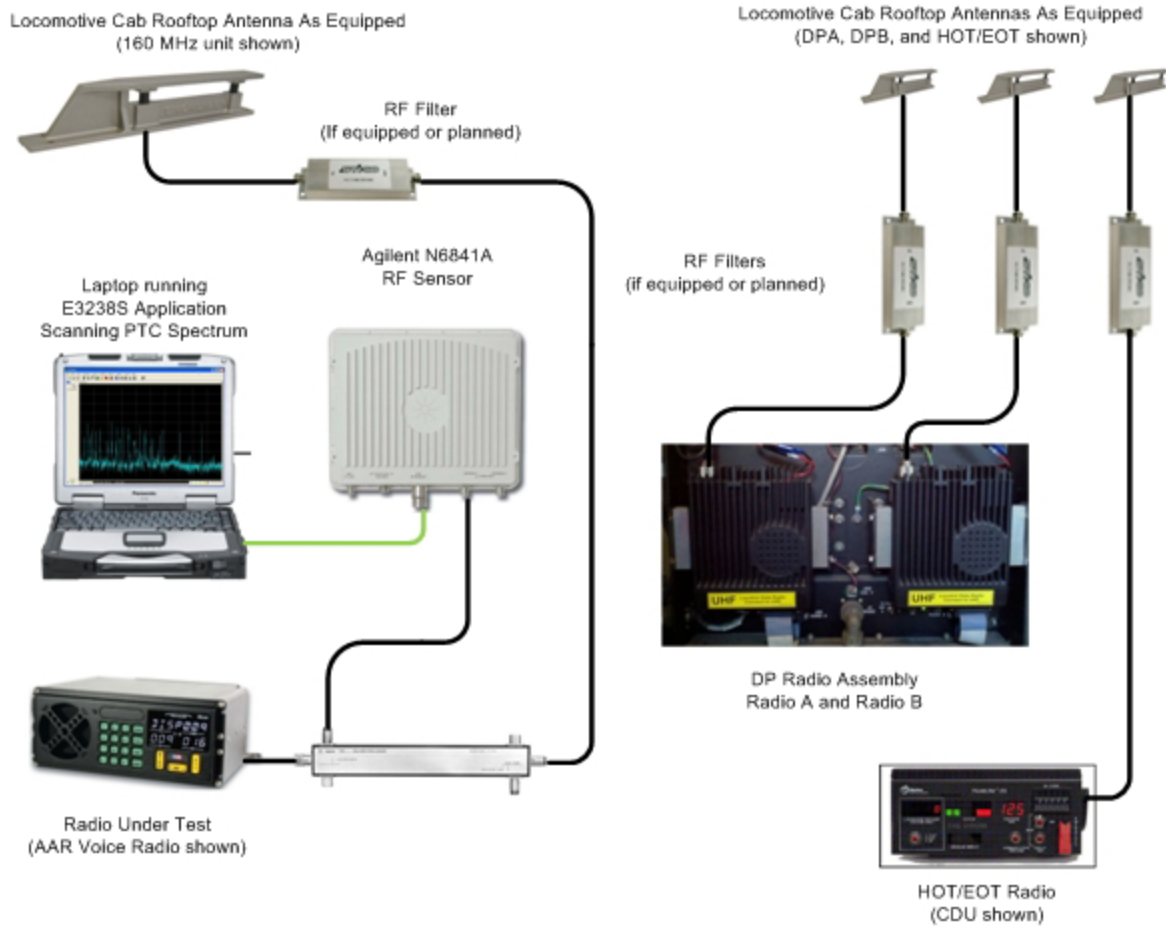
Two, three, four or more on-board radios combined in different groups transmit simultaneously. Each of the radios transmits at nominal power, and using a dual directional coupler each other non-transmitting radio is measured for the amount of signals received from the transmitting radios entering through the antenna, and for the amount of intermodulation products generated at the front end of the radio receiver and transmitted back through the same antenna.

A Dual Directional Coupler rated for a maximum power handling of 500 Watts is used to separately measure signals coming from the antenna to the radio receiver front end, and from the receiver front end travelling to the antenna and being transmitted as intermodulation products.

This Dual Directional Coupler has six ports, one for Antenna, one for Radio, two for 50 ohms loads, one to measure signals coming from the antenna to the radio transceiver, and one port to measure signals from the radio transceiver to the antenna.

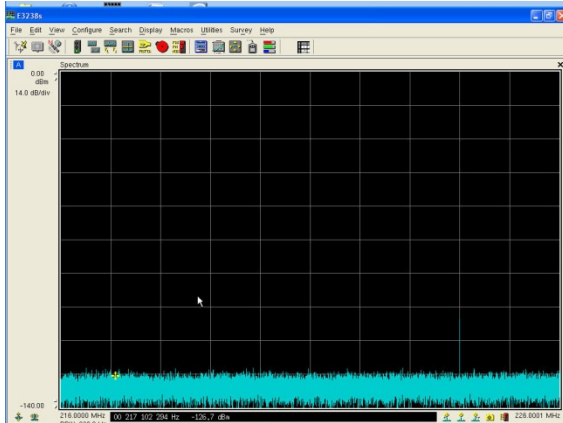
In the IMD Test Apparatus diagram, the initial radio under test shown is the AAR Voice Radio, operating at ~ 160 MHz. Its Transmitter is coupled directly to its existing transmission path, including Antenna (and Filter, if equipped or planned). The RF Sensor is coupled 20 dB down (or more, as needed to protect the RF Sensor) to the Transmitter in the Radio under Test. The other radios of interest on the Locomotive (DPA, DPB, and HOT/EOT) are then keyed and RF energy from those radios pass through their respective existing transmission paths, including Antennas (and Filters, if equipped or planned). The RF energy then propagates into the Antenna of the Radio under Test, and then into the Transmitter under test. Any IMD products in the 220 MHz spectrum generated in the Transmitter that would be propagated via the Antenna system are measured by the RF Sensor.

A permutation of the IMD Test Apparatus is configured for each of the other radios of interest (DPA, DPB, and HOT/EOT), so that each of them is connected as a Radio under Test, and the process is repeated.

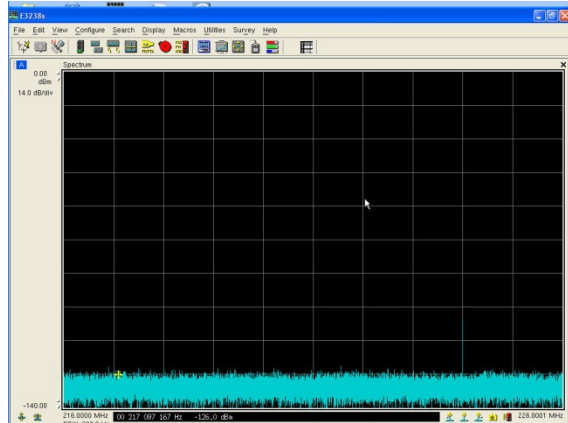


Transmit Intermodulation Testing Configuration  
Figure 24

**SENSOR IN-LINE WITH VHF ANTENNA**

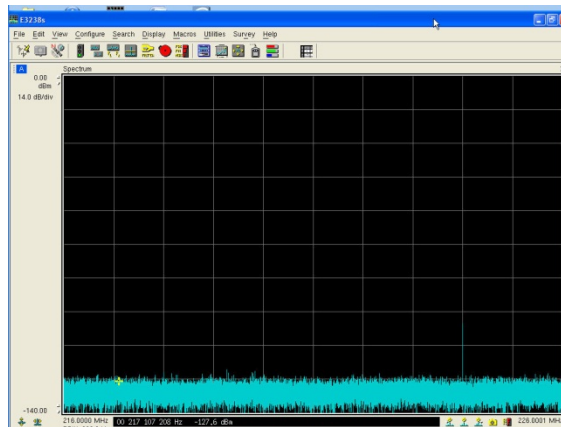


VHF Transmit  
DPA Transmit  
HOT Transmit



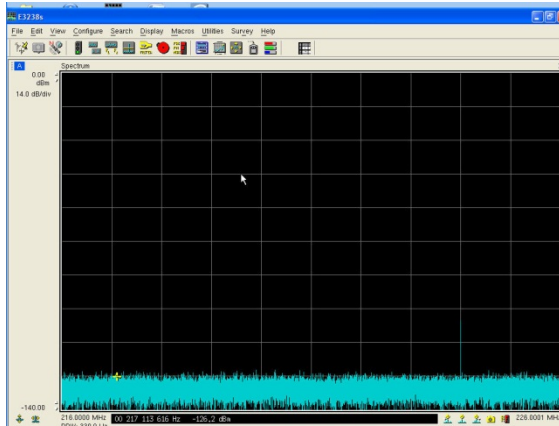
VHF Transmit  
DPB Transmit  
HOT Transmit

**SENSOR IN-LINE WITH DPA ANTENNA**



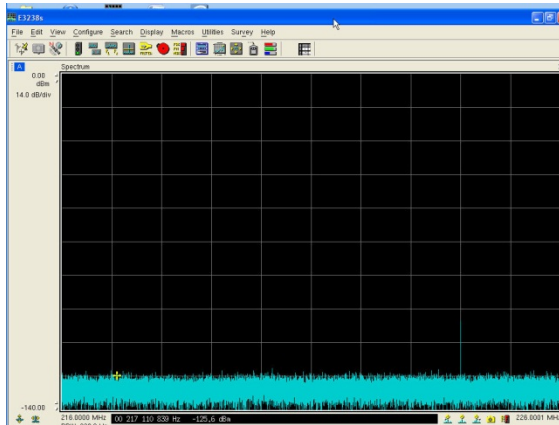
DPA Transmit  
VHF Transmit  
HOT Transmit

**SENSOR IN-LINE WITH DPB ANTENNA**



DPB Transmit  
VHF Transmit  
HOT Transmit

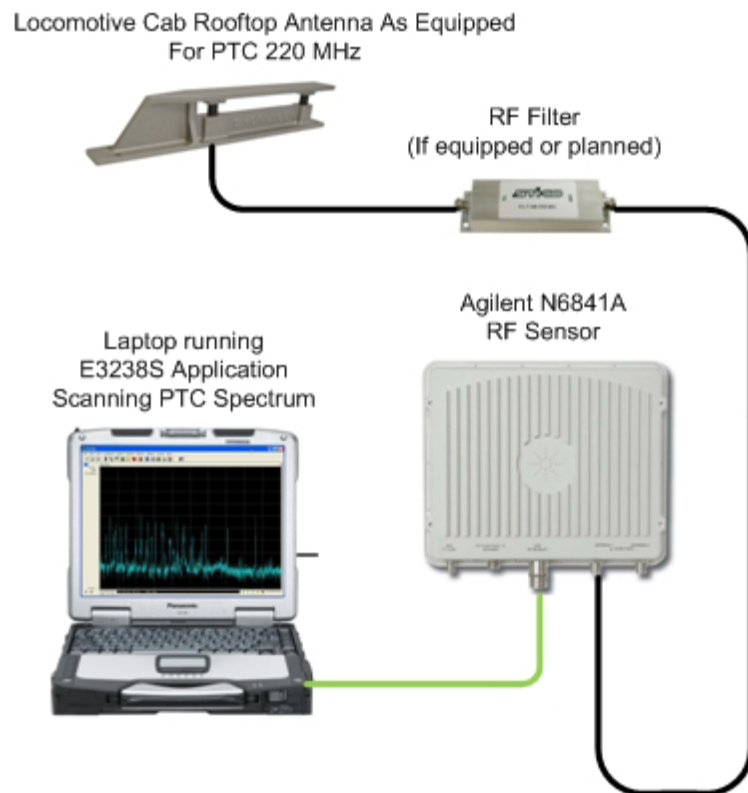
**SENSOR IN-LINE WITH HOT ANTENNA**



HOT Transmit  
VHF Transmit  
HOT Transmit

## EMI Testing

The testing results showed some increases in the noise floor level while operating through the start-up and shut-down phases. There were not significant variations while changing through the various power conditions. A very minor difference between the conductor and engineer side noise floor (only about 1-2 DB) was indicated during testing. This may be attributed to the physical location of the antenna feed point relative to some on-board power sources, the pattern characteristic differences between the two antennas, or the routing of the two different cable bundles.



EMI Testing Configuration  
Figure 25

UP 5802 (AC44CWCTE-GE) Locomotive Noise Test Battery Report

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O
	Frequency	Bandwidth	Number Sweeps	Intercepts	Detections	Minimum Amplitude (DBm)	Average Amplitude (DBm)	Maximum Amplitude (DBm)	Minimum Bandwidth	Average Bandwidth	Maximum Bandwidth	Minimum Duration	Average Duration	Maximum Duration	Percent Occupancy
1	216000214	214	1314	85	10.00	-131.57	-125.99	-120.80	213.62	213.62	213.62	0.05	0.01	0.06	6.5%
2	216000427	214	1341	254	29.00	-131.92	-126.97	-120.89	213.62	213.62	213.62	0.05	0.01	0.27	18.9%
3	216000641	214	1334	330	60.00	-131.98	-126.83	-121.90	213.62	213.62	213.62	0.05	0.01	0.30	24.7%
4	216000855	214	1339	288	48.00	-131.80	-127.21	-121.00	213.62	213.62	213.62	0.05	0.01	0.20	21.5%
5	216001068	214	1341	190	23.00	-131.98	-126.77	-121.79	213.62	213.62	213.62	0.05	0.01	0.23	14.2%
6	216001282	214	1342	545	131.00	-131.94	-124.90	-119.33	213.62	214.01	427.25	0.05	0.02	0.38	40.6%
7	216001495	214	1340	420	92.00	-131.87	-125.24	-119.77	213.62	214.13	427.25	0.05	0.02	0.20	31.3%
8	216001709	214	1334	174	16.00	-131.86	-126.68	-120.89	213.62	214.85	427.25	0.05	0.00	0.11	13.0%
9	216001923	214	1342	361	71.00	-131.98	-126.29	-120.77	213.62	213.62	213.62	0.05	0.02	1.45	26.9%
10	216002136	214	1336	406	82.00	-131.95	-125.97	-119.31	213.62	213.62	213.62	0.05	0.01	0.25	30.4%
11	216002350	214	1342	252	39.00	-131.94	-126.71	-121.37	213.62	213.62	213.62	0.05	0.01	0.11	18.8%
12	216002564	214	1329	262	41.00	-131.98	-127.02	-122.01	213.62	213.62	213.62	0.05	0.01	0.16	19.7%
13	216002777	214	1341	329	59.00	-131.98	-125.90	-119.16	213.62	214.27	427.25	0.05	0.01	0.16	24.5%
14	216002991	214	1338	463	102.00	-131.92	-125.54	-119.63	213.62	213.62	213.62	0.05	0.02	0.27	34.6%
15	216003204	214	1340	307	59.00	-131.84	-125.81	-120.77	213.62	213.62	213.62	0.05	0.01	0.16	22.9%
16	216003418	214	1342	305	48.00	-131.71	-126.40	-119.80	213.62	214.32	427.25	0.05	0.01	0.16	22.7%
17	216003632	214	1341	301	53.00	-131.80	-126.54	-120.70	213.62	213.62	213.62	0.05	0.01	0.20	22.4%
18	216003845	214	1337	289	56.00	-131.98	-127.10	-120.43	213.62	214.36	427.25	0.05	0.01	0.22	21.6%
19	216004059	214	1336	308	58.00	-131.97	-127.08	-122.06	213.62	213.62	213.62	0.05	0.01	0.27	23.1%
20	216004273	214	1338	298	53.00	-131.98	-126.85	-120.96	213.62	214.34	427.25	0.05	0.01	0.20	22.3%
21	216004486	214	1339	332	65.00	-131.80	-127.04	-121.12	213.62	213.62	213.62	0.05	0.01	0.33	24.8%
22	216004700	214	1341	381	75.00	-131.98	-126.40	-121.15	213.62	213.62	213.62	0.05	0.02	0.23	28.4%
23	216004913	214	1335	277	44.00	-131.97	-127.08	-120.32	213.62	213.62	213.62	0.05	0.01	0.11	20.7%
24	216005127	214	1337	296	49.00	-131.98	-127.02	-121.40	213.62	213.62	213.62	0.05	0.01	0.22	22.1%
25	216005341	214	1341	327	65.00	-131.97	-127.02	-119.80	213.62	213.62	213.62	0.05	0.01	0.16	24.4%
26	216005554	214	1342	293	52.00	-131.98	-126.89	-121.16	213.62	213.62	213.62	0.05	0.01	0.20	21.8%
27	216005768	214	1335	311	56.00	-131.87	-127.15	-121.00	213.62	214.31	427.25	0.05	0.01	0.11	23.3%
28	216005981	214	1338	293	54.00	-131.98	-126.86	-120.96	213.62	214.35	427.25	0.05	0.01	0.13	21.9%
29	216006195	214	1342	312	59.00	-131.97	-126.99	-120.94	213.62	213.62	213.62	0.05	0.02	1.45	23.2%
30	216006409	214	1338	302	55.00	-131.98	-127.35	-122.10	213.62	214.33	427.25	0.05	0.01	0.16	22.6%
31	216006622	214	1342	322	60.00	-131.98	-127.00	-121.25	213.62	214.29	427.25	0.05	0.01	0.25	24.0%
32	216006836	214	1339	296	49.00	-131.92	-127.08	-122.56	213.62	213.62	213.62	0.05	0.01	0.25	22.1%
33	216007050	214	1341	325	63.00	-131.97	-127.04	-121.10	213.62	214.94	427.25	0.05	0.01	0.23	24.2%
34	216007263	214	1336	313	64.00	-131.98	-127.22	-121.77	213.62	213.62	213.62	0.05	0.01	0.31	23.4%

Energy File Data Format  
Engine Off State  
Figure 26

This is a sample of the data captured on each locomotive, each excel file is approximately 10 MB, comprised 46000 frequency information points and the associated amplitude, duration, bandwidth and percent occupancy information.

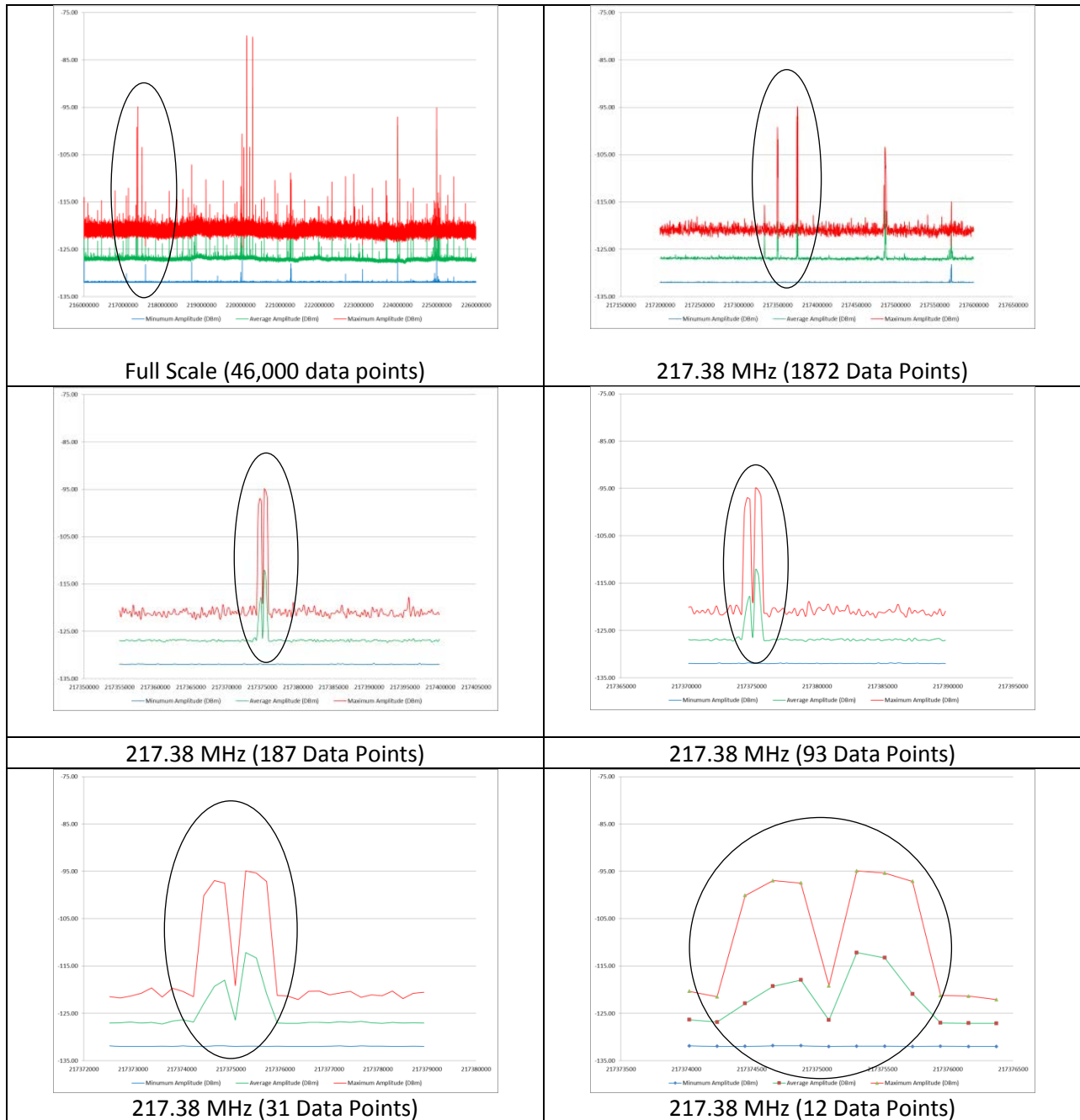
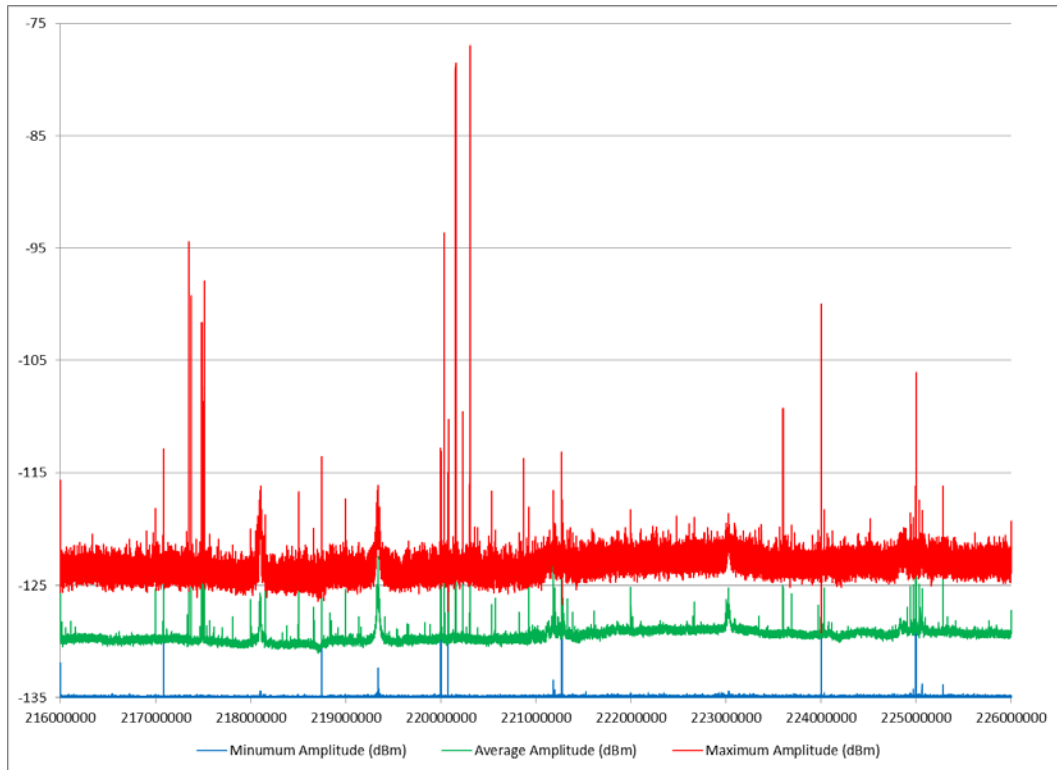
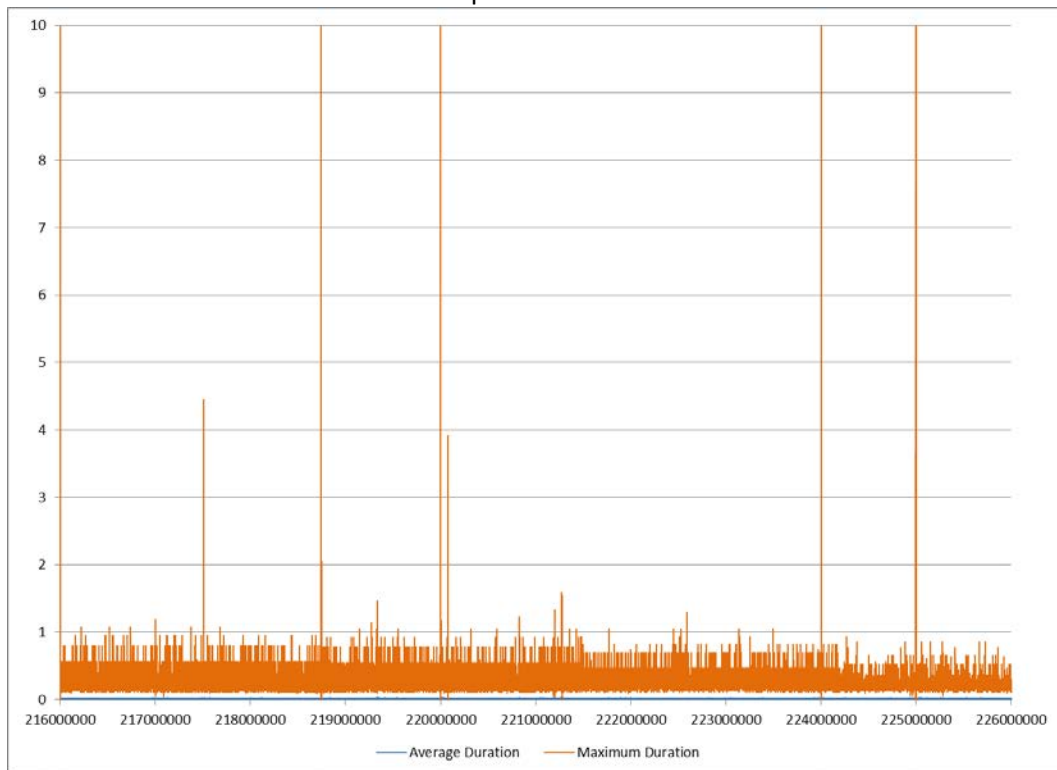


Figure 27

The following charts represent XY scatter chart with lines in EXCEL. Because of the amount of information shown in each chart the data might appear to be a spectrograph exported from a spectrum analyzer, rather than a record of the signal amplitude levels or duration information extracted and plotted from the energy history files that it actually represents. In Figure 27, three different resolutions of the information have been created to show the individual data points and how they are interconnected.



Amplitude Profile

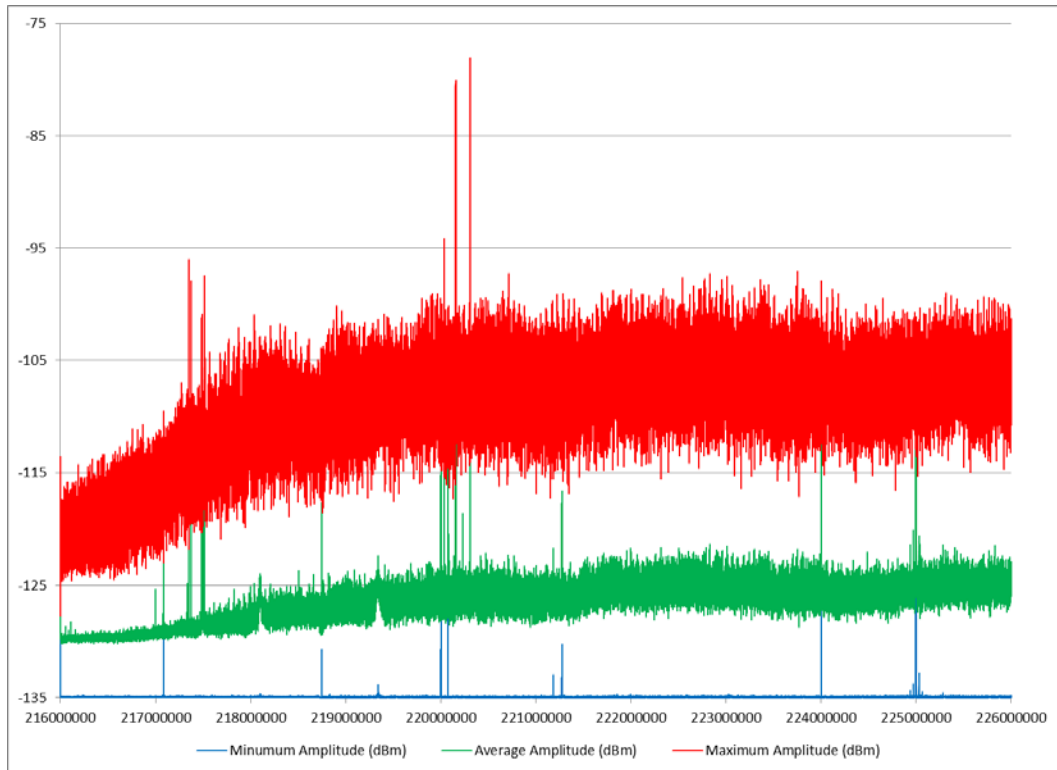


Duration Profile

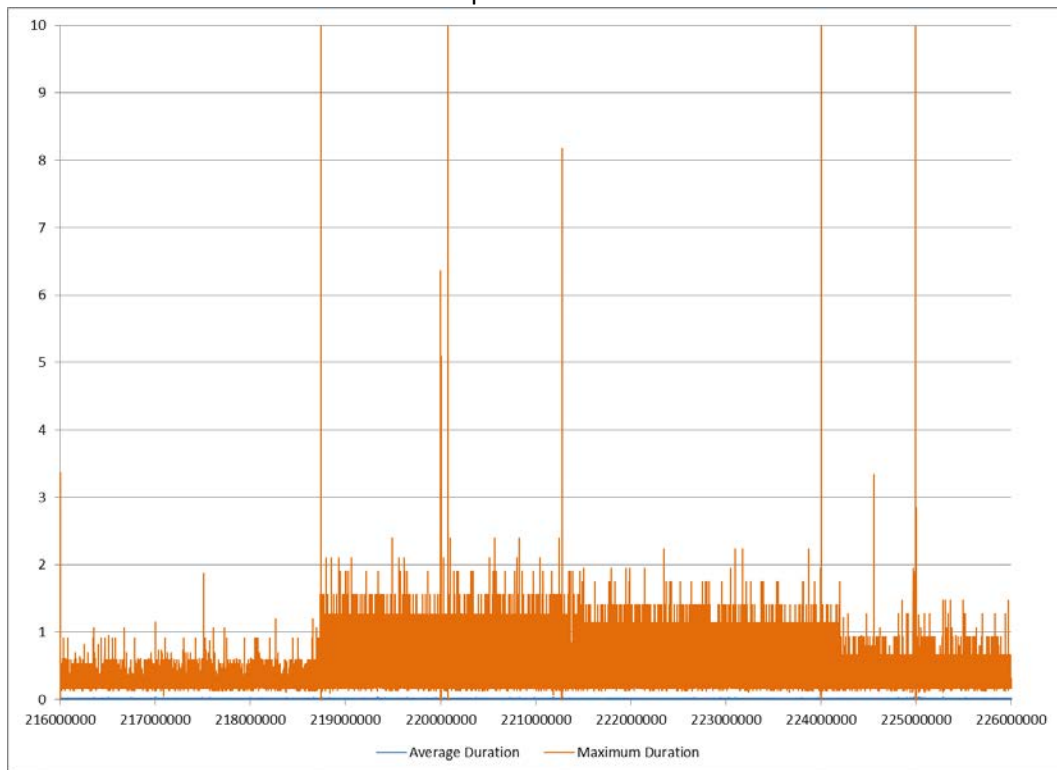
UP 5802 Engine Off State

Figure 28



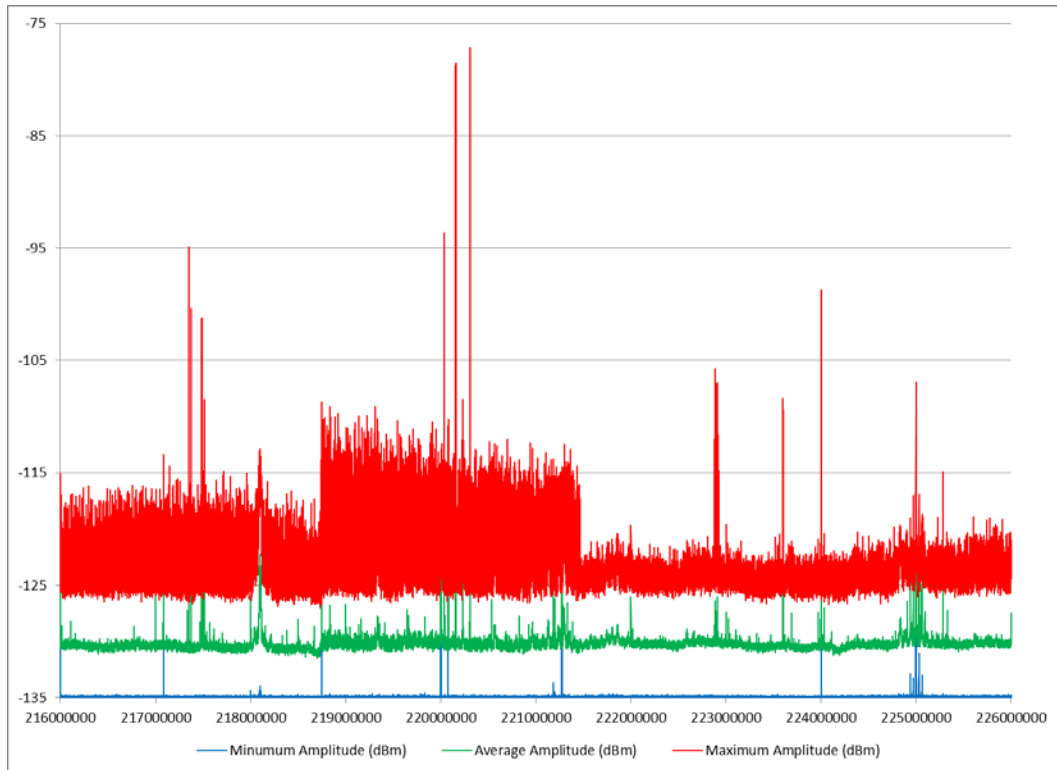


Amplitude Profile

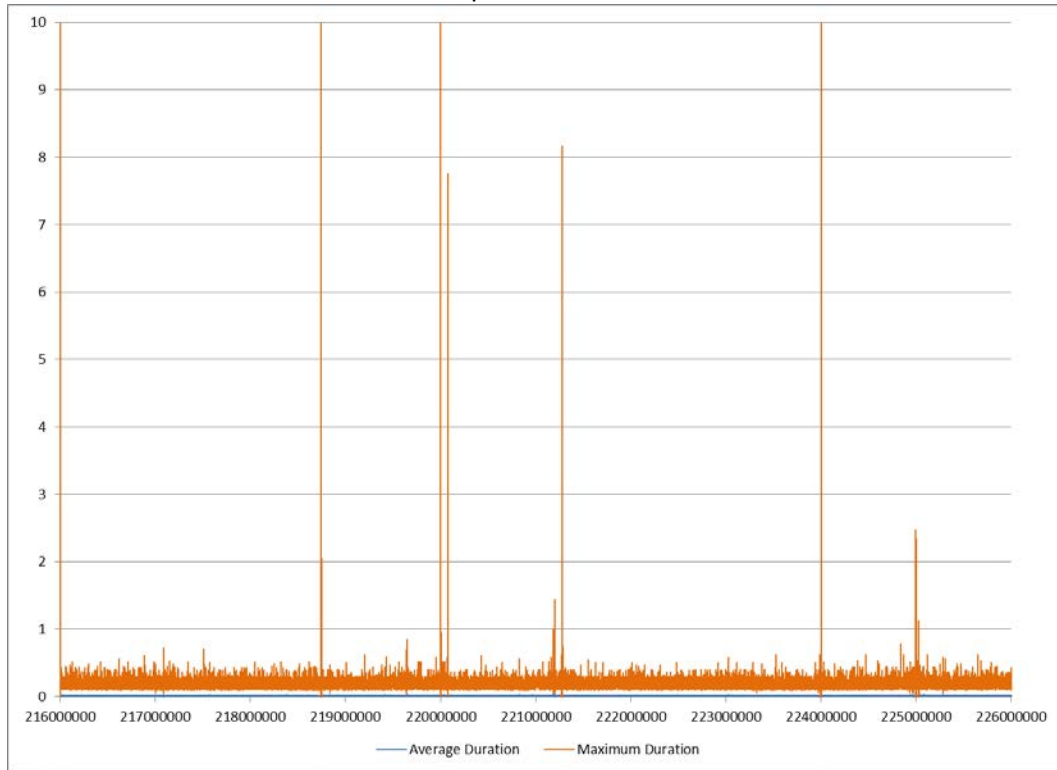


Duration Profile

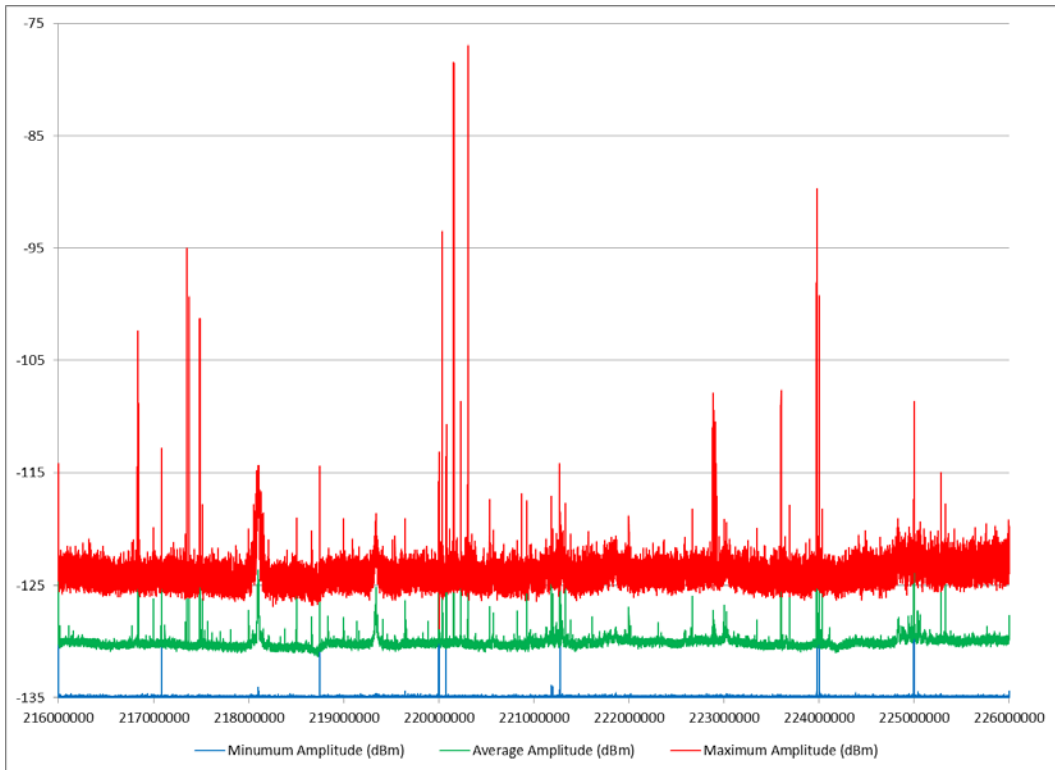
UP 5802 Startup Sequence  
Figure 29



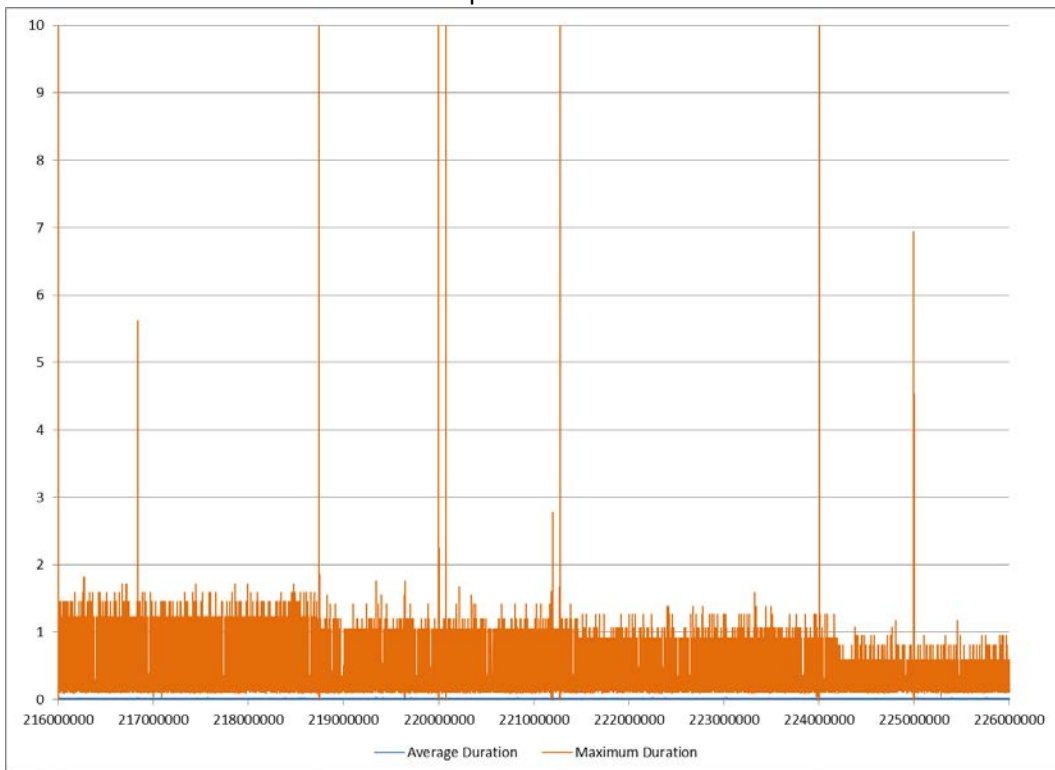
Amplitude Profile



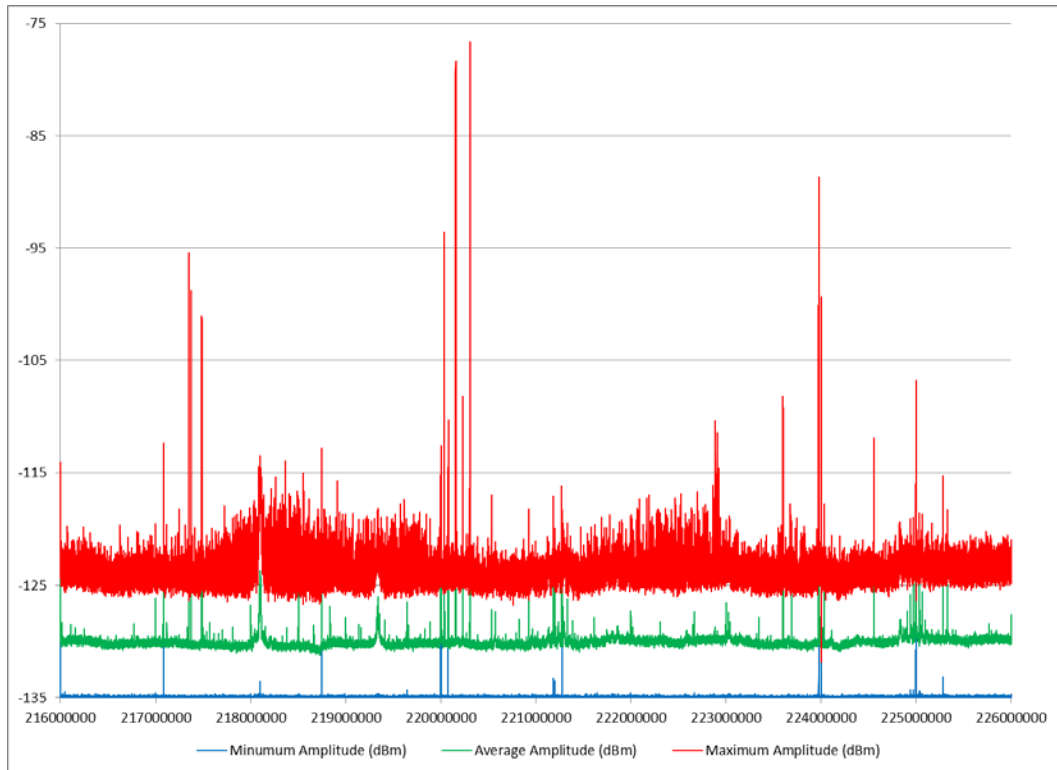
Duration Profile  
UP 5802 Engine Idle  
Figure 30



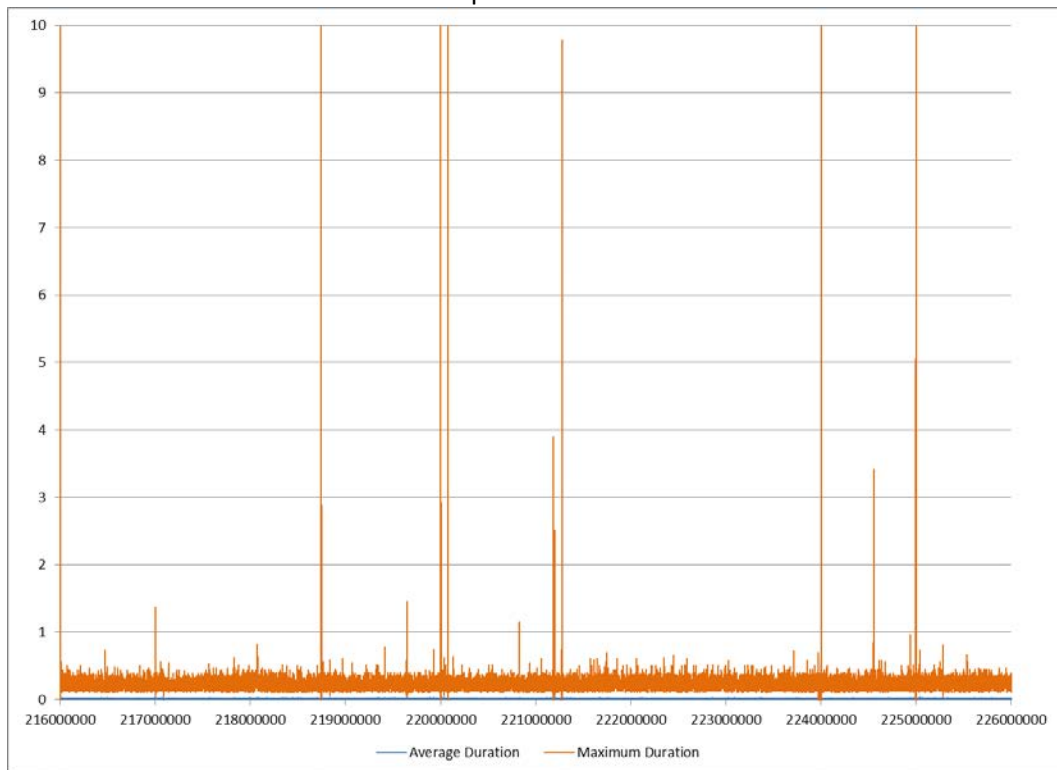
Amplitude Profile



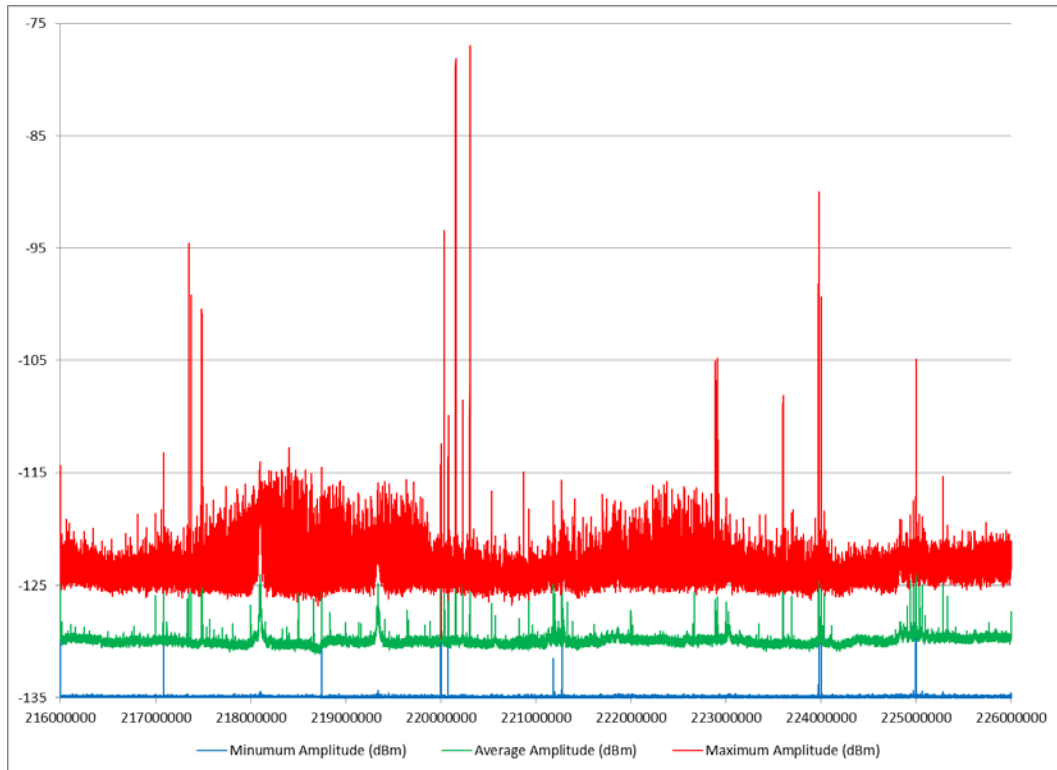
Duration Profile  
UP 5802 Notch 1  
Figure 31



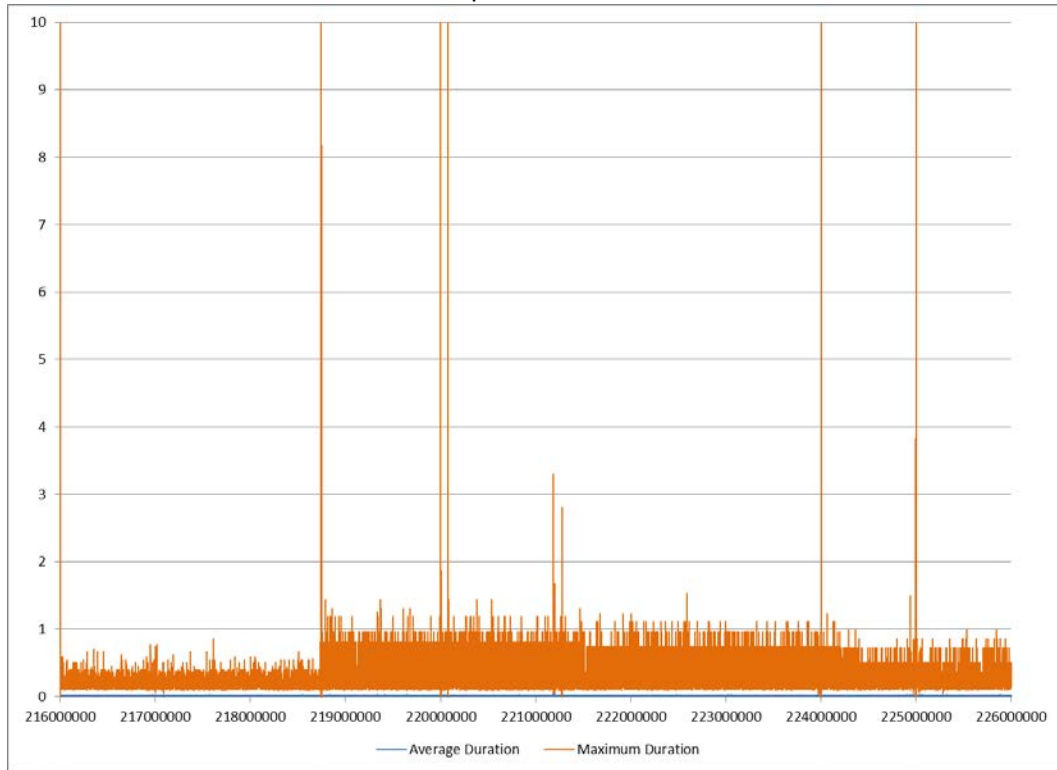
Amplitude Profile



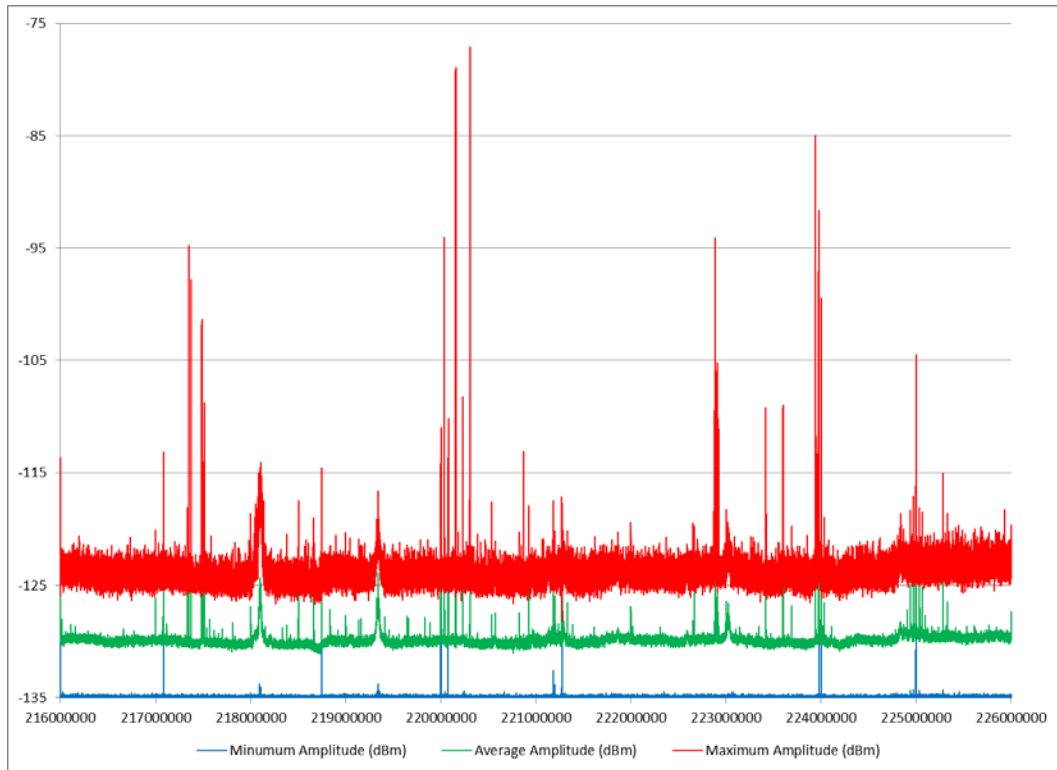
Duration Profile  
UP 5802 Notch 2  
Figure 32



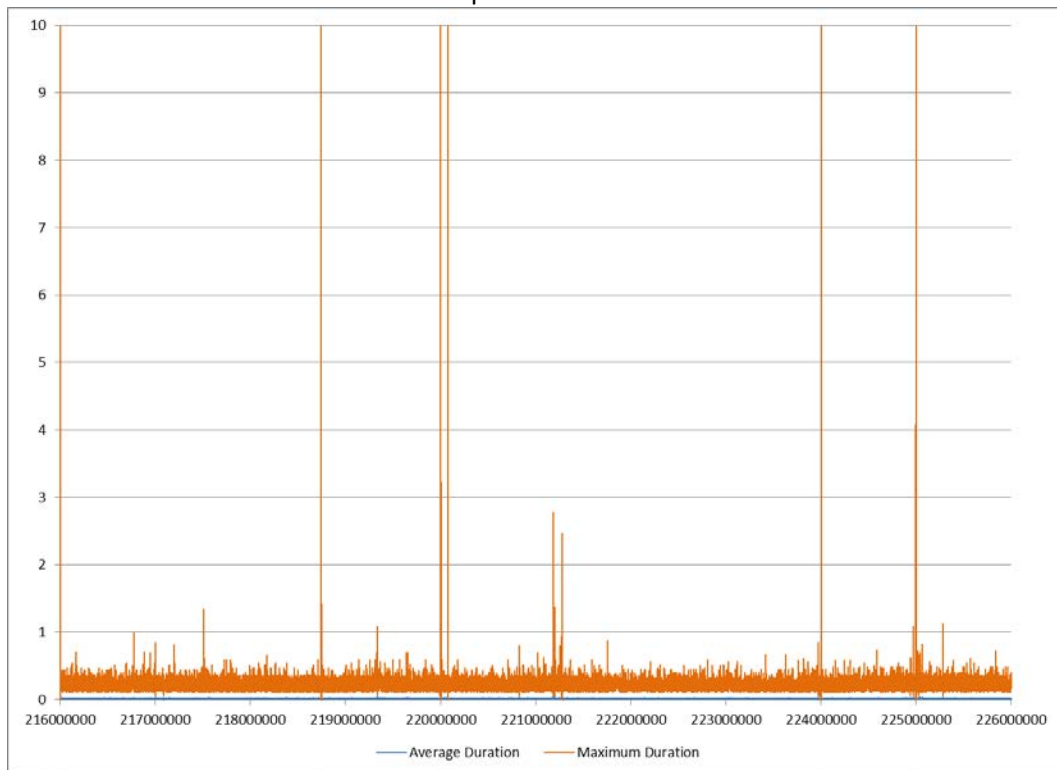
Amplitude Profile



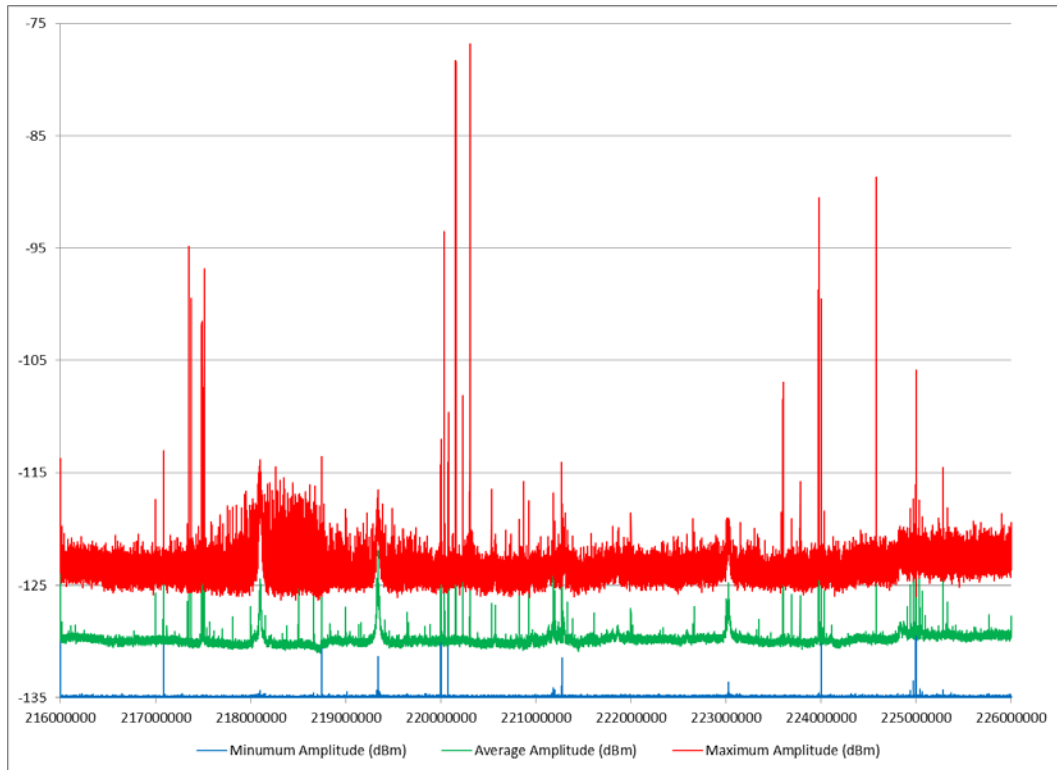
Duration Profile  
UP 5802 Notch 3  
Figure 33



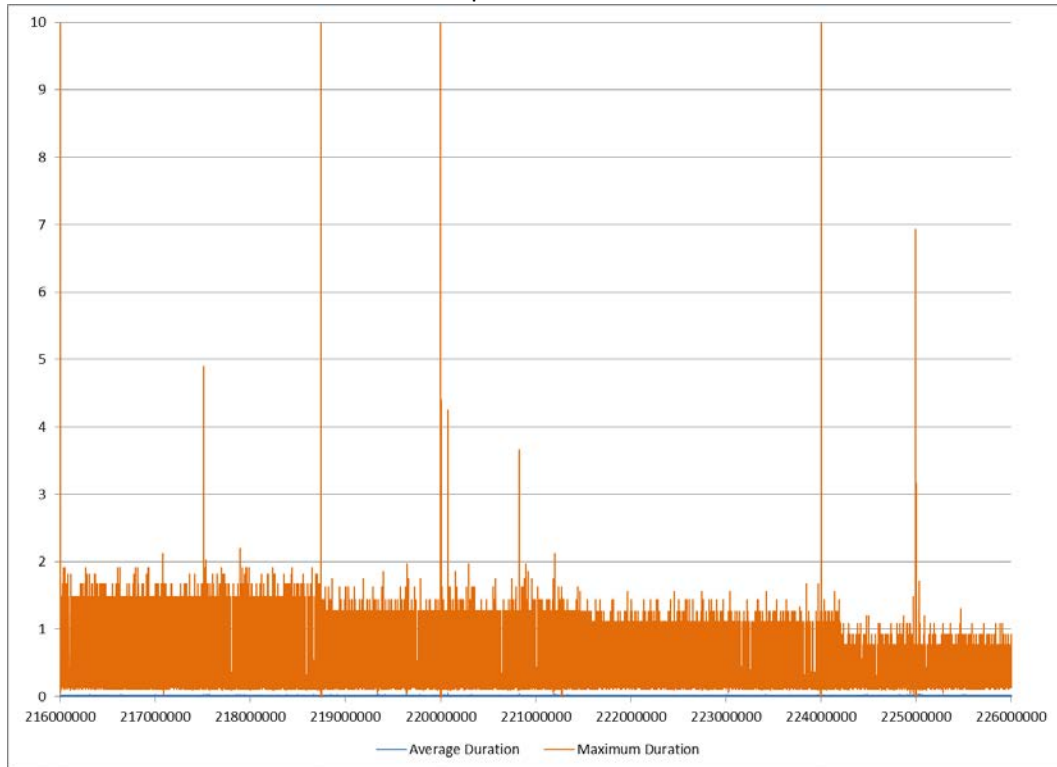
Amplitude Profile



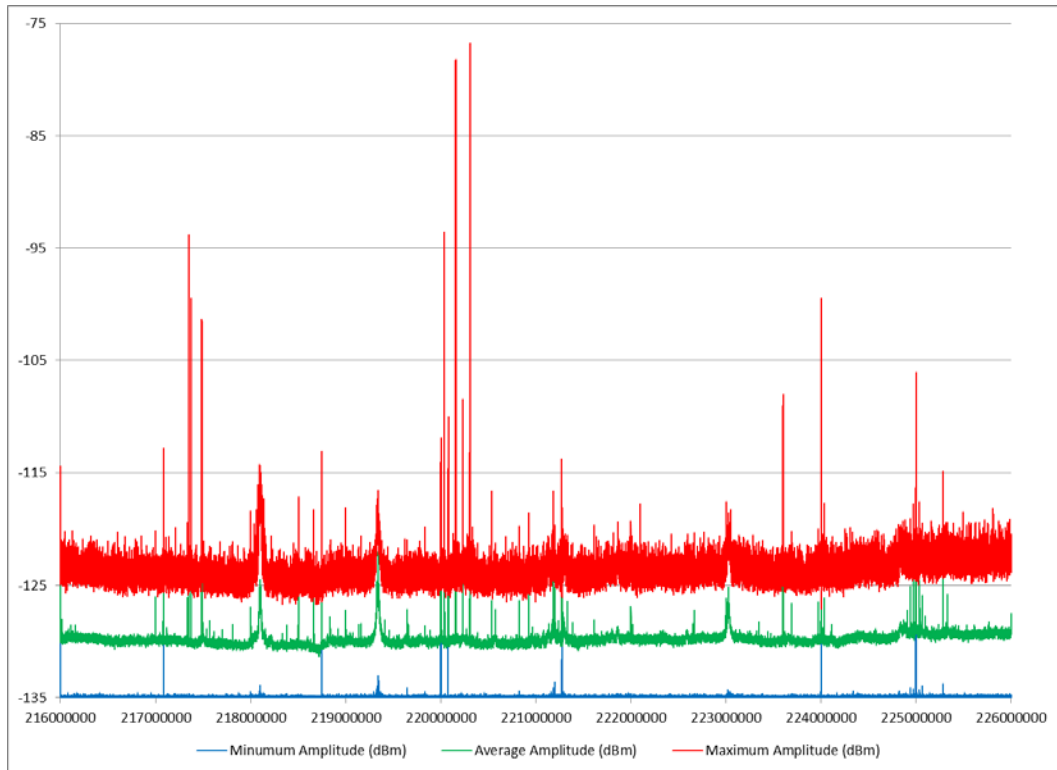
Duration Profile  
UP 5802 Notch 4  
Figure 34



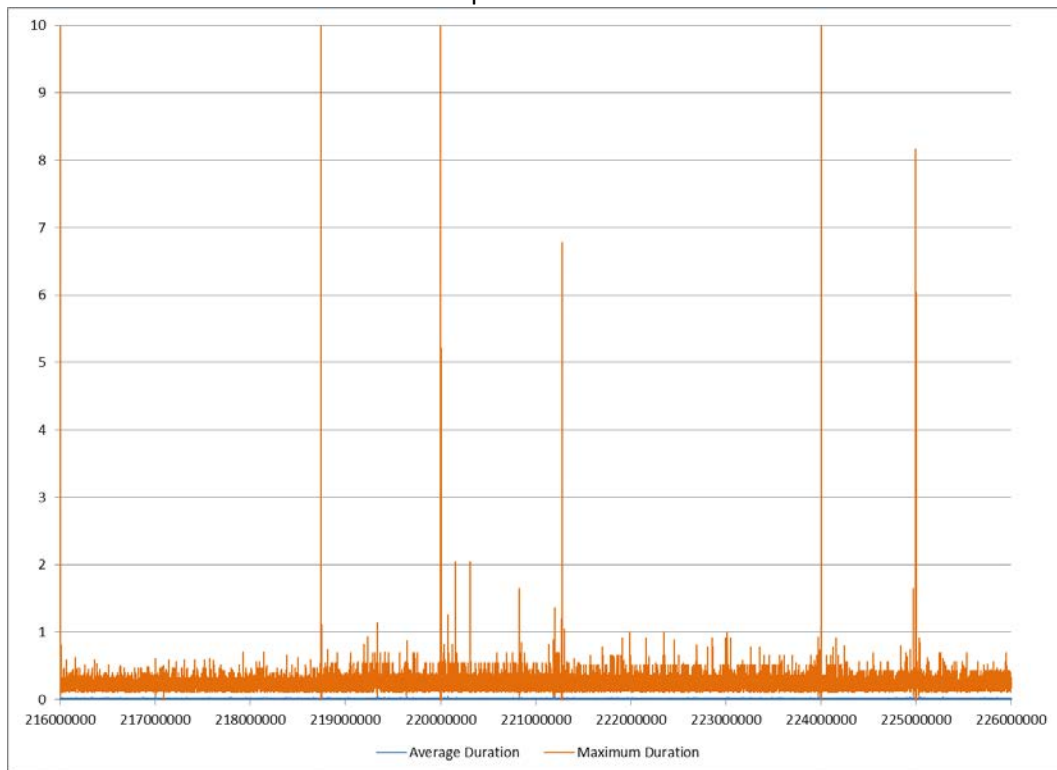
Amplitude Profile



Duration Profile  
UP 5802 Notch 5  
Figure 35

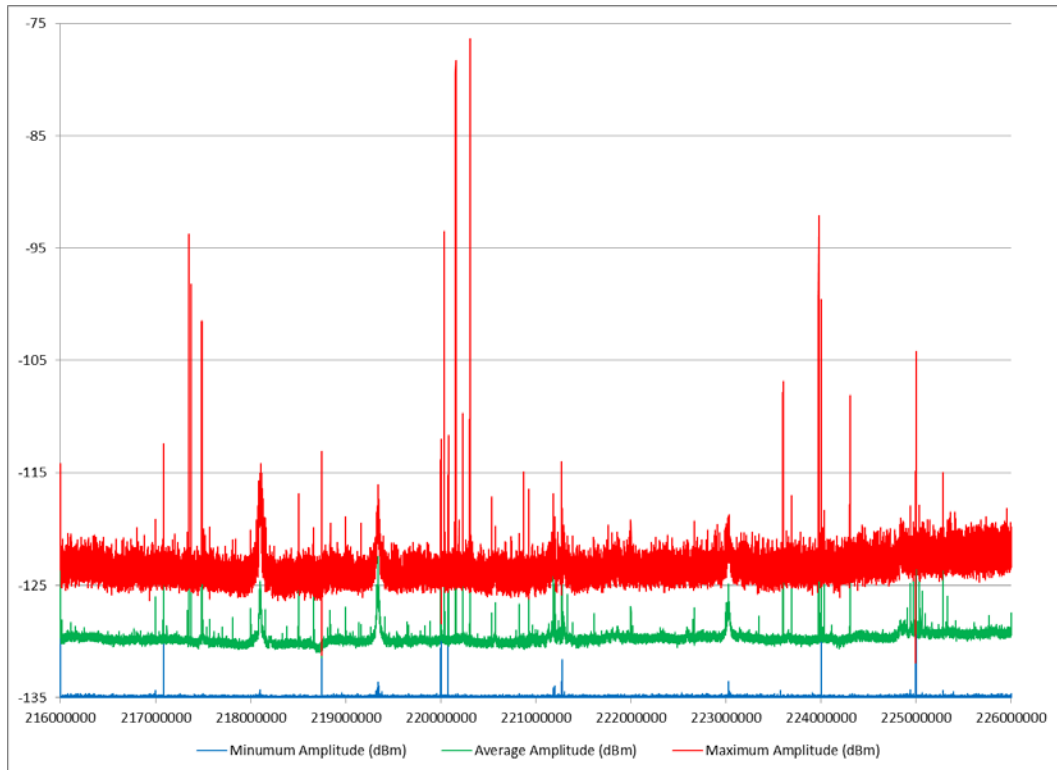


Amplitude Profile

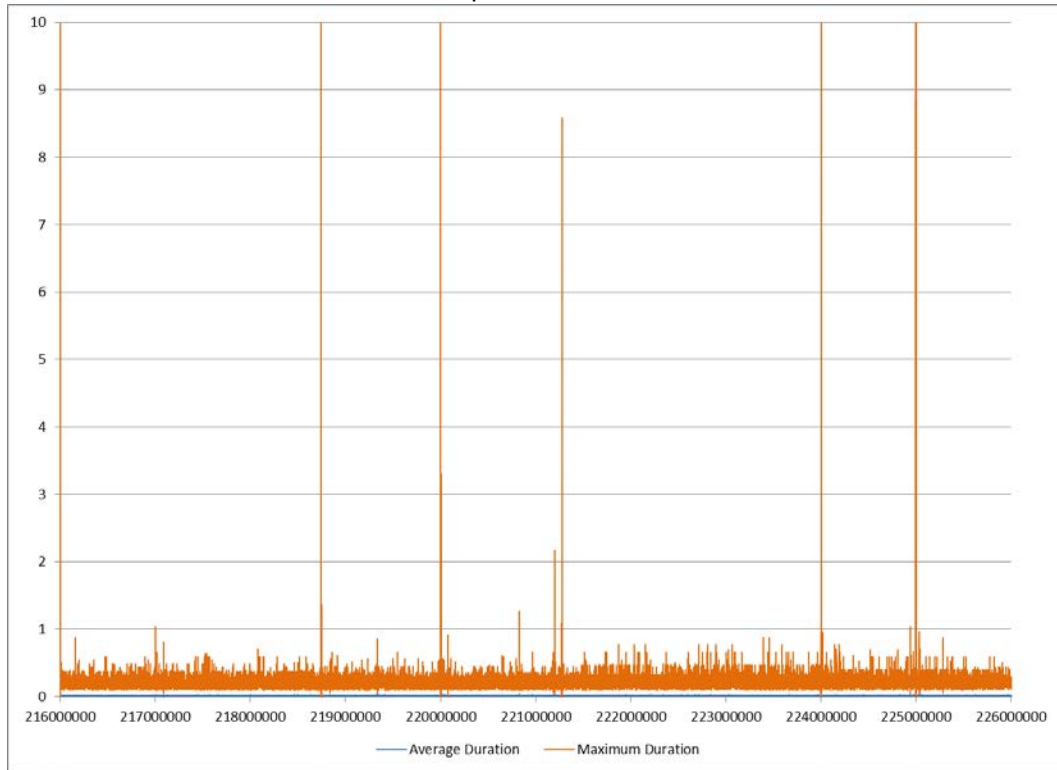


Duration Profile  
UP 5802 Notch 6  
Figure 36





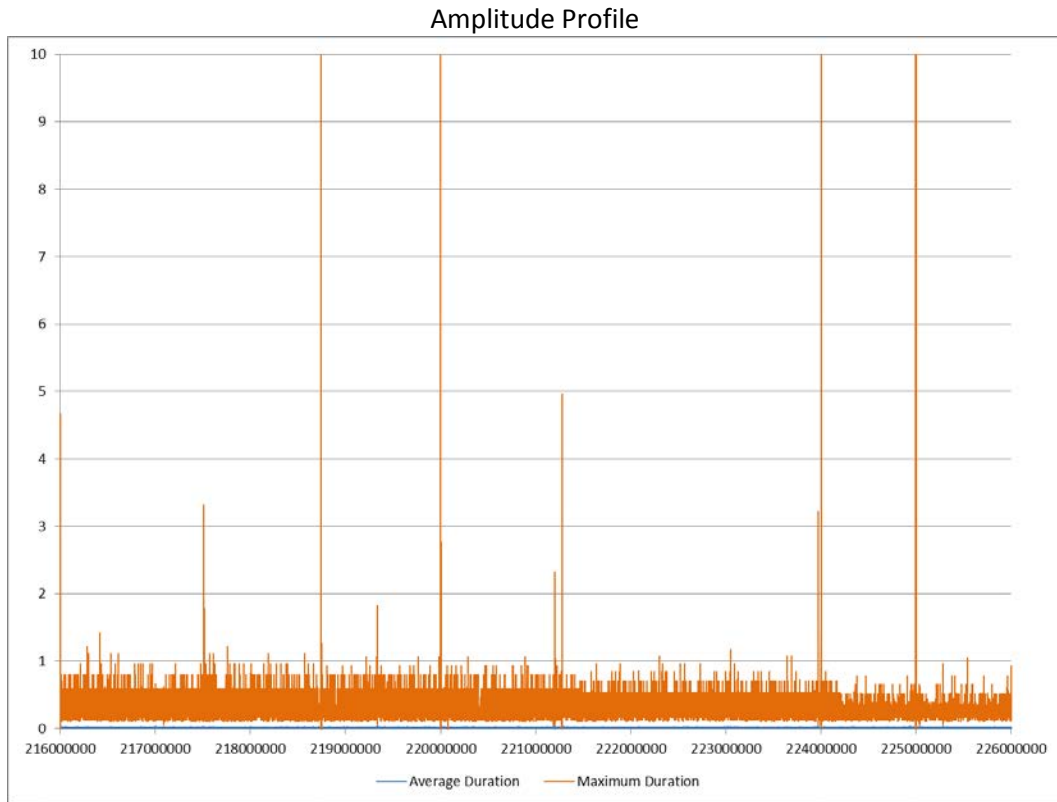
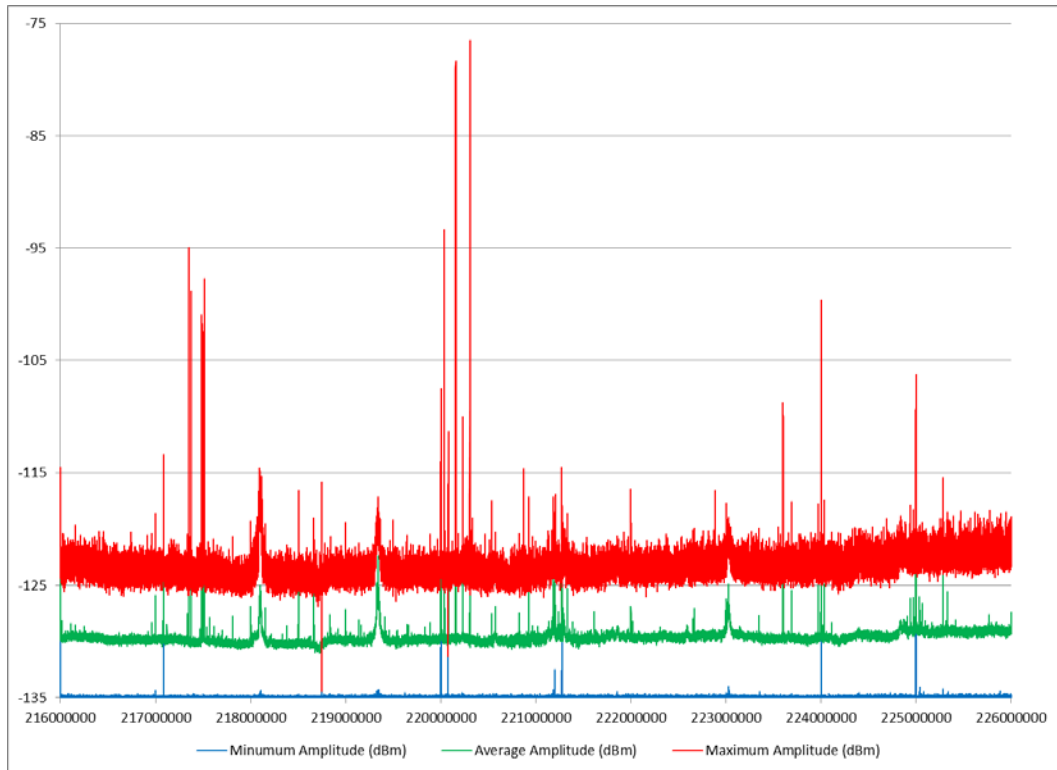
Amplitude Profile



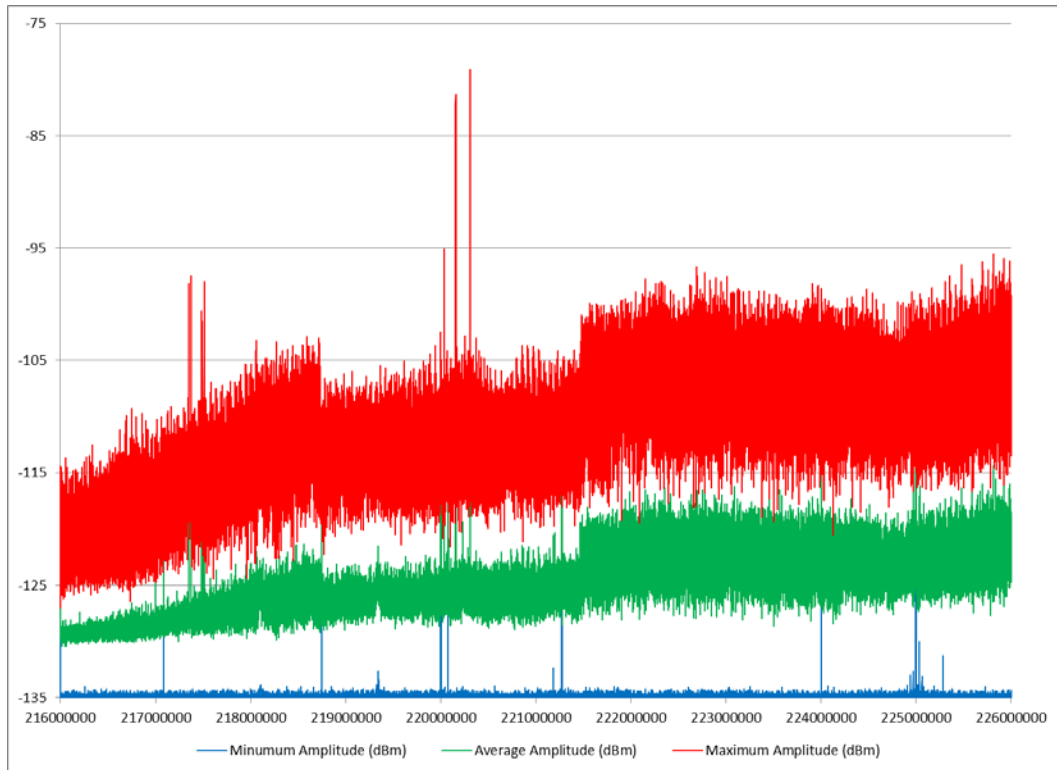
Duration Profile

UP 5802 Notch 7

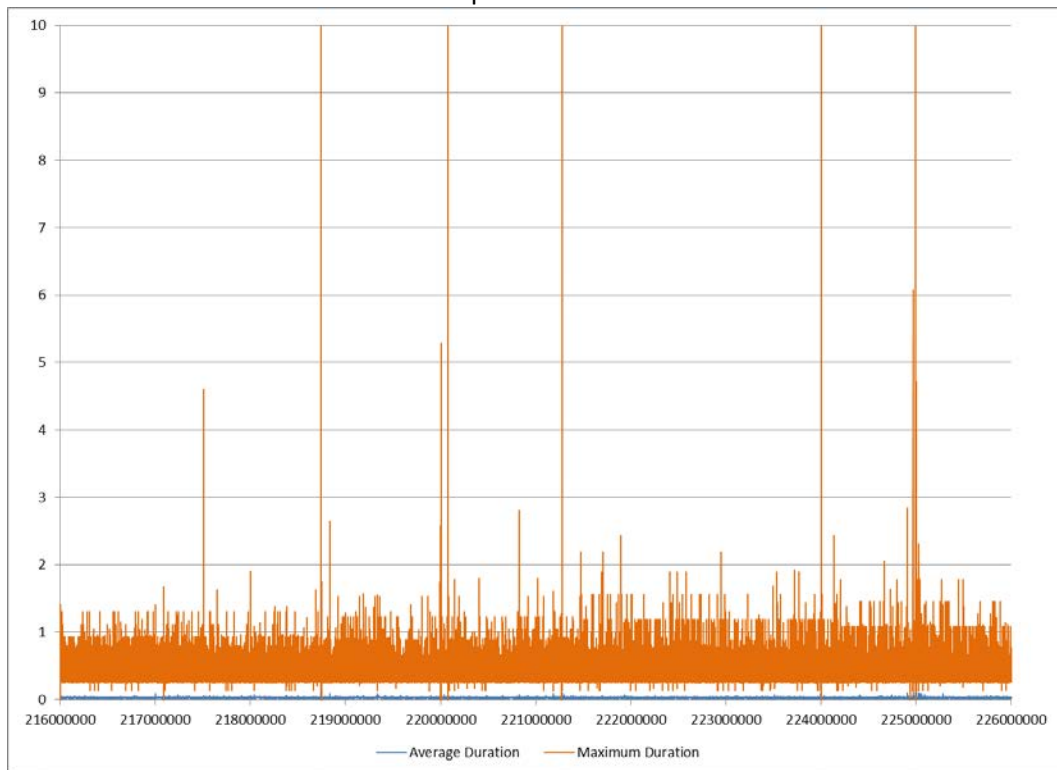
Figure 37



UP 5802 Notch 8  
Figure 38



Amplitude Profile



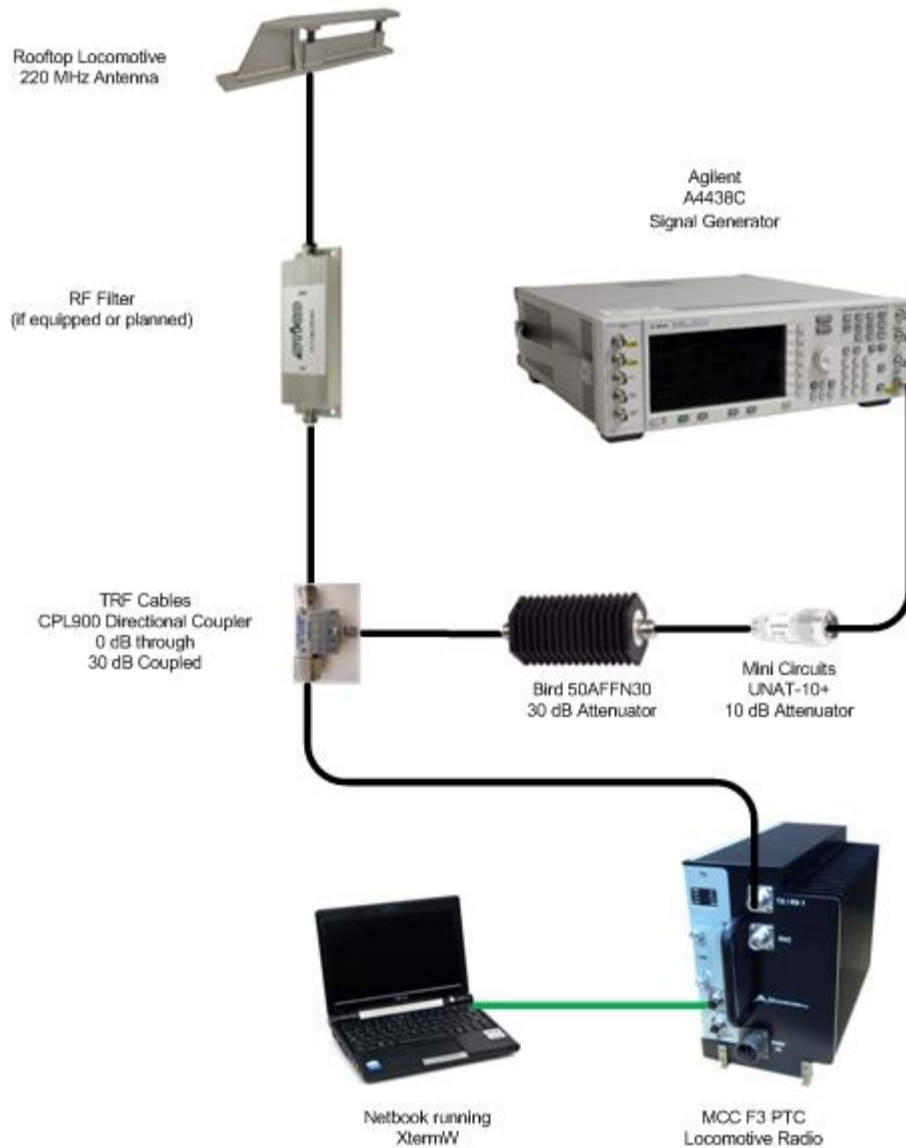
Duration Profile

UP 5802 Shutdown Sequence

Figure 39

### BER Testing

The purpose of this test is to determine the impact on receiving PTC transmissions in the locomotive noise environment, with the focus on capturing the minimum signal level needed for radio network planning. To accomplish this, a PTC Locomotive Radio (F3) was connected through a Directional Coupler to a Signal Generator equipped with an attenuator pad, and to the worse-case locomotive PTC Antenna. See Figure 40.



BER Testing Configuration  
Figure 40

The PTC Radio's design is based on a Receiver noise floor of -123 dBm, and a C/N ratio (for sustaining a BER of E-4) of 11 dB, and a C/I (for sustaining a BER of E-4) of 14 decibels.

To establish a baseline, the PTC Antenna was disconnected from the Directional Coupler port, and the port was terminated. This effectively isolated the radio from the noise environment. The Signal Generator was configured to send a Test Pattern, and the signal level was set so that a BER of E-4 was sustainable. In this configuration, the PTC Radio was able to report a BER of E-4 at -113 dBm. Note that this radio, under these test conditions, was performing slightly better than spec with a C/N of 10 decibels.

The PTC Antenna was then reconnected, and the test was repeated for each of ten Locomotive Operational States (Engine Off, Idle, and Notches 1 through 8). The limitations of the test do not permit reliable BER measurements for brief conditions such as Startup Sequence and Shutdown Sequence, so these two locomotive operational states were not tested.

The worse-case level observed for a reliable BER of E-4 was -103 dBm.

The following table shows the observed minimum signal levels required to sustain a BER of E-4 for the Baseline, and for the ten Locomotive Operational States.

**TABLE E BER Test Results**

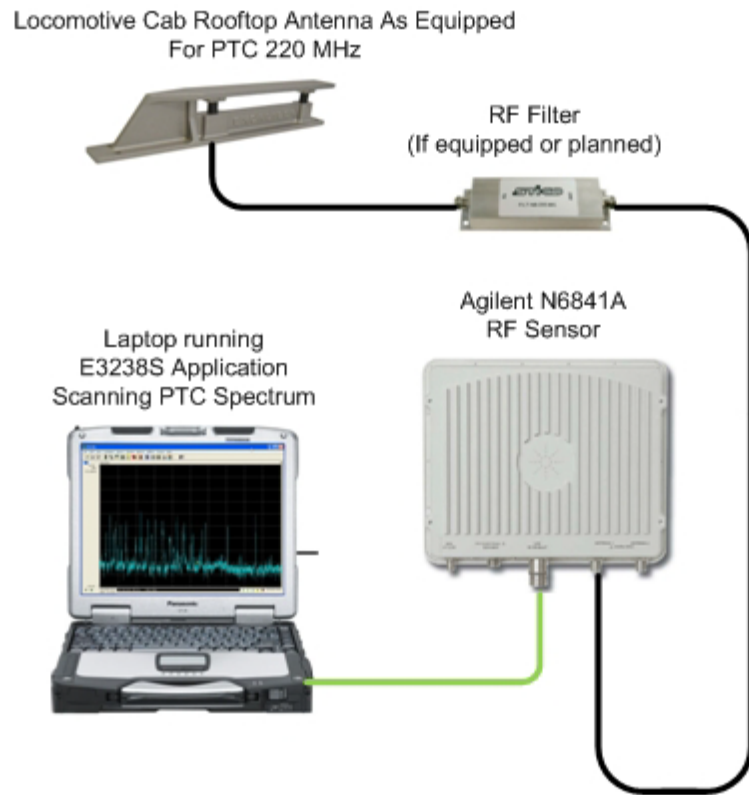
<b>Locomotive State</b>	<b>BER E-4 Level</b>
Radio Isolated	-113
Off	-107
Idle	-104
Notch 1	-103
Notch 2	-103
Notch 3	-105
Notch 4	-106
Notch 5	-105
Notch 6	-105
Notch 7	-104
Notch 8	-104

## Locomotive run through Stevens Pass



Stevens Pass Run  
Figure 41

During testing of the Locomotive, an opportunity to measure aggregate noise in the 220 MHz spectrum while in motion and under load was presented. The locomotive under test was coupled into a Consist of seven Locomotives, carrying a typical revenue train from the BNSF Delta Yard in Everett, Washington, following the US Route 2, over Stevens Pass (see Figure 41), through some tunnels, most notably, the Cascade Tunnel (red line segment), which is some 8 miles in length, finally terminating in Wenatchee Washington. The route was then reversed. The original intent was to capture any detectable EMI being generated by the Traction Motors of this specific locomotive. During testing, it soon became evident that separating the EMI of the locomotive under test from the other six locomotives in the Consist, as well as the passing Locomotives of other trains would not be possible. However, the information is still useful in that it reflects what the PTC-220 Radio receiver would be exposed to in an actual operating environment.



EMI Testing Configuration  
Figure 42

### **EMI Observations- Revenue Run From Everett, Washington to Wenatchee, Washington**

The text below will reflect observations from both test locomotives in the Consist (BNSF 5018, and UP 5802), and will reference data files from both. While still useful for understanding the EMI environmental exposure to PTC-220 Radios installed on locomotives, the discussion will be more qualitative than quantitative, even though the Energy History Files will be included in the Appendix.

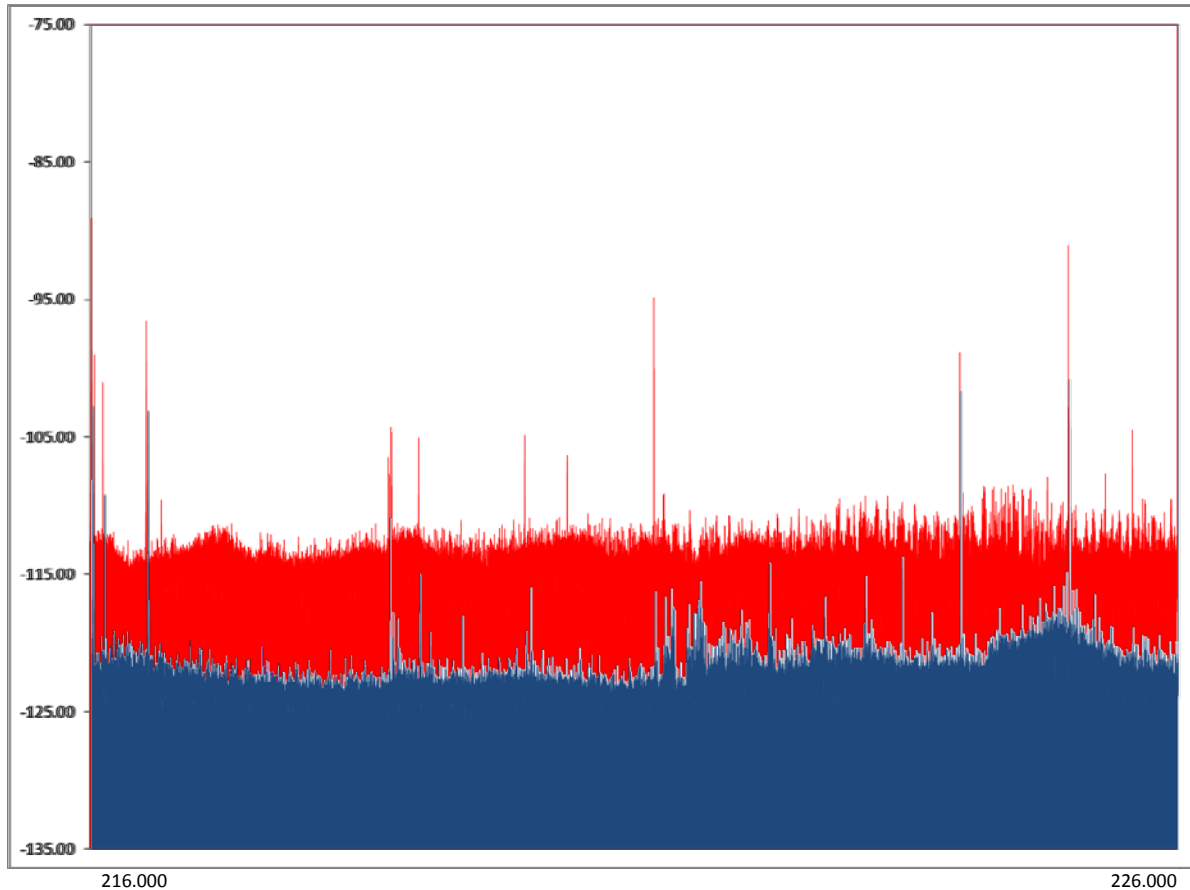
The Agilent RF Sensor (Model N6841A) was connected to the Conductor-side PTC 220 Antenna and Filter. Energy History Files were generated under various conditions of interest as they presented themselves.

Two data-capture methods were available during this set of observations. The RF Sensor captures data for its Energy History files using an Energy Threshold setting. Any energy exceeding the amplitude of the Energy Threshold setting will be captured and quantified. The two types of Energy Thresholds of interest are:

- Flat Energy Threshold—the operator selects a specific threshold, in dBm, and any Energy encountered across the frequency sweep that exceeds that level is measured and collected in the Energy History File. This approach is most useful in reasonably controlled conditions, such as Static EMI Testing and Intermodulation Testing;
- Energy Environment Threshold—the operator chooses some value, in dB, above the ambient Energy, and lets the instrument characterize the ambient peak Energy. This builds a mask, under which all Energy encountered will be ignored, and any Energy above the mask is measured and collected in the Energy History File. This approach is most useful in uncontrolled conditions, where a change in environment is anticipated;

The Energy Environment Threshold, in this test environment, is the more useful of the two, and files so captured are referenced in the discussion that follows.

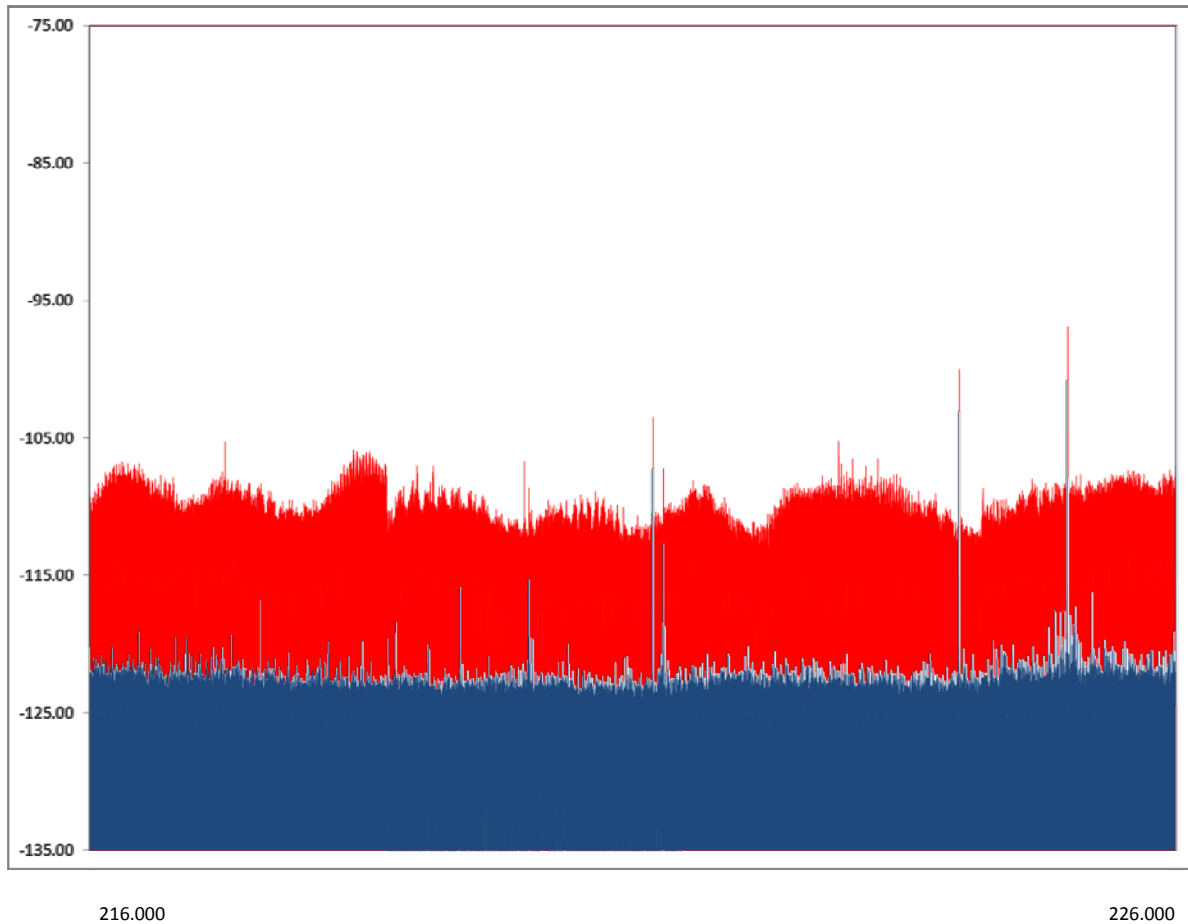




Departing yard  
Figure 43

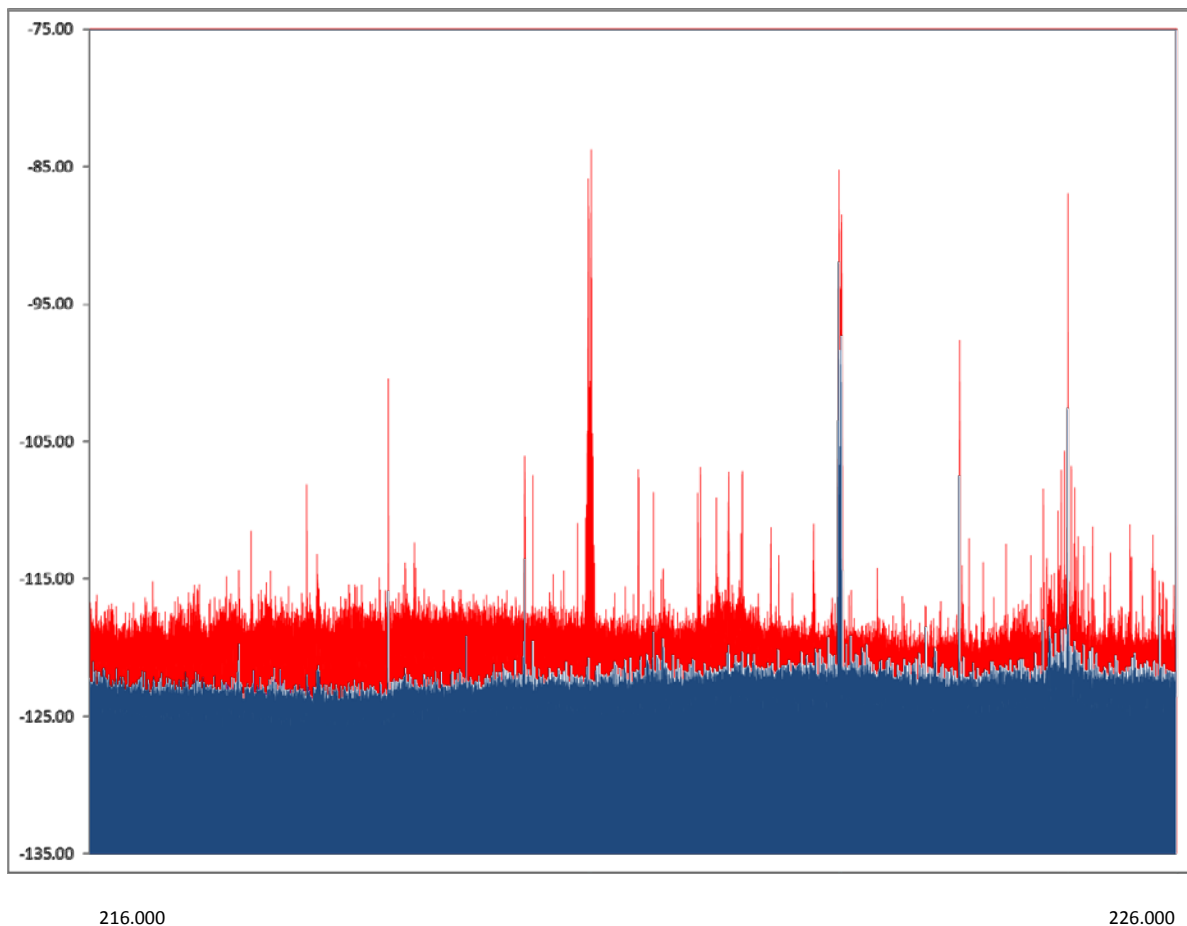
The first condition of interest that presented itself occurred as the Consist departed the yard. The instrument had been allowed to build an Energy Environment Threshold, and the threshold was set at 1 dB above Ambient Peak. As the train left the yard, there was a series of very brief transient events ranging from 4 dB to 11 dB over Ambient Peak. The events were few (order of magnitude of E+1 detections or less), narrow in bandwidth, and short lived (E-1 milliseconds or less). It is unclear what equipment on the yard perimeter may have been responsible for these disturbances, and, given the revenue nature of the run, it was not feasible to stop the train in order to explore the disturbances. See associated files labeled 'Idle Rolling Noise Departing Yard'.





Power Lines  
Figure 44

The next condition of interest involved passing another freight train. The instrument had been allowed to build an Energy Environment Threshold, and, again, the threshold was set to 1 dB above Ambient Peak. As the other train's locomotives passed, there were no Detections of any energy above Ambient Peak. However, there was a series of brief transient events when several Automobile Carrier type rolling stock passed by. It appeared that the rolling stock was empty, and a quick visual scan of the surrounding environment identified a three phase power utility line running parallel to the tracks, then diverging way. These appeared to be at least sub-station intertie level voltages (likely in the 120kV range or higher). Given the nature of the disturbance, and no easily associative observations regarding the passing train, it is possible that the transient events were generated by the proximal electrical utility facilities. See associated files labeled 'Rolling Noise 3'.



Cascade Tunnel  
Figure 45

The next condition of interest involved the approach to, and the traverse within, the Cascade Tunnel. The instrument had been allowed to build an Energy Environment Threshold, and, again, the threshold was set to 1 dB above Ambient Peak. The intent was to observe how much, if any, EMI Noise generated by the locomotive would be reflected by the confined space and materials of such a tunnel back into the PTC 220 Antenna aperture. Not surprisingly, Energy Amplitude rose once inside the tunnel. Much of the noise characteristics captured are similar to what was seen in the Static EMI Testing elsewhere in this report. However, given the isolated nature of the tunnel environment, it is unlikely that the anomalous signals (spikes) shown in the above figure were being generated by 'non-PTC-220 users' when actually inside the tunnel. However, it is of note to explain that human occupation of any Locomotives other than the Lead locomotive while inside the Cascade Tunnel is prohibited by BNSF for Environmental Human Exposure reasons, so it is possible that these anomalous signals (spikes) were intercepted at the Tunnel Portals while the Test Operators were unable to observe the Test Equipment in real time. Given the logistics of a revenue run, it was not feasible to stop the train to explore the source of these disturbances. See associated files labeled 'Cascade Tunnel'.

**Summary:**

**VSWR:**

The VHF antenna reflection response passes the manufacturers specification both with and without the filtering applied.

Both of the 220 MHz PTC band antennas passed all manufacturers specifications. The EOT, DPA, and DPB all passed VSWR testing.

All cellular, SPEC 200, and 802.11 antennas passed the manufacturers VSWR specification.

**Insertion Loss:**

All cabling tested was within allowable limits for insertion loss. No mechanical errors were found.

**Antenna Isolation:**

The antenna isolation testing shows how the addition of filtering will improve the electrical isolation between the different antenna systems. Filtering of all significant contributor radios is emphatically recommended. Significant contributor radios include AAR VHF Voice, Distributed Power UHF A, Distributed Power UHF B, HOT, and both branches of the PTC 220 Radio.

**Receive Intermodulation Testing:**

With the applied OEM filtering no intermodulation effects were noted.

**Transmit Intermodulation Testing:**

With the applied OEM filtering no intermodulation effects were noted. However, there is a known issue with High Level FM Broadcast signals mixing in the PA section of the AAR VHF Voice Radio when it is transmitting. See Locomotive Noise Test Battery Reports for CSX-4022, CSX-985, NS-2623, and NS-8898.

**EMI Testing:**

Electromechanically generated power plant noise during the twelve Locomotive Operational States (Engine Off, Startup Sequence, Idle, Notches 1 through 8, and Shutdown Sequence) were less disruptive than expected, except for the Startup Sequence and the Shutdown Sequence. However, some auxiliary devices not fully identified produced intermittent disruptions. Methods to isolate and measure the emissions of these devices on a similar Locomotive have been subsequently developed. See Locomotive Noise Test Battery Report CSX-985.

**BER Testing:**

Since the EMI Noise is an on-platform phenomenon, any EMI produced travels with the PTC Radio Receivers. The testing, to date, has established a worse case noise number of 10 dB, and this should be accounted for in the PTC Locomotive Radio Receive Path Link Budget.